Introduction to Wastewater Treatment Table of Contents

Section 1	Introduction to Wastewater Treatment	Page 1
Section 2	Preliminary Treatment	Page 17
Section 3	Flow Measurement	Page 49
Section 4	Activated Sludge Systems	Page 71
Section 5	Fixed Film Systems	Page 105
Section 6	Sedimentation and Floatation	Page 141
Section 7	Ponds and Lagoons	Page 171
Section 8	Disinfection	Page 201
Section 9	Effluent Disposal	Page 237
Section 10	Administration and Management	Page 251
Section 11	Safety	Page 261
Section 12	References & Need to Know Answers	Page 287
Section 13	to Vocabulary	Page 305

Section 1 Introduction to Wastewater Treatment





Section 1 Introduction to Wastewater Treatment





History of Wastewater – Romans Water from the baths, toilets, fountains, etc. + urban runoff was discharged into collection system · Few private connections to the sewers - Rich paid to use public toilets, poor used chamber pots No significant improvements in collection systems until the 1840's (17 centuries later)

History of Wastewater - 1800's

- 1817 1824: First Cholera Pandemic
- South Asia + Southeast Asia + Middle East little is known
- 1829 1849: Second Cholera Pandemic
- India to Asia + Europe + United Kingdom + Americas
- 1854: London Cholera Pandemic
 - · Dr. John Snow collected and mapped cholera data that led to the identification of epidemic's source - contaminated public drinking water





Know this acronym!!!

3

Important Dates

- 1948: Federal Water Pollution Control Act
- · Basis of Clean Water Act first major U.S. law to address water pollution
- 1972: Clean Water Act
 - 1948 Act amended Establishes the basic structure for regulating discharges of pollutants to U.S. waters
 - · Primary objective: restore and maintain the chemical, physical, and biological integrity of U.S. waters
 - National Pollutant Discharge Elimination System (NPDES) permits



4

National Pollutant Discharge Elimination System (NPDES) Permits

- · Typically specify:
 - Discharge location
 - · Allowable discharge flows
 - · Allowable concentrations of pollutants in the discharge
 - "Mass loading" typically expressed in mg/L or lbs/day
 - · Limits of the mixing zone (if any)
 - · Area where wastewater discharged from a permitted facility enters and mixes with a stream or water body
 - · Sampling, monitoring, and reporting requirements

Before discharge, municipal wastewater must have secondary received treatment to meet water quality standards

5

Objectives of Wastewater Treatment

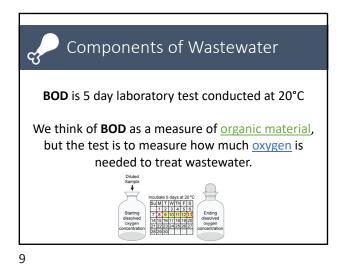
- Overloading a waterbody with wastewater can cause:
 - Low dissolved oxygen (DO) in the water
 - · Fish Kills
 - Algae blooms*
 - · Spread of waterborne diseases like cholera
 - · Violations of safe drinking water standards

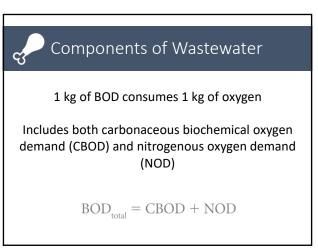


Nutrients discharged to rivers and lakes act like fertilizer and can cause algae



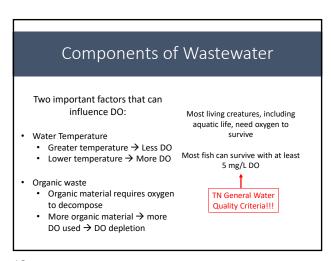


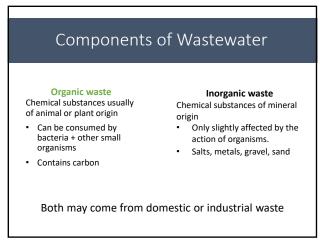




10

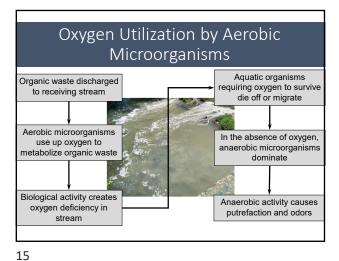






Components of Wastewater **Organic** waste The treatment plant removes the organic matter the same way a stream would in nature Objective: Prevent as much of this "oxygen-demanding" organic material as possible from entering the receiving water by using microorganisms to stabilize and remove organic matter in secondary treatment

13 14



Components of Wastewater **Nutrients** · Macronutrients: Nitrogen **Eutrophication** • Phosphorus Iron · Problems associated with excess nutrients: Act as fertilizer – algae blooms Eutrophication · Odor problems • Extra vegetation near surface may inhibit light penetration



Components of Wastewater **Solids** Acronym Term Definition TSS Total Suspended Solids Solids that cannot pass through a 1.2-µm filter Solids that cannot pass through a 1.2-µm filter AND are burned away when placed in a furnace at 550 °C Total Volatile Suspended Solids TVSS Solids that are small enough to pass through a 1.2-µm filter. The sample must be dried completely before the dissolved solids can be seen with the naked eye. All of the solid material in a sample. This includes both organic and inorganic solids. TS = TSS + TDS TS Total Solids All of the solids in a sample that are burned away when Total Volatile Solids TVS placed in a furnace at 550 °C.

17 18

Components of Wastewater

- Organic Solids + Inorganic Solids
 - Organic can be treated by biological processes, inorganic cannot
- · Suspended Solids
 - · Particles that settle
- · Dissolved Solids
- "Soluble solids" particles that do not settle
- Colloidal solids are measured in the total dissolved solids test even though they are not truly dissolved

 Colloids: particles that art
- Total solids
- Suspended Solids + Dissolved Solids

Colloids: particles that act as if they are dissolved because they are so small that even random thermal currents in water keep them from settling.

Fats, Oils, and Grease

• Generally listed under one heading called FOG as it is often not important to know the exact make-up of this group of components.

Sewer Blockage Formation

The start of a blocked pipe begins when grease and solids collect on the top and sides of the pipe interior.

The bulld-up increases over time when grease and other debris are washed down the drain.

Excessive accumulation will restrict the flow of wastewater and can result insamilary sewer overflow.

19



Wastewater Characteristics

Fresh Wastewater

- Usually a grey/dishwater color
- Domestic wastewater has a musty/earthy
 odor



21

Septic Wastewater

- · Typically a black color
- Can change to a rotten egg odor associated with the production of hydrogen sulfide gas



Components of Wastewater

Sludge and Scum



20

22

- If wastewater does not receive adequate treatment, solids may build up in the receiving stream as sludge (settled) or scum (floating)
- Unsightly
- May cause oxygen depletion
- Source of odors

Components of Wastewater

Turbidity

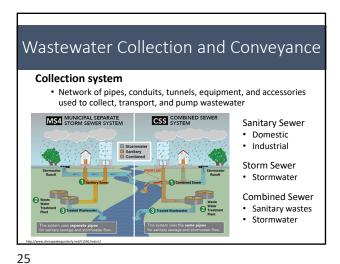


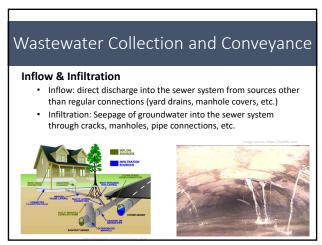
- measures the cloudiness of water
- A light is shined through the water and a detector, placed at a 90-deg angle to the light source, measures the amount of light scattered by suspended particles in the water.

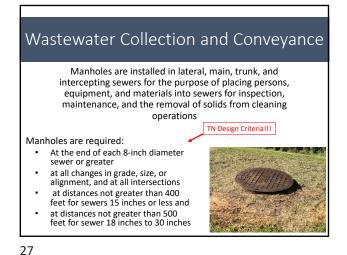
Wastewater Collection and Conveyance









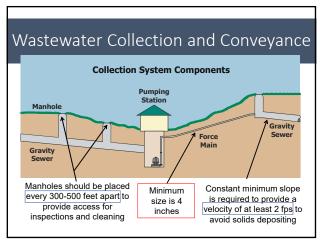


Relation to Water Mains

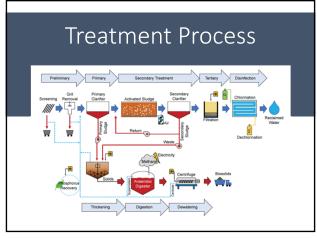
Horizontal Separation: Maintain at least 10 feet of horizontal separation between the sewer and any existing or proposed water main measured edge to edge.

Vertical Separation: Whenever sewers must cross under water mains, install the sewer at such elevation that the top of the sewer is at least 18 inches below the bottom of the water main.

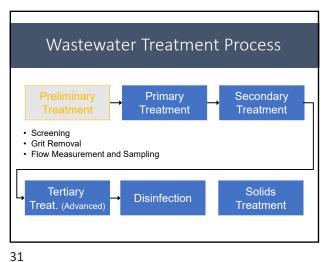
28

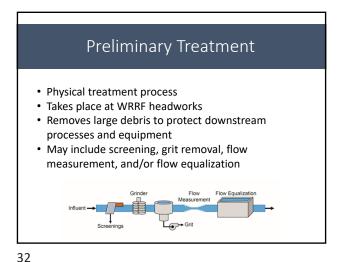


29



9

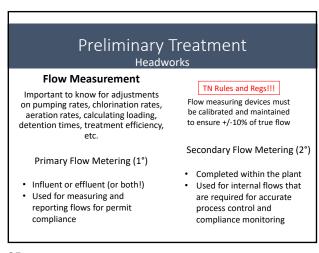




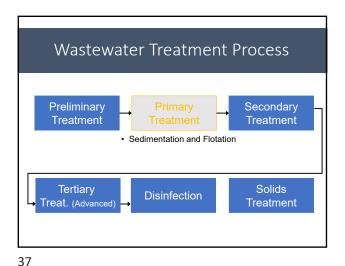
Preliminary Treatment Screening Protect equipment against damage such as clogging of pipes and pumps by removing larger debris (roots, rags, cans, etc.) Manual or Mechanical Openings can be from a few millimeters to 2 in. · Coarse, bar, fine, & micro "Blinding off": excess material accumulates on screen & water can't move easily through openings

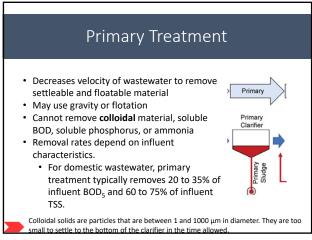
Preliminary Treatment Grit Removal Fine, discrete, nonbiodegradable particles that have a settling velocity greater than organic solids Sand, eggshells, gravel, coffee grounds, etc. Protects equipment from abrasion and accompanying 1 ft/sec flow through grit Know this!!! chamber

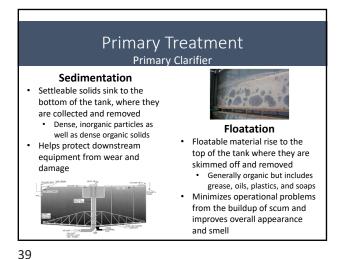
33 34

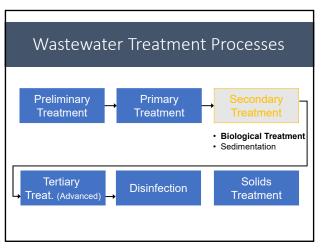


Preliminary Treatment Headworks Sampling Collected to obtain, develop, and use Composite Sample representative data for a variety of A single, larger sample that is needs prepared by combining a series of smaller grab samples **Grab Sample** over a known time or flow Represents one moment in time intervals and is not mixed with any other Minimum of 8 samples, at samples least 100mL each, collected Defined by U.S. EPA as samples over a 24-hour period that are collected over a period TN requirement: Flow of 15 minutes or less. proportioned TN Rules and Regs!!!

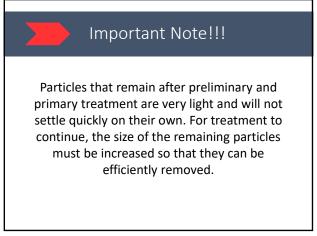


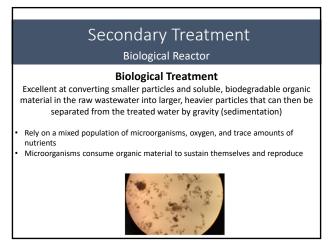


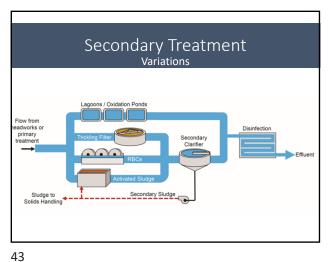




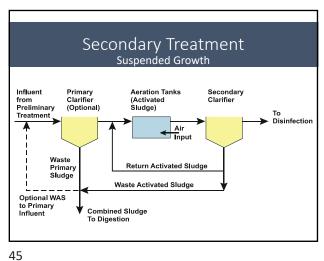
40

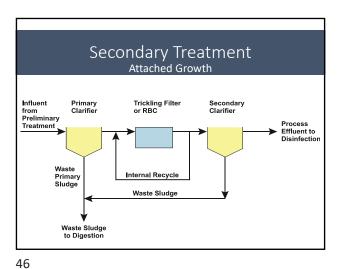


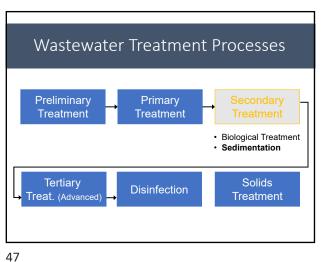


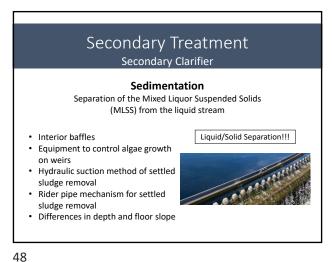


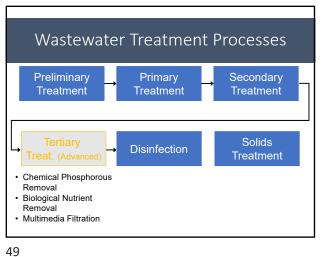


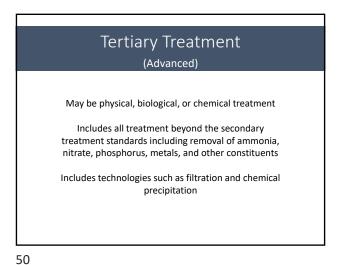


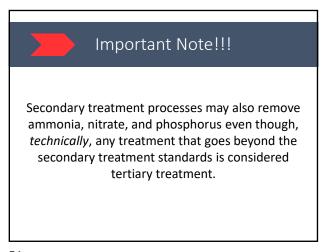


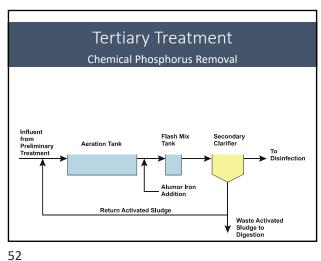


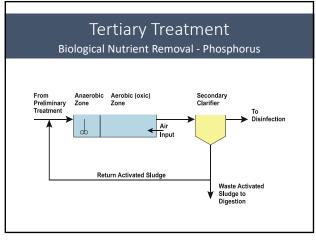


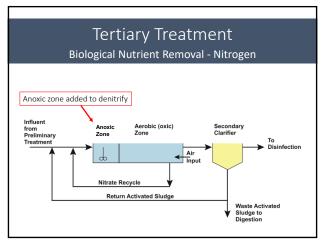






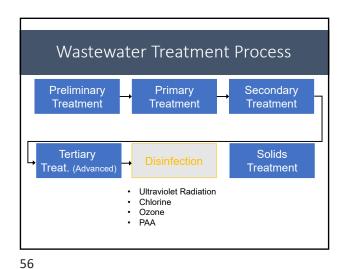


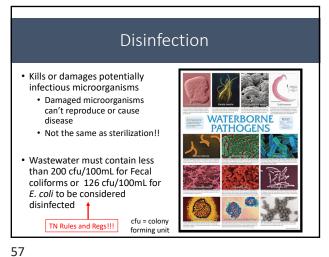




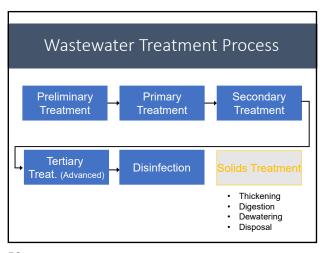
53 54

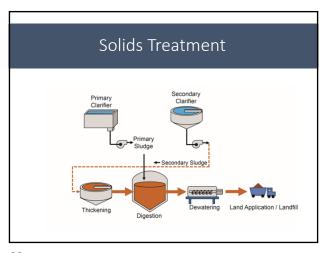






Disinfection **Ultraviolet Radiation** Uses UV light to damage the DNA of microorganisms Chlorine Chlorine Gas (Cl₂) Ozone 100% pure chlorine • Produced when oxygen (O2) Sodium Hypochlorite (NaOCI) molecules are exposed to an bleach energy source and converted Calcium Hypochlorite [Ca(ClO)₂] Solid – powder, granular, disk, briquette, tablet form to the unstable gas ozone (O_3) Generate on site because it is unstable





59 60

Solids Vocab

Sludge

 encompasses any and all solid material—scum, settled solids, and floatables—that is removed from wastewater during treatment.

Biosolids

 refers to stabilized solids that have been thoroughly treated and meet regulatory criteria. Biosolids may be beneficially reused as a soil amendment and fertilizer or can be sent to a landfill

Residuals

 refers to the solid material left over after liquid treatment is completed

Solids Treatment 1. Thickening 3. Dewatering Increases solids 2. Digestion Reduce volume concentration · Reduce volatile solids (excess water) of Low enough solids sludge for further · Aerobic + Anaerobic concentration (2%-· Microorganisms use processing or 10%) that they internally stored food + disposal remain pourable consume organic Higher solids material from primary concentration (10%sludge (if available) 45%) and no longer Dead microorganisms pourable become food for survivors 4. Disposal • 40 CFR Part 503:

Class A or Class B

62

61





Introduction Vocabulary

1.	The impairment of water quality by agricultural, domestic, or industrial wastes to the point where the water is unusable, offensive, or poses a potential threat to human health or the environment is called
2.	Water discharged directly into a sewer system from sources other than regular connections is called This includes flow from yard drains, foundations, and around access and manhole covers.
3.	A refers to any substance that is taken in by organisms and promotes growth. Nitrogen and phosphorus are examples that promote the growth of algae.
4.	are a group of bacteria that are used as "indicator organisms," which means their presence may indicate that the water is polluted with pathogenic organisms.
5.	Organic material undergoes by bacteria, in which the material is converted to gases and other relatively inert substances. Stabilized organic material generally will not give off obnoxious odors.
6.	Thetest , which lasts for 5 days, is the amount of oxygen used during the breakdown of organic material. It is considered an indirect measure of the organic content of a sample.
7.	A wastewater treatment process that takes place in a rectangular or circular tank (ex. Primary clarifier) and allows those substances in wastewater that readily settle or float to be separated from the wastewater being treated is referred to as
8.	refers to the seepage of groundwater into a sewer system, including service connections. This seepage frequently occurs through defective or cracked pipes, pipe joints and connections, interceptor access risers and covers, or manhole walls.
9.	sewers carry waste (mostly domestic) from homes and commercial businesses sewers collect runoff from streets, land, and building roofs and is normally discharged to a waterway without treatment. A sewer system combines the two previously listed sewer systems into one, these types of sewers often become overloaded during heavy storms.
10.	Waste material that comes from animal or plant sources is classified as waste. These natural wastes generally can be consumed by bacteria and other small organisms.
11	
11.	The process is used to convert dissolved or suspended materials

	settle out.	
12.	A stream, river, lake, ocean, or other surface or groundwaters into which treated or untreated wastewater is discharged is called a	
13.	The water that has been treated and is discharged to a receiving stream, river, lake, or ocean is called NPDES permit limitations apply to this discharge.	
14.	Waste material such as sand, salt, iron, calcium, and other mineral materials that are only slightly affected by the action of organisms is classified as waste.	
Wo	ord Bank	
Infl	ow	
Effl	uent	
Cor	mbined	
Wa	ter pollution	
Col	iforms	
Nut	trients	
Sec	condary treatment	
Prir	mary treatment	
San	nitary	
Org	ganic	
Bio	chemical oxygen demand (BOD)	
Red	ceiving water	
Infi	ltration	
Sto	rmwater	
Ino	rganic	
Sta	bilization	

generally a type of biological treatment followed by secondary clarifiers that allow the solids to

Section 2 Preliminary Treatment







Preliminary Treatment

The removal of large debris that may hinder the operation of a treatment plant



Large debris can consist of:

- Sticks Plastic products
- Scrap metal Rags/Trash Rocks • Sand
- Large debris must be removed to prevent:
 - Blockages of pipes
 - Damage to pumps
 - Excessive wear on pumps and chains
 - Filling of digesters
 - Plant operating at reduced capacity

2



Screening

- Screens must be cleaned or raked by either manual or automatic control methods
- The type of screening selected will depend on which treatment processes are downstream and how much protection they require
- Debris collected on the screen depends on the opening space and the size, configuration, and amount of debris
- Screenings are typically sent to landfill for disposal



This Photo by Unknown Author is licensed under CC BY-ND

Categorized based on size opening:

- Coarse Screens
- Fine screens
 - Microscreens

₹

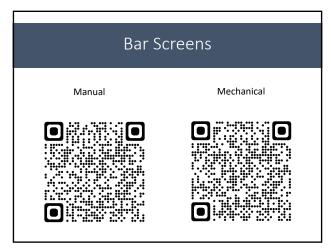
Screening Fine Screens **Coarse Screens** Trash/Bar Rack Bar Screens Perforated Plate Closely spaced bars Chain/Cable-Driven Single Rake Multiple Rake Stair (Step) Screen Catenary Drum Continuous Self-Cleaning Continuous-Element Inclined Cylindrical

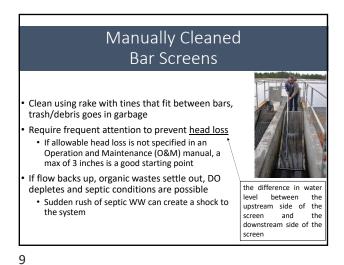
5

Coarse Screens Coarse Screens Manually cleaned: 1-2 inches between **Bar Screens** Trash/Bar Rack openings Spacing is 3/8-inch Spacing is 3-4 to 2 inches inches or more Mechanically cleaned: no less Manually or Typically used for than 5/8-inch mechanically bypass channels or openings combined systems cleaned Mechanically Manually or cleaned mechanically TN Design Criteria!!! recommended for cleaned facilities greater than 1 MGD

6







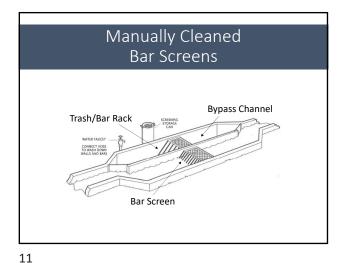
Manually Cleaned
Bar Screens

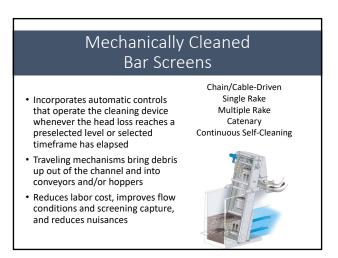
DEBRIS

TROUGH

HEAD LOSS

10





Chain/Cable-Driven Screen



How it Works:

- Two points of tension at the upper and lower sprockets that keep the chain taught
- Typical front-cleaning unit includes a toothed hopper (rake) that swings out from the bar screen as it travels down to the bottom of the channel
- When the channel reaches the bottom of the channel, cables, chains, or cogwheels draw the toothed hopper toward the bar screen
- The teeth of the hopper then slide between the bars and drag the screenings out of the wastewater

Single Rake Screen

How it Works:

- Simulates the movement of a person raking the screen
- Consists of stationary components (frame, bar rack, dead plate, and pin rack) along which the rake assembly travels
- A rake arm engages the screening materials and lifts it up and out of the channel
- Typically goes through a single operation cycle when initiated by timer or differential water-level signal



13

14

Multiple Rake Screen



How it Works:

- Similar to a single rake screen but with multiple rakes
- Stationary components (frame, bar rack, dead plate, and pin rack) along which the rake assembly travels
- Rake arms engage the screening materials and lift it up and out of the channel

Catenary Screen

How it Works:

- Similar to chain-driven and multiple rake screen
- Instead of having a flexible chain, catenary screens use rigid metal links or bars with joints that lock with one another
- Catenary screens only have one point of tension: the sprocket at the top



15

16

Continuous Self-Cleaning Screen



How it Works:

- Continuous belt of plastic or stainless-steel elements that are pulled through the wastewater to provide screening along the entire submerged length of the screen
- Solids are captured on the face of the screen and as the belt rotates, teeth protrude on the upward movement to collect screenings

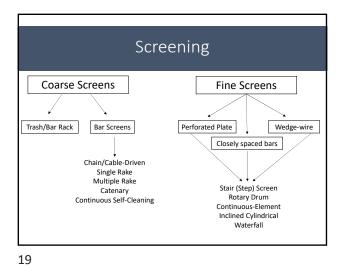
Mechanically Cleaned Bar Screens

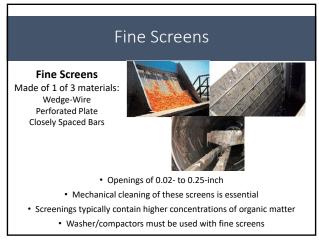
Maintenance

Preventative maintenance is key – routine inspection, lubrication, and repair (at recommendations of equipment supplier)

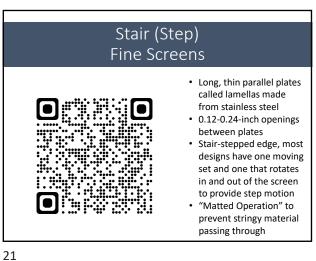
- Observe all moving mechanisms to determine if the components are free of obstructions, properly aligned, moving at constant speeds, and producing no unusual vibrations
- Lock out power to unit and divert flow through another channel before performing maintenance
- Chain drives require frequent replacement of chains, sprockets, and other parts

17

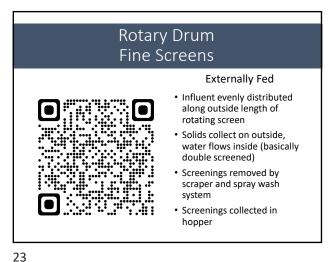


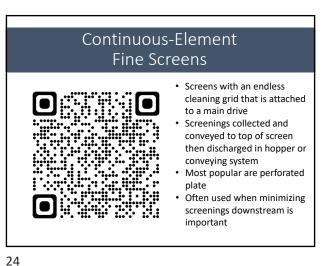


22



Rotary Drum Fine Screens Internally Fed · Influent fed into center · Wastewater enters open end of drum and flows outward through rotating drum filter Spray systems wash debris off the screen and into hopper · Screenings removed by auger/conveyor for disposal





Inclined Cylindrical Fine Screens



- · Cylindrical screening basket with an internal screenings removal mechanism that is typical a helical screw
- Typical installed at 30°- 45°
- Screenings drop into hopper
- Big advantage: supplied with internal washer/compactor
- Large footprint and shallower influent

Wedge-Wire Waterfall Fine Screens



- Simple screen with no moving parts
- · Influent flows over the top of the concave face of screen
- · Gravity and weight of new screenings push debris down
- · Not recommended for wastewater that contains grease
- 0.010-0.100-inch opening

25 26

Comminutors

- Grinds or chops solids that could interfere with downstream processes
- Solids stay in water + decrease treatment capacity
- Cutting teeth mounted in rows on
- Shredded rags can adversely affect operation and maintenance of primary clarifiers, thickening units, and dewatering units
- Often used in pump stations, smaller plants, and ponds



27

Macerators

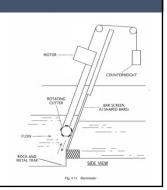
- Designed for in-line pipe installation + best suited for refined cutting after the headworks
- Perforated sheer plate and rotating headstock
- These units tend to do better with small solids like hair, wipes, rags, and plastics as compared to large heavy solids
- Heavy solids separation (built in "rock trap")



28

Barminutors

- · Variation of comminutor
- · Bar screen made of U-shaped bars and a rotating drum with teeth and "shear bars"
- · The rotating drum moves up and down the bar screen
- Shredded material continues with the waste stream



Comminutors, Macerators, and Barminutors

Maintenance

Preventative maintenance is key – routine inspection, lubrication, and repair (at recommendations of equipment supplier)

- Observe all moving mechanisms to determine if the components are free of obstructions, properly aligned, moving at constant speeds, and producing no unusual vibrations
- Check for debris hung up in cutting drums and bars
- If stringing parts of rags are hanging from slotted drum or U-shaped bars of comminutor, it may indicate that the cutter is worn or out of adjustment - sharpen and adjust cutting blades

Indicator/Observations	Probable Cause	Check or Monitor	Solutions
1. Obnoxious odors, flies, and	1. Accumulation of rags and	1. Method and frequency of debris	1. Increase frequency of removal and
other insects	debris	removal	disposal to an approved facility.
2. Excessive grit in bar	2. Flow velocity too low	2. Depth of grit in chamber,	2. Remove bottom irregularity or
screen chamber		irregular chamber bottom, flow	reslope the bottom.
		velocity	Increase flow velocity in a chamber.
			Flush regularly with a hose.
3. Excessive screen clogging	3a. Unusual amount of debris	3a. Upstream conditions	3a. Identify source of waste causing the
	in wastewater. Check	3b. Cleaning frequency	problem so discharge can be stopped.
	industrial wastes.		3b. Increase cleaning frequency.
	3b. Inadequate cleaning		
	frequency		
 Mechanical rake inoperable, 	4. Jammed mechanism	4. Screen channel	4. Remove obstruction. Adjust spring
circuit breaker will not reset			tension if appropriate.
5. Rake inoperative, but motor	5a. Broken shear pin	5a. Inspect shear pin.	5a. Identify cause of break and replace
runs	5b. Broken chain or cable	5b. Inspect chain.	shear pin.
	5c. Broken limit switch	5c. Inspect switch.	5b. Replace chain or cable.
			5c. Replace limit switch.
6. Rake inoperative, no visible	6. Defective remote control	6. Check switching circuits.	6. Verify correct operation of the PLC
problem frequency.	circuit		Replace circuit.
			Then replace circuit and motor.
7. Marks or metal against metal on	7. Screen needs adjustment	7. Operate screen through one	7. Manufacturer's adjustments
screen binding		cycle and listen for or observe	recommended in equipment O&M
		metal-to-metal contact.	manual.
8. Slow operation of grinders,	8. Worn components	8. Operate through one cycle to	8. Lubricate machine as indicated.
screenings press, or belt		identify components. Check	Replace worn components.
conveyors. Screeching sounds		maintenance logs.	
during operation			
9. Thumping sound during	9. Broken or loose	9. Complete inspection of all	9. Replace or tighten component.
operation of screens, grinders,	components	components, nuts, and bolts.	
screenings press, or conveyors			
10. Belt not tracking properly	10. Belt stretched; self-	10. Inspect belts, idlers, and tail	10. Adjust take-up; clean and lubricate
	aligning idlers seized; tail	pulley.	self-aligning idlers; adjust tail pulley
	pulley misaligned		alignment.

Grit Removal **Grit Removal** Fine, discrete, nonbiodegradable particles that have a settling velocity greater than organic solids Sand, eggshells, gravel, coffee grounds, etc. Protects equipment from abrasion and accompanying 1 ft/sec flow through grit chamber Know this!!!

32 31

Grit Removal

Grit Chambers

- Allow grit to settle out while keeping the lighter organic solids moving along to next treatment unit
 - · Rely on differences in settling velocities
 - Slower settling particles require longer basins
- Best velocity is 1 ft/sec*
 - Slowed to 0.7-1.4 ft/sec

*for rectangular and square grit chambers

33

Grit Removal

Velocity slowed by several means:

- · In multiple channel installations, operator may vary number of channels (chambers) in service at any one time to maintain certain velocity
- Use of proportional weirs
- Shape of grit channel
- Using bricks or cinder blocks to change cross-sectional shape or area

Detritus Tanks Earliest grit chambers Constant level, short hydraulic retention time Flow is distributed across the tank inlet to minimize velocity across tank Require grit-washing step to remove organic material and return it to the wastewater stream Even flow distribution is maintained by proper

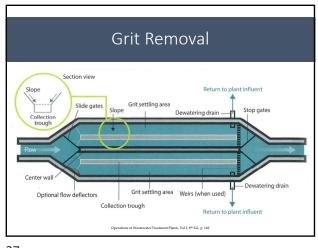
Velocity Control Tanks Velocity is related to the cross-sectional Proportional Weir area according to the formula: · Will maintain the velocity in grit channels when flow $Velocity = \frac{r_{10\pi}}{Area}$ increases Exit area will decrease, thus · Horizontal flow grit chambers use increasing the depth of water proportional weirs to vary the depth flow in the channel in direct of flow and keep the velocity of the proportion to the flow flow stream at a constant 1 ft/sec Debris must not be allowed to accumulate across opening · Constant velocity can also be maintained by giving the grit channel a u-shaped cross-sectional area.

36

34

baffles 35

adjustments of the deflector



Aerated Grit Chamber Air injected through diffusers located along one side of basin near bottom • Diffused air rolls wastewater at 1 ft/sec The mixture of air and water has a lower specific gravity than water, so grit settles out Particles travel in spiral direction Grit removed from hopper by conveyor or is pumped Aeration: · Adds DO and freshens wastewater · Improves sludge settleability · Removes floatables

37

Aerated Grit Chamber

- · If the velocity of the roll is too great, grit will be carried out of chamber
- · If the velocity is too low, organic matter will be removed with grit
- A good way to improve the effectiveness of all type of grit removal systems is to perform a volatile solids test on the collected grit
 - · This should help you adjust your air flow and velocity

Vortex Grit Basin

- Gravity-type chambers that swirl the raw wastewater in the chamber
- Wastewater enters a vortex grit basin through a long, straight, inlet channel
- At the end of the inlet flume, a ramp causes grit that may already be on the flume bottom to slide downward along the ramp until reaching the chamber floor, where it is captured
- The inlet channel connects to the circular portion of the basin along one side, which creates a whirlpool or vortex effect
- The velocity of the vertical roll pattern allows denser particles to settle while keeping lighter organic material suspended
- Natural hydraulics or slow rotating mixer
- Ideal velocity: 1.5 to 3.5 ft/sec



39

40

38

Hand-Cleaned vs. Mechanically Cleaned

Hand cleaned channels

- Used in the smallest facilities with flows less than 1 MGD
- Flow drains to empty tanks for manual removal by shoveling
- Build up could interfere with flow-through velocity and cause wastewater to back up into sewer or cause an overflow

41

Mechanically Cleaned

- Gravity-type units rectangular, circular, square
- Screw augers are most common
- · Larger facilities with larger basins-Chain- and-flights (series of boards)



Flights are moved slowly along bottom and up an incline out of water to a hopper, or along the bottom to an underwater trough where a screw conveyor lifts the grit to a storage hopper or truck. Some designs use conveyor belts with buckets attached

Cyclones use centrifugal force in a cone-shaped unit A pump discharges a slurry of grit and ("primary vortex") bottom

Cyclone Grit Separators

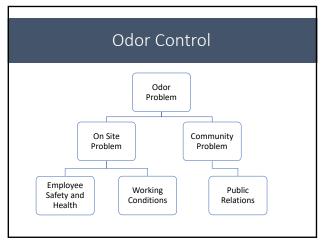
to separate grit and organics from the wastewater

- organics into the cyclone at a controlled rate The velocity of the slurry as it enters along the wall of the cyclone causes slurry to spin or swirl around the outside of the cyclone
- The grit is forced outward to the primary vortex and spirals downward towards
- A larger volume of slurry containing mostly volatile material is carried upward ("secondary vortex") and out the overflow discharge pipe



Disposal of Screenings and Grit • Burial, incineration, or landfilling. Most common · Must pass paint-filter liquids test for landfilling Measures the leaching effect of FREE LIQUID - TEST METHOD screenings • Filter of Mesh No. 60 If any liquid passes through the filter, the material is deemed to contain free liquid 1. Pour in 100 mL of sample 2. Wait five (5) minutes 3. After five minutes if any liquid collects in cylinder see 40 CFR 264.314 and 265-314

44



Odor Control

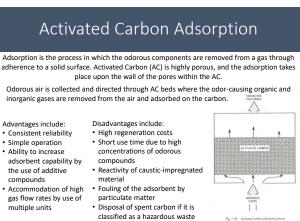
- Hydrogen Sulfide (H₂S)
 - Main cause of odors in wastewater systems
 - Poisonous to respiratory system
 - Rotten egg odor
 - Produced under anaerobic conditions
 - Explosive, flammable, corrosive
 - Dulls sense of smell on exposure
- Ammonia (NH₃)
- Methane (CH₄)

46

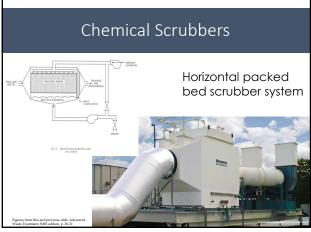
Concentration, ppm	Health effect
0.03	Can smell. Safe for 8-hour exposure.
4	May cause eye irritation. Mask must be used as exposure damages metabolism.
10	Maximum exposure for 8-hour period. Kills sense of smell in 3 to 15 minutes.
20	Exposure for more than 1 minute may cause eye injury.
30	Loss of smell, injury to blood brain barrier through olfactory nerves.
100	Respiratory paralysis in 30 to 45 minutes. Needs prompt artificial resuscitation. Will become unconscious quickly (15 minutes maximum).
200	Serious eye injury and permanent damage to eye nerves. Stings eyes and throat.
300	Loses sense of reasoning and balance. Respiratory paralysis in 30 to 45 minutes.
500	Asphyxia. Needs prompt artificial resuscitation. Will become unconscious in 3 to 5 minutes.
700	Breathing will stop and death will result if not rescued promptly, immediate unconsciousness. Permanent brain damage may result unless rescued promptly.

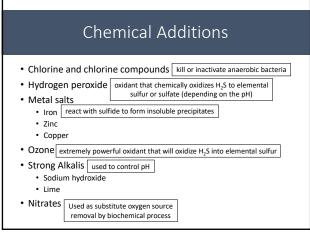
Odor Control Often requires a combination of treating/removing/and reducing potential causes • Vapor-phase odor control methods Atmospheric discharge and dilution Masking agents and counteraction chemicals Chemical wet scrubbing Activated carbon adsorption Bar screens/racks being maintained · Liquid-phase odor control methods and not allowing solids to build up Chemical addition (chlorine) Efficient grit washing/burial/incineration/etc. · Operational odor control methods Collection system improvements and maintenance – ensure 2 fps to Source control Housekeeping improvements avoid solids depositing Process or operational changes

47 48



50 49



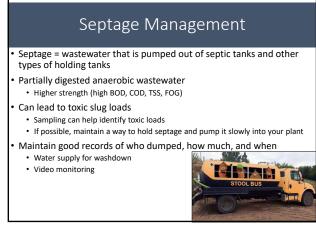


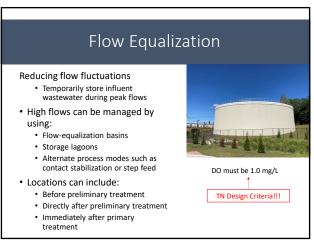
Chemical Scrubbers

• Packed bed is the most common type of wet scrubber system

that uses chemical absorption to control odors.

52







<u>Preliminary Treatment Vocabulary</u>

bles in an aeration tank or reactor. is the heavy material present in wastewater such as sand, coffee grounds, shells, gravel, and cinders. is the gas with a rotten egg odor that is produced under anaerobic
shells, gravel, and cinders is the gas with a rotten egg odor that is produced under anaerobic
is the gas with a rotten egg odor that is produced under anaerobic
distance is in demandable by many breakly and also compressing annually of demanding
ditions. It is dangerous to human health and also very corrosive, capable of damaging
crete. This is the main cause of odors in a wastewater system.
veling rakes bring debris up of out the water channel in a cleaned bar unit.
screens generally have openings of 0.06 – 0.25 inches and are located
vnstream from coarse screens.
simplest type of fine screen that contains no moving parts is called the
een. Influent flows over the top and gravity and the weight of new screenings push the debris
vn.
screens fall into one of two types: internally fed or externally fed.
screen, also called a continuous conveyor, is made up of
nless steel plates with $0.125-0.250$ inch openings which move up and around a top and tom axis.
is a device that acts as both a cutter and a screen. Cutting teeth
unted in rows on the drum shred debris, which is left in the waste stream.
eenings are either buried or incinerated. For landfill disposal, screenings must be dewatered
ough to pass the, which measures the leaching effect of the
eenings.
t described as partially digested anaerobic wastewater, has
n pumped out of septic tanks and other types of holding tanks and is transported via truck to
astewater treatment plant for treatment.
order to allow grit to settle out while keeping the lighter organic solids moving along to the
t treatment unit, a velocity of 1 ft/sec must be maintained in the
particles travel in a spiral direction due to diffused air that rolls the wastewater at 1 ft/sec de the

14.	The principle behind the	separator is that the primary vortex will	
	force the grit outward, while the sec and out the overflow discharge pipe.	ondary vortex carries lighter particles and water upward	
15.		athering of a gas, liquid, or dissolved substance on the another material. Activated carbon is utilized in this process	
16.	•	pochlorite, and hydrogen peroxide are used as the packing systems use the process of chemical to	
17.	A device or tank designed to hold back or store a portion of peak flows for release during low-flow periods is part of the system. According to the TN Design Criteria for Sewage Works, this may be required where peak flows are greater than 2 times the average design flow. Either in-line or side-line systems are acceptable.		
<u>Word</u>	d Bank:		
Flow	equalization	Paint filter test	
Abso	rption	Mechanically	
Diffus	ser	Hydrogen Sulfide (H₂S)	
Septa	age	Grit	
Rotar	ry drum	Screen	
Comr	minutor	Aerated grit chamber	
Grit c	channel	Fine	
Adso	rption	Wedgewire	
Cyclo	nic grit	Escalating step screen	



Wastewater Technology Fact Sheet

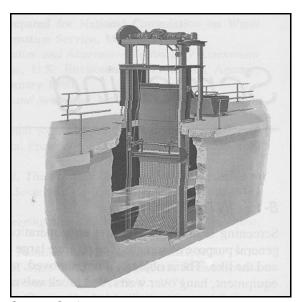
Screening and Grit Removal

DESCRIPTION

Wastewater contains large solids and grit that can interfere with treatment processes or cause undue mechanical wear and increased maintenance on wastewater treatment equipment. To minimize potential problems, these materials require separate handling. Preliminary treatment removes these constituents from the influent wastewater. Preliminary treatment consists of screening, grit removal, septage handling, odor control, and flow equalization. This fact sheet discusses screening and grit removal.

Screening

Screening is the first unit operation used at wastewater treatment plants (WWTPs). Screening removes objects such as rags, paper, plastics, and metals to prevent damage and clogging of downstream equipment, piping, and appurtenances. Some modern wastewater treatment plants use both coarse screens and fine screens. Figure 1 depicts a typical bar screen (a type of coarse screen).



Source: Qasim, 1994.

FIGURE 1 CABLE OPERATED BAR SCREEN

Coarse Screens

Coarse screens remove large solids, rags, and debris from wastewater, and typically have openings of 6 mm (0.25 in) or larger. Types of coarse screens include mechanically and manually cleaned bar screens, including trash racks. Table 1 describes the various types of coarse screens.

Fine Screens

Fine screens are typically used to remove material that may create operation and maintenance problems in downstream processes, particularly in systems that lack primary treatment. Typical opening sizes for fine screens are 1.5 to 6 mm (0.06 to 0.25 in). Very fine screens with openings of 0.2 to 1.5 mm (0.01 to 0.06 in) placed after coarse or fine screens can reduce suspended solids to levels near those achieved by primary clarification.

Comminutors and Grinders

Processing coarse solids reduces their size so they can be removed during downstream treatment operations, such as primary clarification, where both floating and settleable solids are removed. Comminuting and grinding devices are installed in the wastewater flow channel to grind and shred material up to 6 to 19 mm (0.25 to 0.75 in) in size.

Comminutors consist of a rotating slotted cylinder through which wastewater flow passes. Solids that are too large to pass through the slots are cut by blades as the cylinder rotates, reducing their size until they pass through the slot openings.

Grinders consist of two sets of counterrotating, intermeshing cutters that trap and shear wastewater solids into a consistent particle size, typically 6 mm (0.25 in). The cutters are mounted on two drive

TABLE 1 DESCRIPTION OF COARSE SCREENS

Screen Type	Description
Trash Rack	Designed to prevent logs, timbers, stumps, and other large debris from entering treatment processes. Opening size: 38 to 150 mm (1.5-6 in)
Manually Cleaned Bar Screen	Designed to remove large solids, rags, and debris. Opening size: 30 to 50 mm (1 to 2 in) Bars set at 30 to 45 degrees from vertical to facilitate cleaning. Primarily used in older or smaller treatment facilities, or in bypass channels.
Mechanically Cleaned Bar Screen	Designed to remove large solids, rags, and debris. Opening size: 6 to 38 mm (0.25 to 1.5 in). Bars set at 0 to 30 degrees from vertical. Almost always used in new installations because of large number of advantages relative to other screens.

Source: Design of Municipal Wastewater Treatment Plants, WEF MOP 8, Fourth Edition, 1998.

shafts with intermediate spacers. The shafts counterrotate at different speeds to clean the cutters. Figure 2 depicts a channel wastewater grinder.

The chopping action of the grinder reduces the formation of rag "balls" and rag "ropes" (an inherent problem with comminutors). Wastewaters that contain large quantities of rags and solids, such as prison wastewaters, utilize grinders downstream from coarse screens to help prevent frequent jamming and excessive wear.

Grit Removal

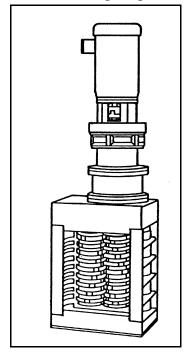
Grit includes sand, gravel, cinder, or other heavy solid materials that are "heavier" (higher specific gravity) than the organic biodegradable solids in the wastewater. Grit also includes eggshells, bone chips, seeds, coffee grounds, and large organic particles, such as food waste. Removal of grit prevents unnecessary abrasion and wear of mechanical equipment, grit deposition in pipelines and channels, and accumulation of grit in anaerobic digesters and aeration basins. Grit removal facilities typically precede primary clarification, and

follow screening and comminution. This prevents large solids from interfering with grit handling equipment. In secondary treatment plants without primary clarification, grit removal should precede aeration (Metcalf & Eddy, 1991).

Many types of grit removal systems exist, including aerated grit chambers, vortex-type (paddle or jetinduced vortex) grit removal systems, detritus tanks (short-term sedimentation basins), horizontal flow grit chambers (velocity-controlled channel), and hydrocyclones (cyclonic inertial separation). Various factors must be taken into consideration when selecting a grit removal process, including the quantity and characteristics of grit, potential adverse effects on downstream processes, head loss requirements, space requirements, removal efficiency, organic content, and cost. The type of grit removal system chosen for a specific facility should be the one that best balances these different considerations. Specifics on the different types of grit removal systems are provided below.

Aerated Grit Chamber

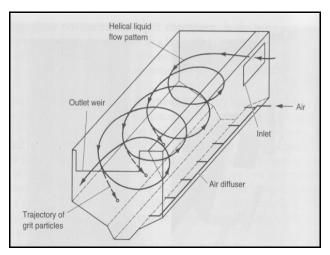
In aerated grit chambers, grit is removed by causing the wastewater to flow in a spiral pattern, as shown



Source: WEF, 1998.

FIGURE 2 WASTEWATER GRINDER: CHANNEL UNIT

in Figure 3. Air is introduced in the grit chamber along one side, causing a perpendicular spiral velocity pattern to flow through the tank. Heavier particles are accelerated and diverge from the streamlines, dropping to the bottom of the tank, while lighter organic particles are suspended and eventually carried out of the tank.



Source: Crites and Tchobanoglous, 1998.

FIGURE 3 AERATED GRIT CHAMBER

Vortex-Type Grit Chamber

The vortex-type grit chamber consists of a cylindrical tank in which the flow enters tangentially, creating a vortex flow pattern. Grit settles by gravity into the bottom of the tank (in a grit hopper) while effluent exits at the top of the tank. The grit that settles into the grit hopper may be removed by a grit pump or an air lift pump.

Detritus Tank

A detritus tank (or square tank degritter) is a constant-level, short-detention settling tank. These tanks require a grit-washing step to remove organic material. One design option includes a grit auger and a rake that removes and classifies grit from the grit sump.

Horizontal Flow Grit Chamber

The horizontal flow grit chamber is the oldest type of grit removal system. Grit is removed by maintaining a constant upstream velocity of 0.3 m/s (1 ft/s). Velocity is controlled by proportional weirs or rectangular control sections, such as

Parshall flumes. In this system, heavier grit particles settle to the bottom of the channel, while lighter organic particles remain suspended or are resuspended and transported out of the channel. Grit is removed by a conveyor with scrapers, buckets, or plows. Screw conveyors or bucket elevators are used to elevate the grit for washing or disposal. In smaller plants, grit chambers are often cleaned manually.

Hydrocyclone

Hydrocyclone systems are typically used to separate grit from organics in grit slurries or to remove grit from primary sludge. Hydrocyclones are sometimes used to remove grit and suspended solids directly from wastewater flow by pumping at a head ranging from 3.7 to 9 m (12 to 30 ft). Heavier grit and suspended solids collect on the sides and bottom of the cyclone due to induced centrifugal forces, while scum and lighter solids are removed from the center through the top of the cyclone.

APPLICABILITY

Because various types of screening and grit removal devices are available, it is important that the proper design be selected for each situation. Though similarities exist between different types of equipment for a given process, an improperly applied design may result in an inefficient treatment process.

Screening

As discussed above, most large facilities use mechanically cleaned screening systems to remove larger materials because they reduce labor costs and they improve flow conditions and screening capture. Typically, only older or smaller treatment facilities use a manually cleaned screen as the primary or only screening device. A screening compactor is usually situated close to the mechanically cleaned screen and compacted screenings are conveyed to a dumpster or disposal area. However, plants utilizing mechanically cleaned screens should have a standby screen to put in operation when the primary screening device is out of service. This is standard design practice for most newly designed plants.

The use of fine screens in preliminary treatment has experienced a resurgence in the last 20 years. Such screens were a common feature before 1930 but their use diminished because of difficulty in cleaning oils and grease from the screens. In the early 1980s, fine screens regained popularity because of improved materials.

Communitors and Grinders

Comminutors and grinders are used primarily at smaller treatment facilities (less than 5 MGD) to process material between 6 and 19 mm (0.25 to 0.75 in) (WEF, 1998). This shredded material remains in the wastewater and is removed in downstream treatment processes.

Grit Removal

When selecting a grit removal process, the quantity and characteristics of grit and its potential to adversely affect downstream processes are important considerations. Other parameters to consider may include headloss requirements, space requirements, removal efficiency, organic content, and economics.

ADVANTAGES AND DISADVANTAGES

Advantages

Screening

Manually cleaned screens require little or no equipment maintenance and provide a good alternative for smaller plants with few screenings. Mechanically cleaned screens tend to have lower labor costs than manually cleaned screens and offer the advantages of improved flow conditions and screening capture over manually cleaned screens.

Communitors and Grinders

A major advantage of using communitors and grinders is that removal of grit reduces damage and maintenance to downstream processes. Comminutors and grinders also eliminate screenings handling and disposal, which may improve the aesthetics of the plant, reducing odors, flies, and the unsightliness associated with

screenings. Some recently developed grinders can chop, remove, wash, and compact the screenings. The use of comminutors in cold weather eliminates the need to prevent collected screenings from freezing. Comminutors and grinders typically have a lower profile than screens, so cost savings can be significant when the units must be enclosed.

Grit Removal

Aerated Grit Chamber

Some advantages of aerated grit chambers include:

- Consistent removal efficiency over a wide flow range.
- A relatively low putrescible organic content may be removed with a well controlled rate of aeration.
- Performance of downstream units may be improved by using pre-aeration to reduce septic conditions in incoming wastewater.
- Aerated grit chambers are versatile, allowing for chemical addition, mixing, preaeration, and flocculation.

Vortex-Type Grit Chamber

- These systems remove a high percentage of fine grit, up to 73 percent of 140-mesh (0.11 mm/0.004 in diameter) size.
- Vortex grit removal systems have a consistent removal efficiency over a wide flow range.
- There are no submerged bearings or parts that require maintenance.
- The "footprint" (horizontal dimension) of a vortex grit removal system is small relative to other grit removal systems, making it advantageous when space is an issue.
- Headloss through a vortex system is minimal, typically 6 mm (0.25 in). These systems are also energy efficient.

Detritus Tank

Detritus tanks do not require flow control because all bearings and moving mechanical parts are above the water line. There is minimal headloss in this type of unit.

Horizontal Flow Grit Chamber

Horizontal flow grit chambers are flexible because they allow performance to be altered by adjusting the outlet flow control device. Construction is not complicated. Grit that does not require further classification may be removed with effective flow control.

Hydrocyclone

Hydrocyclones can remove both grit and suspended solids from wastewater. A hydrocyclone can potentially remove as many solids as a primary clarifier.

Disadvantages

Screening

Manually cleaned screens require frequent raking to avoid clogging and high backwater levels that cause buildup of a solids mat on the screen. The increased raking frequency increases labor costs. Removal of this mat during cleaning may also cause flow surges that can reduce the solids-capture efficiency of downstream units. Mechanically cleaned screens are not subject to this problem, but they have high equipment maintenance costs.

Communitors and Grinders

Comminutors and grinders can create problems for downstream processes, such as increasing plastics buildup in digestion tanks or rag accumulation on air diffusers. In addition, solids from comminutors and grinders will not decompose during the digestion process. If these synthetic solids are not removed, they may cause biosolids to be rejected for reuse as a soil amendment.

Grit Removal

Grit removal systems increase the headloss through a wastewater treatment plant, which could be problematic if headloss is an issue. This could require additional pumping to compensate for the headloss.

The following paragraphs describe the specific disadvantages of different types of grit removal systems.

Aerated Grit Chamber

Potentially harmful volatile organics and odors may be released from the aerated grit chamber. Aerated grit chambers also require more power than other grit removal processes, and maintenance and control of the aeration system requires additional labor.

Vortex-Type Grit Chamber

- Vortex grit removal systems are usually of a proprietary design, which makes modifications difficult.
- Paddles tend to collect rags.
- Vortex units usually require deep excavation due to their depth, increasing construction costs, especially if unrippable rock is present.
- The grit sump tends to clog and requires high-pressure agitation using water or air to loosen grit compacted in the sump.

Detritus Tank

- Detritus tanks have difficulty achieving uniform flow distribution over a wide range of flows because the inlet baffles cannot be adjusted.
- This type of removal system removes large quantities of organic material, especially at low flows, and thus requires grit washing and classifying.

• Grit may be lost in shallow installations (less than 0.9 m [3 ft]) due to the agitation created by the rake arm associated with this system.

Horizontal Flow Grit Chamber

- It is difficult to maintain a 0.3 m/s (1 ft/s) velocity over a wide range of flows.
- The submerged chain, flight equipment, and bearings undergo excessive wear.
- Channels without effective flow control will remove excessive amounts of organic material that require grit washing and classifying.
- Head loss is excessive (typically 30 to 40 percent of flow depth).
- High velocities may be generated at the channel bottom with the use of proportional weirs, leading to bottom scour.

Hydrocyclone

Hydrocyclones require energy because they use a pump to remove grit and suspended solids. Coarse screening is required before these units to remove sticks, rags, and plastics.

DESIGN CRITERIA

Screening

Screening devices are classified based on the size of the material they remove (the screenings). The "size" of screening material refers to its diameter. Table 2 lists the correlation between screening sizes and screening device classification.

In addition to screening size, other design considerations include the depth, width, and approach velocity of the channel; the discharge height, the screen angle; wind and aesthetic considerations; redundancy; and head loss.

Table 3 lists typical design criteria for mechanically cleaned bar rack type screens.

TABLE 2 SCREENING DEVICE CLASSIFICATION

Screening Device Classification	Size Classification/Size Range of Screen Opening	
Bar screen		
Manually Cleaned	Coarse/25-50 mm (1-2 in)	
Mechanically Cleaned	Coarse/15-75 mm (0.6-3.0 in)	
Fine bar or perforated coarse screen (mechanically cleaned)		
Fine Bar	Fine Coarse/3-12.5 mm (0.1-0.5 in)	
Perforated Plate	Fine Coarse/3-9.5 mm (0.1-0.4 in)	
Rotary Drum	Fine Coarse/3-12.5 mm (0.1-0.5 in)	
Fine screen (mechanically cleaned)		
Fixed Parabolic	Fine/0.25-3.2 mm (0.01-0.13 in)	
Rotary Drum	Fine/0.25-3.2 mm (0.01-0.13 in)	
Rotary Disk	Very fine (micro)/0.15-0.38 mm (0.01-0.02 in)	

Source: Crites and Tchobanoglous, 1998.

The use of fine screens produces removal characteristics similar to primary sludge removal in primary sedimentation. Fine screens are capable of removing 20 to 35 percent suspended solids and BOD₅. Fine screens may be either fixed or movable, but are permanently set in a vertical, inclined, or horizontal position and must be cleaned by rakes, teeth, or brushes.

Communitors and Grinders

Figure 4 depicts a typical comminutor. When designing a comminutor, headloss should be considered. Headloss through a comminutor is usually in the range of a few centimeters to 0.9 m (3 ft). Therefore, the manufacturer's ratings should be decreased by 70 to 80 percent to account for clogging of the screen, since manufacturer's headloss characteristics are usually based on clean water flow (Crites and Tchobanoglous, 1998).

TABLE 3 DESIGN CRITERIA FOR MECHANICALLY CLEANED BAR SCREENS

lt a ma	Design Criteria		
Item	Metric Units	English Units	
Bar width	5-15 mm	0.2-0.6 in	
Bar depth	25-40 mm	1.0-1.5 in	
Clear spacing between bars	15-75 mm	0.6-3.0 in	
Slope from vertical	0-30 degrees	0-30 degrees	
Approach velocity	0.6-1.0 m/s	2.0-3.25 ft/s	
Allowable Headloss	150 mm	6 in	

Source: WEF, 1998.

When a comminution device is installed upstream of a grit removal device, the teeth of the comminutor are subject to high wear and tear. Rock traps are recommended to prolong the life of the comminutor. In addition, a bypass manual bar rack should be installed in the event that flow rates exceed the comminutor capacity or there is a mechanical failure.

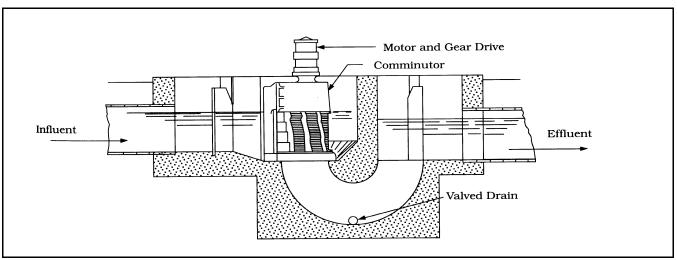
Grit Removal

With respect to grit removal systems, grit is traditionally defined as particles larger than 0.21 mm (0.008 in) (65 mesh) and with a specific gravity of greater than 2.65 (U.S. EPA, 1987). Equipment design was traditionally based on removal of 95 percent of these particles. However, with the recent recognition that smaller particles must be removed to avoid damaging downstream processes, many modern grit removal designs are capable of removing up to 75 percent of 0.15 mm (0.006 in) (100 mesh) material.

Aerated Grit Chamber

Aerated grit chambers are typically designed to remove particles of 70 mesh (0.21 mm/0.008 in) or larger, with a detention period of two to five minutes at peak hourly flow. When wastewater flows into the grit chamber, particles settle to the bottom according to their size, specific gravity, and the velocity of roll in the tank. A velocity that is too high will result in lower grit removal efficiencies, while a velocity that is too low will result in increased removal of organic materials. Proper adjustment of air velocity will result in nearly 100 percent removal of the desired particle size and a well-washed grit.

Design considerations for aerated grit chambers include the following (WEF 1998):



Source: Reynolds/Richards, 1996.

FIGURE 4 TYPICAL COMMINUTOR INSTALLATION

- Air rates typically range from 0.3 to 0.7 m³/m•min (3 to 8 ft³/ft•min) of tank length.
- A typical minimum hydraulic detention time at maximum instantaneous flow is two minutes.
- Typical length-to-width ratio is 2.5:1 to 5:1.
- Tank inlet and outlet are positioned so the flow is perpendicular to the spiral roll pattern.
- Baffles are used to dissipate energy and minimize short circuiting.

Vortex-Type Grit Chamber

Two designs of vortex grit units exist: chambers with flat bottoms and a small opening to collect grit; and chambers with a sloping bottom and a large opening into the grit hopper. Flow into a vortex-type grit system should be straight, smooth, and streamlined. The straight inlet channel length is typically seven times the width of the inlet channel, or 4.6 m (15 ft), whichever is greater. The ideal velocity range in the influent is typically 0.6 to 0.9 m/s (2 to 3 ft/s) at 40 to 80 percent of peak flow. A minimum velocity of 0.15 m/s (0.5 ft/s) should be maintained at all times, because lower velocities will not carry grit into the grit chamber (WEF, 1998).

Detritus Tank

Detritus tanks are designed to keep horizontal velocity and turbulence at a minimum while maintaining a detention time of less than one minute. Proper operation of a detritus tank depends on well-distributed flow into the settling basin. Allowances are made for inlet and outlet turbulence as well as short circuiting by applying a safety factor of 2.0 to the calculated overflow rate.

Horizontal Flow Grit Chamber

Horizontal flow grit chambers use proportional weirs or rectangular control sections to vary the depth of flow and keep the velocity of the flow stream at a constant 0.3 m/s (1 ft/s). The length of the grit chamber is governed by the settling velocity

of the target grit particles and the flow control section-depth relationship. An allowance for inlet and outlet turbulence is added. The cross sectional area of the channel is determined by the rate of flow and the number of channels. Allowances are made for grit storage and grit removal equipment. Table 4 lists design criteria for horizontal flow grit chambers.

TABLE 4 HORIZONTAL FLOW GRIT CHAMBER DESIGN CRITERIA

	Design Criteria		
Item	Range Metric (English)	Typical Metric (English)	
Detention time	45-90 s	60 s	
Horizontal velocity	0.24-0.4 m/s (0.8-1.3 ft/s)	0.3 m/s (1.0 ft/s)	
Settling velocity ¹ :			
50-mesh	2.8-3.1 m/min (9.2-10.2 ft/min)	2.9 m/min (9.6 ft/min)	
100-mesh	0.6-0.9 m/min (2.0-3.0 ft/min)	0.8 m/min (2.5 ft/min)	
Headloss (% of channel depth)	30-40%	36%²	
Inlet and outlet length allowance	25-50%	30%	

¹If the specific gravity of the grit is significantly less than 2.65, lower velocities should be used.

Source: Crites and Tchobanoglous, 1998.

PERFORMANCE

The use of screening and grit removal systems is well documented. The performance of bar screens varies depending on the spacing of the bars. Table 5 lists typical screening quantities for various screen sizes.

The quantity of screenings depends on the length and slope of the collection system and the presence of pumping stations. When the collection system is long and steep or when pumping stations exist, fewer screenings are produced because of disintegration of solids. Other factors that affect screening quantities are related to flow, as quantities generally increase greatly during storm flows. Peak

²For Parshall flume control.

TABLE 5 SCREENING REMOVAL QUANTITIES

Compan Cina	Screenings Quantity		
Screen Size	$m^3/10^6 m^3$	ft³/Mgal	
13 mm (0.5 in)	60	8	
38 mm (1.5 in)	11.2	1.5	

Source: Reynolds and Richards, 1996.

daily removals may vary by a 20:1 ratio on an hourly basis from average flow conditions. Combined collection systems may produce several times the coarse screenings produced by separate collection systems.

Given the complexity of collection systems and types of materials that may be considered "grit," the quantity and characteristics of grit removed from wastewater will vary. Grit quantity is influenced by the type and condition of the collection system, the characteristics of the drainage area, garbage disposal methods, the slope of the collection system, and the efficiency of the grit removal system. The quantity of grit may vary from 0.004 to 0.21 m³/10³m³ (0.5 to 30 ft³/Mgal) (Crites and Tchobanoglous, 1998). The performance of a grit removal system may be enhanced if actual plant data is used when designing a new grit removal system.

Table 6 depicts quantities of screenings and grit from various wastewater treatment plants. There are no obvious trends associated with design flow through a plant and grit and screenings removal quantities. Differences in wastewater characteristics and equipment efficiencies make a correlation between flow and quantities of screenings and grit removed nearly impossible.

OPERATION AND MAINTENANCE

Screening

Manually cleaned screens require frequent raking to prevent clogging. Cleaning frequency depends on the characteristics of the wastewater entering a plant. Some plants have incorporated screening devices, such as basket-type trash racks, that are manually hoisted and cleaned. Mechanically cleaned screens usually require less labor for operation than manually cleaned screens because screenings are raked with a mechanical device rather than by facility personnel. However, the rake teeth on mechanically cleaned screens must be routinely inspected because of their susceptibility to breakage and bending. Drive mechanisms must also be frequently inspected to prevent fouling due to grit and rags. Grit removed from screens must be disposed of regularly.

TABLE 6 GRIT AND SCREENINGS REMOVAL QUANTITIES AT VARIOUS PLANTS

Plant Location	Flow, m³/d (MGD)	Grit, m³/10³m³ (ft³/Mgal)	Screenings, m³/10³m³ (ft³/Mgal)ª
Uniontown, Pennsylvania	11,400 (3.0)	0.074 (10.5)	0.006 (0.9)
East Hartford, Connecticut	15,100 (4.0)	0.017 (2.4)	0.009 (1.33)
Duluth, Minnesota	45,400 (12.0)	0.006 (0.8)	0.004 (0.56)
Lamberts Point Water Pollution Control Plant, Norfolk, Virginia	75,700 (20.0)	0.034 (4.85)	0.009 (1.20)
Village Creek Wastewater Treatment Plant, Ft. Worth, Texas	170,000 (45.0)	0.009 (1.29)	0.005 (0.72)
County of Milwaukee, Wisconsin, South Shore	454,000 (120.0)	0.003 (0.48)	0.004 (0.60)
Twin Cities Metro Wastewater Treatment Plant, Minnesota	825,000 (218.0)	0.034 (4.82)	0.008 (1.15)
Chicago, Illinois (Northside)	1,260,000 (333.0)	0.003 (0.41)	0.006 (0.83)

aft3/Mgal=cubic feet per million gallons

Source: WEF, 1998.

Communitors and Grinders

Comminutors can create operation and maintenance problems in downstream processes. While shredding solids eliminates the problem of handling screening materials at the head of the plant, problems inherent to the use of communitors, such as the decreased quality of digested biosolids and the accumulation of rags on air diffusers, have lessened the popularity of this technology. Comminutors are generally avoided in new designs and are being removed from many existing plants. Grinders are greatly affected by grit and other solids. As such, they require routine inspection every six months and replacement of bearings and cutter teeth every one to three years.

Grit Removal

Collected grit must be removed from the chamber, dewatered, washed, and conveyed to a disposal site. Some smaller plants use manual methods to remove grit, but grit removal is usually accomplished by an automatic method. The four methods of automatic grit removal include inclined screw or tubular conveyors, chain and bucket elevators, clamshell buckets, and pumping. A two-step grit removal method is sometimes used, where grit is conveyed horizontally in a trough or channel to a hopper, where it is then elevated from the hopper to another location.

Aerated grit chambers use a sloped tank bottom in which the air roll pattern sweeps grit along the bottom to the low side of the chamber. A horizontal screw conveyor is typically used to convey settled grit to a hopper at the head of the tank. Another method to remove grit from the chamber floor is a chain and flight mechanism.

Once removed from the chamber, grit is usually washed with a hydrocyclone or grit classifier to ease handling and remove organic material. The grit is then conveyed directly to a truck, dumpster, or storage hopper. From there, the grit is taken to a landfill or other disposal facility.

COSTS

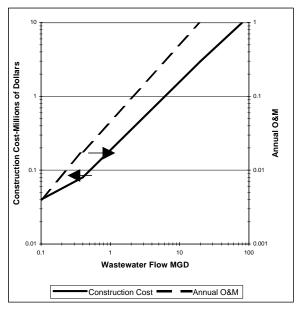
The cost of screens and grit removal systems varies depending on the type of technology used, ancillary

equipment, and applicability of various technologies to different situations.

Graphs can be used to relate average wastewater flow through a plant to a specific technology. Figure 5 shows a graph relating wastewater flow to the cost of a horizontal shaft rotary screen. Costs include construction, operation, and maintenance. Contractor bids on a recent wastewater project ranged from \$150,000 to \$400,000 for Rotary Drum Screenings Removal and from \$150,000 to \$208,800 for Vortex-type Grit Removals. Generally, equipment costs will be close for each bid. However, the overall costs vary for each treatment process/project because of differences in construction approaches by the contractors.

REFERENCES

Other Related Fact Sheets



Source: Martin, 1991.

FIGURE 5 COST CURVE FOR HORIZONTAL SHAFT ROTARY SCREEN

Sewer Lift Station EPA 832-F-00-073 September 2000

Sewer Cleaning & Inspection EPA 832-F-99-031 September 1999 Screens EPA 832-F-99-040 September 1999

Other EPA Fact Sheets can be found at the following web address:

http://www.epa.gov/owm/mtb/mtbfact.htm

- 1. Crites, R. and G. Tchobanoglous, 1998. Small and Decentralized Wastewater Management Systems. The McGraw-Hill Companies. Boston, Massachusetts.
- 2. Martin, E.J. and E.T. Martin, 1991. Technologies for Small Water and Wastewater Systems. Van Nostrand Reinhold. New York, New York.
- 3. Qasim, S., 1994. Wastewater Treatment Plants: Planning, Design and Operation. Technomic Publishing Co., Lancaster, Pennsylvania.
- 4. Reynolds, T. and P. Richards, 1996. *Unit Operations and Processes in Environmental Engineering*. PWS Publishing Company. Boston, Massachusetts.
- 5. Urquhart, L., 1962. *Civil Engineering*. Costs include construction, operation, and maintenance. Specific cost data from contractor bids.
- 6. Water Environment Federation, 1998.

 Design of Municipal Wastewater Treatment
 Plants. Water Environment Federation.
 Alexandria, Virginia.

ADDITIONAL INFORMATION

H.I.L. Technology, Inc. 94 Hutchins Drive Portland, ME 04102

Lakeside Equipment Corporation 1022 E. Devon Ave. Bartlett, IL 60103

National Small Flows Clearing House at West Virginia University P.O. Box 6064 Morgantown, WV 26506

Parkson Corporation 2727 NW 62nd Street P.O. Box 408399 Fort Lauderdale, FL 33340-8399

U.S. Filter Link-Belt Headworks Products 100 High Point Drive - Suite 101 Chalfont, PA 18914

The mention of trade names or commercial products does not constitute endorsement or recommendation for use by the U.S. Environmental Protection Agency (EPA).

Office of Water EPA 832-F-03-011 June 2003

For more information contact:

Municipal Technology Branch U.S. EPA Mail Code 4204 1200 Pennsylvania Avenue, NW Washington, D.C. 20460





CHAPTER 4

Preliminary and Pretreatment Facilities

4.1 Screening and Grinding

- 4.1.1 General
- 4.1.2 Location
- 4.1.3 Bar Screens
- 4.1.4 Fine Screens
- 4.1.5 Communition
- 4.1.6 Operability
- 4.1.7 Disposal

4.2 <u>Grit Removal</u>

- 4.2.1 General
- 4.2.2 Location
- 4.2.3 Design
- 4.2.4 Disposal
- 4.2.5 Operability

4.3 <u>Pre-aeration</u>

4.4 Flow Equalization

- 4.4.1 General
- 4.4.2 Location
- 4.4.3 Design and Operability

4.5 Swirls and Helical Bends

PRELIMINARY AND PRETREATMENT FACILITIES

4.1 Screening and Grinding

4.1.1 General

Some type of screening and/or grinding device shall be provided at all mechanical wastewater plants. The effective removal of grit, rocks, debris, excessive oil or grease and the screening of solids shall be accomplished prior to any activated sludge process. Any grinding which does not dispose of the shredded material outside of the wastewater stream must be evaluated with regard to the influent characteristics (rags, combined sewers) of the waste prior to any activated sludge process.

4.1.2 Location

4.1.2.1 Indoors

Screening devices installed in a building where other equipment or offices are located shall be accessible only through an outside entrance. Adequate lighting, ventilation and access for maintenance or removal of equipment and screenings shall be provided.

4.1.2.2 Outdoors

The removal point for screenings should be as practical as possible for the plant personnel, preferably at ground level. Ladder access is not acceptable unless hoisting facilities for screenings are provided. Separate hoisting is not required for bar screens in manual bypass channels.

4.1.2.3 Deep Pit Installations

Stairway access, adequate lighting and ventilation with a convenient and adequate means for screenings removal shall be provided.

4.1.3 Bar Screens

4.1.3.1 Manually Cleaned

Clear openings between bars shall be from 1 to 2 inches. Slope of the bars shall be 30 to 60 degrees from the vertical. Bar size shall be from 1/4 to 5/8 inches with 1 to 3 inches of depth, depending on the length and material to maintain integrity. A perforated drain plate shall be installed at the top of the bar screen for temporary storage and drainage.

4.1.3.2 Mechanically Cleaned

Mechanically cleaned bar screens are recommended for all plants greater than 1 MGD. Both front cleaned or back cleaned models may be acceptable. Clear openings no less than 5/8 inch are acceptable. Protection from freezing conditions should be considered.

Other than the rakes, no moving parts shall be below the water line.

4.1.3.3 Velocities

Approach velocities no less than 1.25 fps nor a velocity greater than 3.0 fps through the bar screen is desired.

4.1.4 Fine Screens

4.1.4.1 General

Fine screens shall be preceded by a trash rack or coarse bar screen. Comminution shall not be used ahead of fine screens. A minimum of two fine screens shall be provided, each capable of independent operation at peak design flow. The design engineer must fully evaluate a proposal where fine screens are to be used in lieu of primary sedimentation. Fine screens shall not be considered equivalent to primary sedimentation or grit removal, but will be reviewed on a case-by-case basis. Oil and grease removal must be considered.

4.1.4.2 Design

The operation should be designed to not splash operating personnel with wastewater or screenings. Fine screens will generally increase the dissolved oxygen content of the influent which may be beneficial in certain circumstances. The screens must be enclosed or otherwise protected from cold weather freezing conditions. Disposal of screenings must be addressed. To be landfilled, screenings must be dried to approximately 20% solids. Odors may be a problem in sensitive locations.

4.1.5 Comminution

4.1.5.1 General

In-line comminution may not be acceptable prior to an activated sludge process for facilities with a history of problems with rags. Out-of-stream comminution or disintegration is acceptable for activated sludge processes; however, screenings should not return to the wastewater stream.

January 2016 4-3 Design Criteria Ch. 4

4.1.5.2 Design

A coarse bar screen with an automatic bypass shall precede comminution for all mechanical plants. Gravel traps shall precede comminution which is not preceded by grit removal. Clear openings of 1/4 inch are prefered in the comminution device. An automatic unit bypass or other means of protection shall be provided to protect the comminutor motor from flooding. The design shall incorporate a method for removing the equipment from service and for repairs or sharpening of the teeth.

4.1.6 Operability

All screening devices shall have the capability of isolation from the wastewater stream. Sufficient wash water shall be available for cleanup of the area. All mechanical screening devices shall be provided with a manually cleaned bar screen bypass. Multiple bar screens should be considered for plants with rag problems instead of comminutors.

Adequate space must be provided for access to each screening or comminution device. This is critical in elevated, indoor or deep pit installations.

4.1.7 Disposal

All screenings shall be disposed of in an approved manner. Suitable containers shall be provided for holding the screenings. Run-off control must be provided around the containers, where applicable. If fine screens are proposed, consideration must be given to the wastewater overflow if the screens clog or blind. Overflows must be contained and bypassed around the screens by dikes or other means.

4.2 Grit Removal

4.2.1 General

Grit removal is recommended for all mechanical wastewater plants and is required in duplicate for plants receiving wastewater from combined sewers. Systems with a history of substantial grit accumulations may be required to provide for grit removal. Where a system is designed without grit removal facilities, the design shall allow for future installation by providing adequate head and area. Grit washing may be required.

4.2.2 Location

Wherever circumstances permit, grit removal shall be located prior to pumps and comminution when so equiped. Bar screens shall be prior to grit removal. Adequate lighting, ventilation and access for maintenance and removal of grit shall be provided. Stairway access is required if the chamber is above or below ground level. Adequate and convenient means of grit removal shall be provided.

4.2.3 Design

4.2.3.1 Channel Type

A controlled velocity of one foot per second is recommended. Control by either sutro or proportional weir should be used. If a Parshall flume is used for control, the grit chamber must be designed to approach a parabolic cross-section. The length of the channel depends on the size of grit to be removed. The design engineer shall provide this information. Inlet and outlet turbulence must be minimized.

4.2.3.2 Square Type

Square-type basins or similar arrangements should be sized for an overflow rate of 46,300 (WPCF) gallons per day per square foot at the peak flow based on 65-mesh grit at a specific gravity of 2.65. Other overflow rates may be used when the design incorporates particle travel distance and detention. Inlet and outlet turbulence must be minimized.

4.2.3.3 Aerated Type

Aerated grit chambers shall be designed on the basis of detention and/or particle travel distance. Detention time of 2-5 minutes at peak flow is acceptable. Control of the air shall be provided for flexibility. Skimming equipment must be provided in the aerated grit chamber if the outlet is below the water surface.

4.2.3.4 Other Types

Cyclone or swirl-type grit removal processes may be acceptable. The design engineer will be expected to provide a complete treatment analysis for approval.

4.2.4 Disposal

Temporary storage containers shall be provided to hold the grit. Run-off control shall be provided. Attention should be given to operations which may splash waste or grit on operating personnel. Grit washing is required before removal to drying beds. If not washed, the grit shall be disposed of in an approved landfill.

January 2016 4-5 Design Criteria Ch. 4

4.2.5 Operability

Adjustable control valves shall be included in each diffuser air line to control mixing and particle segregation. Variable speed arrangements should be provided in cyclone or mechanical type systems. Provisions shall be made for isolation and dewatering each unit or units.

4.3 Pre-Aeration

Pre-aeration is desirable in certain instances, such as to reduce septicity. Pre-aeration may be required where pressure or small diameter collection systems are used. Long detention times in pump stations or collection lines should also be considered. Units shall be designed so that removal from service will not interfere with normal plant operations.

4.4 Flow Equalization

4.4.1 General

Equalization may be used to minimize random or cyclic peaking of organic or hydraulic loadings when the total flow is ultimately processed through the plant. Either in-line or side-line equalization is acceptable. Equalization may be required where peak flows are greater than 2 times the average design flow.

4.4.2 Location

Tanks are generally located after screening and grit removal. Care should be taken in design to minimize solids deposition if located upstream of primary clarifiers. Equalization downstream of primary clarifiers should be investigated, as primary clarifier performance is less sensitive to flow peaking when compared to other processes. Other locations will be evaluated on a case-by-case basis.

4.4.3 Design and Operability

Generally, aeration will be required. Minimum requirements are to maintain 1.0 mg/l of dissolved oxygen. Odor consideration must be addressed when a plant is located in a sensitive area or large equalization basins are used. Large tanks must be divided into compartments to allow for operational flexibility, repair and cleaning. Each compartment shall be capable of dewatering and access. In plant upgrades, existing units which are otherwise to be abandoned may be used for equalization, where possible. Sizing the tankage and compartments will depend on the intended use; i.e., when equalization is for periodic high organic loadings, peak flow events, toxics, etc. A complete analysis shall accompany all engineering report (or plan) submission.

The tank must be capable of being drained and isolated. Controlling the flow rate from the equalization tank to the plant is desirable.

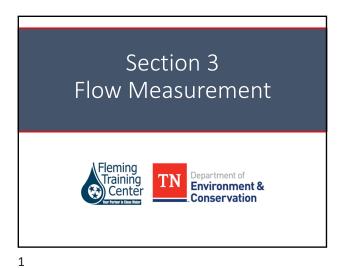
4.5 Swirls and Helical Bends

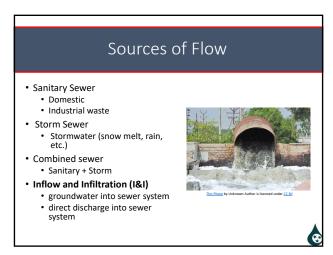
These units are not to be used in lieu of primary clarification unless special design considerations are used. They are primarily designed for 'coarse' floating and settleable solids removal and will be considered only on a case-by-case basis for in-plant processes. They will, however, be approved for replacing regulators in combined sewer systems, as an interim measure until separation of the sanitary and storm flows is completed. Treatability studies will be required as part of the design. A separate NPDES permit will be required for each of these units that will discharge to a surface water.

Section 3 Flow Measurement

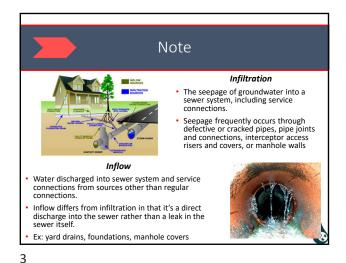




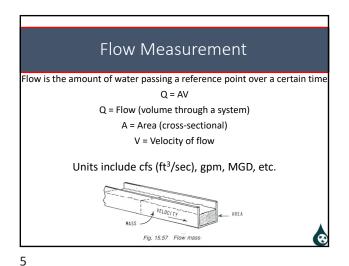


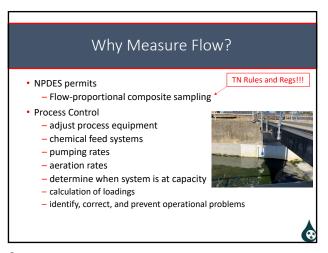


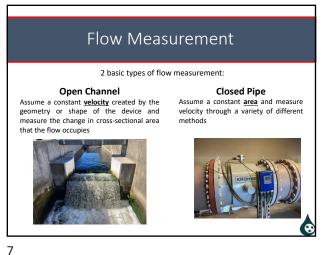
2



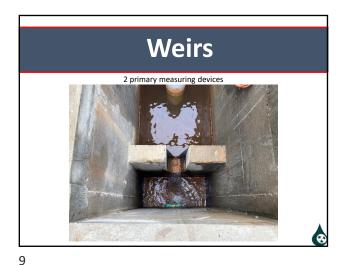
4





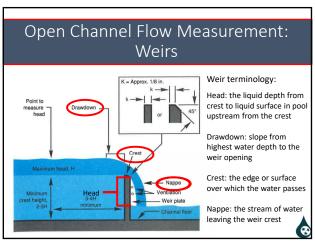


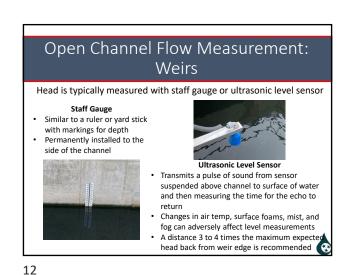
Open Channel Flow Measurement 2 primary measuring devices Flumes Weirs Specially shaped open channel flow Obstruction that stretches section that restricts the channel area across the entire channel and/or changes the slope, resulting in an increased velocity and a change in the level of liquid flowing through the flume

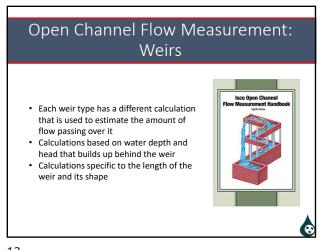


Open Channel Flow Measurement: Weirs 4 most common types: Rectangular Weir with end constrictions Triangular (V-notch) Weirs Trapezoidal (Cipolletti) Wei Rectangular Weir without end constrictions

10







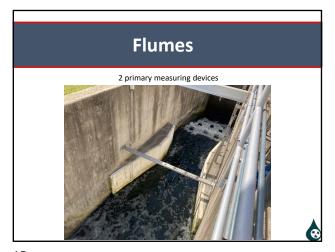
Open Channel Flow Measurement: Weirs



- Inexpensive to install and low cost compared to other flow measurement
- Can trap foam and solids behind weir
- Must be cleaned periodically
- Unsuitable for channels carrying large quantities of debris – good for final effluent

13

14



Open Channel Flow Measurement: Flumes

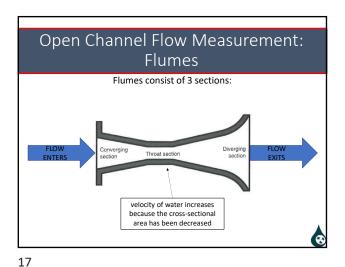
Specially shaped open channel flow section that restricts the channel area and/or changes the slope, resulting in an increased velocity and a change in the level of liquid flowing through the flume.

 Constriction causes a change in head which can be converted to flow rates

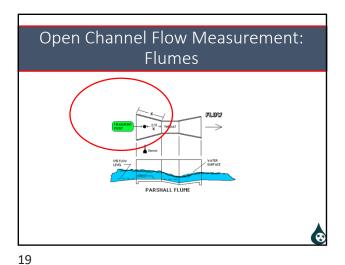


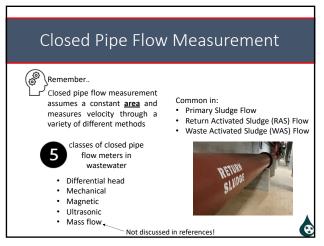
15

16



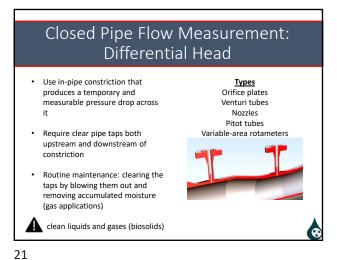
Open Channel Flow Measurement: **Flumes** 3 most common types: Palmer-Bowlus Flume Trapezoidal Flume Originally designed Work well for Parshall Flume for measuring flows measuring flows Most widely used in existing pipes and over a wide range Available in a Well suited for channels variety of sized Widely used for extremely low to accommodate measuring flows in most flowrates manholes



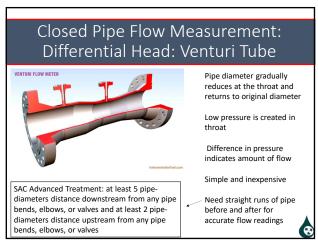


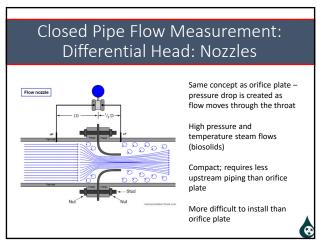
20

22



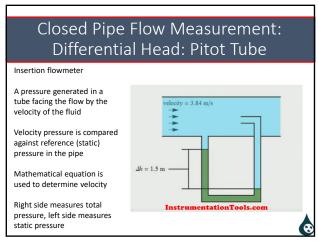
Closed Pipe Flow Measurement: Differential Head: Orifice Plate Thin metal plate with a hole bored through the middle The upstream side has a sharp edge that creates a pressure drop as the flow moves through the hole Work well for large pipe diameters, have no moving parts, and are relatively low Can not be used for with dirty liquids because solids will erode the metal and change

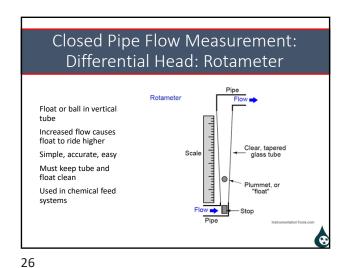


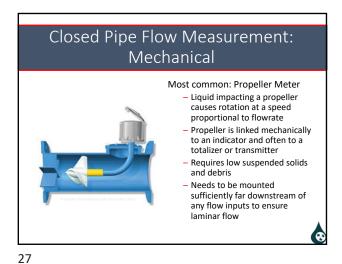


23

25







Closed Pipe Flow Measurement:

Electromagnetic

"Magnetic Flow Meter"

Application range from filtered effluent to thickened or digested solids

Creates magnetic field in water stream

Conductor (water) moving through magnetic field produces electric current

Measure of electricity indicates amount of flow

Require full pipe

Very accurate, low maintenance

Expensive

Closed Pipe Flow Ultrase	
Measurement of ultrasonic wave-transit time or frequency shift caused by the flowing fluid Ultrasonic waves of known frequency and duration are beamed across the pipe at known angles Waves are sensed either: directly by an opposing receiver indirectly as reflected waves The changes in wave transit time or frequency are linearly proportional to the liquid velocity = math Presence or absence of air bubbles and density of solids affect metering	"clamp on" "bownstream transducer Talene Spacing Upstream transducer

	Accuracy	Advantages	Disadvantages
Open- Channel Flume	5-7%	Low headloss, self-cleaning	Requires careful construction, susceptible to flooding
Open- Channel Weir	5-7%	Low cost, ease of installation	High headloss, requires a well- developed flow profile, cleaning required
Full-Pipe Electro- magnetic	1-3%	No headloss, bi-directional	Minimum conductivity required, expensive, well-developed velocity profile required
Full-Pipe Doppler	2-5%	No headloss, low cost, not affected by air bubbles	Not suitable for some pipe material, well-developed velocity profile required
Full-Pipe Venturi	1-3%	Low headloss, high accuracy	Expensive, well-developed velocity profile required

29 30

57

Primary vs. Secondary Flow Measurement

Primary Flow Metering (1°)
• Used for measuring and reporting

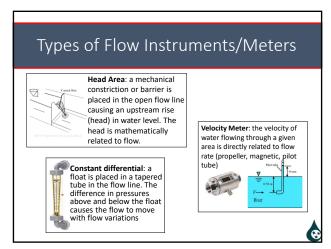
- flows for permit compliance
 Influent or effluent
- "Instantaneous flow" measurements can be obtained from primary flow device
- · Ex: weirs, flume

All flow measurement devices should be calibrated and maintained to ensure the accuracy of the measurement is ± 10% of the true flow.

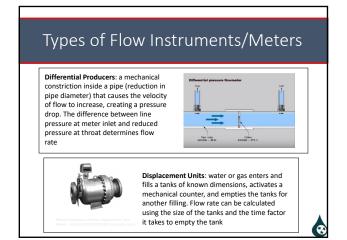
- Secondary Flow Metering (2°)
- Required for process control but not NPDES Permit
- Completed within treatment plant
- Return Activated Sludge (RAS)Wasted Activated Sludge (WAS)
- Side stream flows (digesters, centrifuges, solid filter presses)
- Measures hydraulic responses of the primary flow measurement device
- Ex: float, ultrasonic meter, staff gauge



31



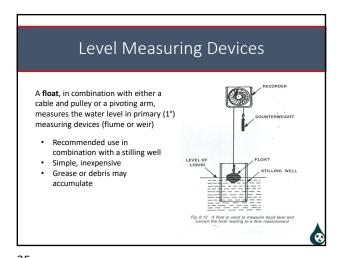
32

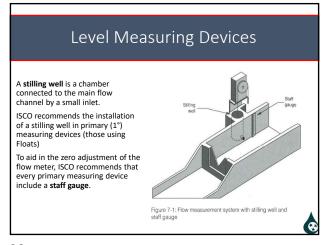


Constant differential Liquids and gases Rotameters (Ex: Chlorination) Liquids - Partially filled Head area Weirs channels, basins, clarifiers Flumes Liquids – Partially filled pipes and channels Velocity meters Propeller Liquids – channel flow, clean water piped flow Magnetic Liquids and sludge in closed pipes Differential producers Venturi tube Gases and liquids in closed Flow nozzle Orifice Displacement units Piston Diaphragm Gases and liquids in closed *See Table 15.10 in Operation of Wastewater Treatment Plants, Vol II for complete table

33

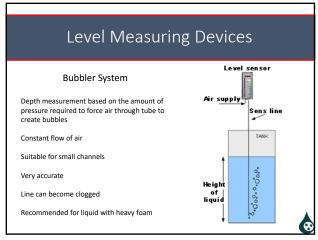
34

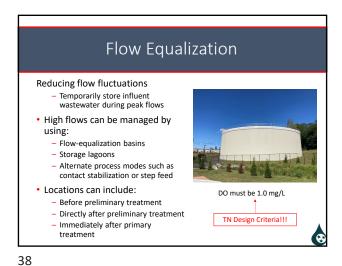


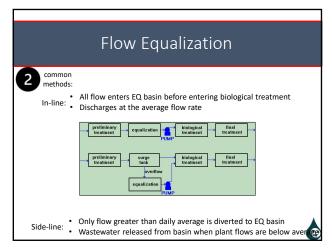


36

37









39

Flow Vocabulary

1.	The amount of water passing a reference point over a certain amount of time is
2.	An is any channel in which the liquid flows with a free or uncovered surface.
3.	An obstruction or dam built across an open channel over which the water flows, often through a specially shaped opening or notch is called a
4.	A is a specially shaped open channel flow section that restricts the channel area and/or changes the slope, resulting in an increased velocity and a change in the level of liquid flowing through it.
5.	Theflume is most commonly used to retrofit manholes.
6.	Theof a flume restricts flow. Velocity is increasing in this area.
7.	The is the section of a flume that creates a hydraulic jump transition from higher velocity to slower velocity. It produces a head that is related to the discharge.
8.	A is any channel in which flow is in a completely filled pressure conduit (a.k.a. pipes). This includes sewer lines running full or force mains.
9.	Weirs, flumes, and nozzles are all examples of measuring devices.
10.	The section of the flume is where water returns to original shape of channel, it assures the downstream level is less than the level in the converging section.
11.	This type of flume is best for wastewater containing solids and debris.
12.	is an indirect measure of loss of energy or pressure. Flowing water will lose some of its energy when it passes through a pipe, bar screen, Comminutor, filter or other obstruction. This is measured as the difference in elevation between the upstream water surface and the downstream water surface and may be expressed in feet or meters.
13.	Open channel flow meters, such as floats, ultrasonic meters, and bubbler systems, are all examples of measuring devices.
14.	Adequate aeration and mixing must be provided in thebasin to keep the basins aerobic and prevent solids deposition. A DO of 1.0 mg/L must be maintained throughout.

Word Bank Flow Diverging Palmer-Bowlus Flume Headloss Parshall Primary (1°) Weir Throat Flow equalization Open channel Closed channel Converging section

Secondary (2°)

CHAPTER 13

Plant Flow Measurement and Sampling

13.1 Purpose

13.2 Flow Measurement

- 13.2.1 General Considerations
- 13.2.2 Parshall Flumes
- 13.2.3 Sharp Crested Weirs
- 13.2.4 Venturi and Modified Flow Tube Meters
- 13.2.5 Other Flow Metering Devices
- 13.2.6 Hydrograph Controlled Release (HCR) Systems

13.3 <u>Sampling</u>

- 13.3.1 Automatic Sampling Equipment
- 13.3.2 Manual Sampling
- 13.3.3 Long Outfall Lines
- 13.3.4 Sampling Schedules

PLANT FLOW MEASUREMENT AND SAMPLING

13.1 Purpose

Complete and accurate flow measuring and sampling are essential in the proper treatment of wastewater. Compliance with discharge limits requires proper flow measurement and sampling. They provide the operator with the information to optimize process control and operational costs, as well as providing an accurate data base of flows and process performance which can be used to analyze changes in operational strategy or assist future plant design.

13.2 Flow Measurement

13.2.1 General Considerations

- 13.2.1.1 Facilities for measuring the volume of sewage flows should be provided at all treatment works.
- 13.2.1.2 Plants with a capacity equal to or less than 100,000 gallons per day (gpd) shall be equipped, as a minimum, with a primary metering device such as: a Parshall flume having a separate float well and staff gauge, a weir box having plate and staff gauge, or other approved devices. Continuous recording devices may be required where circumstances warrant.
- 13.2.1.3 Plants having a capacity of greater than 100,000 gpd shall be provided with indicating, recording, and totalizing equipment using strip or circular charts and with flow charts for periods of 1 or 7 days. The chart size shall be sufficient to accurately record and depict the flow measured.
- 13.2.1.4 Flows passed through the plant and flows bypassed shall be measured in a manner which will allow them to be distinguished and separately reported.
- 13.2.1.5 Measuring equipment shall be provided which is accurate under all expected flow conditions (minimum initial flow and maximum design peak flow). The accuracy of the total flow monitoring system (primary device, transmitter, and indicator) must be acceptable. The effect of such factors as ambient temperature, power source voltage, electronic interference, and humidity should be considered. Surges must be eliminated to provide accurate measurement.

Two primary devices and flow charts may be required in some cases.

- 13.2.1.6 Metering devices within a sewage works shall be located so that recycle flow streams do not inadvertently affect the flow measurement. In some cases, measurement of the total flow (influent plus recycle) may be desirable.
- 13.2.1.7 All clarifiers must be provided with a means for accurate flow measurement of sludge wasting and sludge return lines so that solids handling can be controlled. Sludge digesters, thickeners, and holding tanks should be provided with some way to determine the volume of sludge added or removed. This can be accomplished by a sidewall depth scale or graduation in batch operations.
- 13.2.1.8 Flow meter and indicator selection should be justified considering factors such as probable flow range, acceptable headloss, required accuracy, and fouling ability of the water to be measured. For more detailed information the consultant is encouraged to read the EPA Design Information Report "Flow Measurement Instrumentation"; Journal WPCF, Volume 58, Number 10, pp. 1005-1009. This report offers many installation details and considerations for different types of flow monitoring equipment.
- 13.2.1.9 Flow splitter boxes shall be constructed so that they are reliable, easily controllable, and accessible for maintenance purposes.
- 13.2.1.10 Where influent and effluent flow-proportional composite sampling is required, separate influent and effluent flow measuring equipment is required.
- 13.2.1.11 Consideration should be given to providing some types of flow meters with bypass piping and valving for cleaning and maintenance purposes.

13.2.2 Parshall Flumes

Parshall Flumes are ideal for measuring flows of raw sewage and primary effluents because clogging problems are usually minimal.

The properly sized flume should be selected for the flow range to be encountered. All Parshall Flumes must be designed to the specified dimensions of an acceptable reference.

The following requirements must be met when designing a Parshall Flume.

- 13.2.2.1 Flow should be evenly distributed across the width of the channel.
- 13.2.2.2 The crest must have a smooth, definite edge. If a liner is used, all screws and bolts should be countersunk.

- 13.2.2.3 Longitudinal and lateral axes of the crest floor must be level.
- 13.2.2.4 The location of the head measuring points (stilling well) must be two-thirds the length of the converging sidewall upstream from the crest. Sonar-type devices are only acceptable when foaming or turbulance is not a problem.
- 13.2.2.5 The pressure tap to the stilling well must be at right angles to the wall of the converging section.
- 13.2.2.6 The invert (i.e., inside bottom) of the pressure tap must be at the same elevation as the crest.
- 13.2.2.7 The tap should be flush with the flume side wall and have square, sharp corners free from burrs or other projections.
- 13.2.2.8 The tap pipe should be 2 inches in size and be horizontal or slope downward to the stilling well.
- 13.2.2.9 Free-flow conditions shall be maintained under all flow rates to be encountered by providing low enough elevations downstream of the flume. No constrictions (i.e., sharp bends or decrease in pipe size) should be placed after the flume as this might cause submergence under high flow conditions.
- 13.2.2.10 The volume of the stilling well should be determined by the conditions of flow. For flows that vary rapidly, the volume should be small so that the instrument float can respond quickly to the changes in rate. For relatively steady flows, a large-volume stilling well is acceptable. Consideration should be given to protecting the stilling well from freezing.
- 13.2.2.11 Drain and shut-off valves shall be provided to empty and clean the stilling well.
- 13.2.2.12 Means shall be provided for accurately maintaining a level in the stilling well at the same elevation as the crest in the flume, to permit adjusting the instrument to zero flow conditions.
- 13.2.2.13 The flume must be located where a uniform channel width is maintained ahead of the flume for a distance equal to or greater than fifteen (15) channel widths.

 The approach channel must be straight and the approaching flow must

The approach channel must be straight and the approaching flow must not be turbulent, surging, or unbalanced. Flow -lines should be essentially parallel to the centerline of the flume.

13.2.3 Sharp Crested Weirs

The following criteria are for V-notch weirs, rectangular weirs with and without end contractions, and Cipolletti weirs. The following details must be met when designing a sharp crested weir:

- 13.2.3.1 The weir must be installed so that it is perpendicular to the axis of flow. The upstream face of the bulkhead must be smooth.
- 13.2.3.2 The thickness of the weir crest should be less than 0.1 inch or the downstream edge of the crest must be relieved by chamfering at a 45° angle so that the horizontal (unchamfered) thickness of the weir is less than 0.1 inch.
- 13.2.3.3 The sides of rectangular contracted weirs must be truly vertical. Angles of V-notch weirs must be cut precisely. All corners must be machined or filed perpendicular to the upstream face so that the weir will be free of burrs or scratches.
- 13.2.3.4 The distance from the weir crest to the bottom of the approach channel must be greater than twice the maximum weir head and is never to be less than one foot.
- 13.2.3.5 The distance from the sides of the weir to the side of the approach channel must be greater than twice the maximum weir head and is never to be less than one foot (except for rectangular weirs without end contractions.
- 13.2.3.6 The nappe (overflow sheet) must touch only the upstream edges of the weir crest or notch. If properly designed, air should circulate freely under and on both sides of the nappe. For suppressed rectangular weirs (i.e., no contractions), the enclosed space under the nappe must be adequately ventilated to maintain accurate head and discharge relationships.
- 13.2.3.7 The measurement of head on the weir must be taken at a point at least four (4) times the maximum head on the crest upstream from the weir.
- 13.2.3.8 The cross sectional area of the approach channel must be at least eight (8) times that of the nappe at the crest for a distance upstream of 15-20 times the maximum head on the crest in order to minimize the approach velocity.

The approach channel must be straight and uniform upstream of the weir for the same distance, with the exception of weirs with end contractions where a uniform cross section is not needed.

- 13.2.3.9 The head on the weir must have at least three (3) inches of free fall at the maximum downstream water surface to ensure free fall and aeration of the nappe.
- 13.2.3.10 All of the flow must pass over the weir and no leakage at the weir plate edges or bottom is permissable.
- 13.2.3.11 The weir plate is to be constructed of a material equal to or more resistant than 304 Stainless Steel.

13.2.4 Venturi and Modified Flow Tube Meters

The following requirements should be observed for application of venturi meters:

- 13.2.4.1 The range of flows, hydraulic gradient, and space available for installation must be suitable for a venturi meter and are very important in selecting the mode of transmission to the indicator, recorder, or totalizer.
- 13.2.4.2 Venturi meters shall not be used where the range of flows is too great or where the liquid may not be under a positive head at all times.
- 13.2.4.3 Cleanouts or handholes are desirable, particularly on units handling raw sewage or sludge.
- 13.2.4.4 Units used to measure air delivered by positive displacement blowers should be located as far as possible from the blowers, or means should be provided to dampen blower pulsations.
- 13.2.4.5 The velocity and direction of the flow in the pipe ahead of the meter can have a detrimental effect on accuracy. There should be no bends or other fittings for 6 pipe diameters upstream of the venturi meter, unless treated effluent is being measured when straightening vanes are provided.
- 13.2.4.6 Other design guidelines as provided by manufacturers of venturi meters should also be considered.

13.2.5 Other Flow Metering Devices

Flow meters, such as propeller meters, magnetic flow meters, orifice meters, pitot tubes, and other devices, should only be used in applications in accordance with the manufacturer's recommendations and design guidelines.

13.2.6 Hydrograph Controlled Release (HCR) Systems

For plants utilizing HCR systems, accurate stream flow measurements are required. Detailed plans must be submitted outlining the construction of the primary stream flow measuring device and the associated instrumentation. The following factors should be emphasized in the design.

- 13.2.6.1 Accuracy over the flow range required for effluent discharge limiting purposes.
- 13.2.6.2 Operational factors such as cleaning and maintenance requirements.

13.2.6.3 Cost

The use of sharp crested weirs as described in Section 13.2.3 will not be allowed due to the installation requirements such as approach channel details and upstream pool depth and since entrapment and accumulation of silt and debris may cause the device to measure inaccurately. Parshall Flumes may be used due to their self-cleaning ability but field calibration will be required. Self-cleaning V-notch weirs are recommended due to their accuracy in low flow ranges. The weir can be made self-cleaning by sloping both sides of the weir away from the crest. The top portion of the crest shall be covered with angle-iron to prevent its breakdown. The angle of the V-notch should be determined by the stream characteristics; however, a smaller angle will increase accuracy in the low flow range. The primary device shall be built with sufficient depth into the stream bed to prevent undercutting and sufficient height to cover the required flow range.

It is recommended that the wastewater system director, engineer, or other city official contact the U.S. Geological Survey (USGS), Water Resources Division, in Nashville, Tennessee, for assistance with the design and installation of the flow measuring device. They offer a program which shares much of the costs for designing and maintaining the device. After visiting the site, they can assist with the design of a self-cleaning weir for the stream. They provide the consultant with a field design that shows the proper location and installation of the weir. From this field design, the consultant must provide detailed plans to the State.

The wastewater system is responsible for constructing the weir at their own cost. The flow measuring station is installed, maintained, and calibrated by USGS personnel so that accurate results are insured.

The primary device will record continuous flow of the stream and can be designed to send a feedback signal to the WWTP for other purposes such as controlling plant discharge rates.

This program benefits both the local wastewater system, the State of Tennessee, and the USGS, as it adds to stream flow data bases archived for public use. Cost sharing allows the flow measuring station to be built and operated at a lower cost for all parties concerned.

13.3 Sampling

13.3.1 Automatic Sampling Equipment

The following general guidelines should be adhered to in the use of automatic samplers:

- 13.3.1.1 Automatic samplers shall be used where composite sampling is necessary.
- 13.3.1.2 The sampling device shall be located near the source being sampled, to prevent sample degradation in the line.
- 13.3.1.3 Long sampling transmission lines should be avoided.
- 13.3.1.4 If sampling transmission lines are used, they shall be large enough to prevent plugging, yet have velocities sufficient to prevent sedimentation. Provisions shall be included to make sample lines cleanable. Minimum velocities in sample lines shall be 3 feet per second under all operating conditions.
- 13.3.1.5 Samples shall be refrigerated unless the samples will not be effected by biological degradation.
- 13.3.1.6 Sampler inlet lines shall be located where the flow stream is well mixed and representative of the total flow.
- 13.3.1.7 Influent automatic samplers should draw a sample downstream of bar screens or comminutors. They should be located before any return sludge lines or scum lines.
- 13.3.1.8 Effluent sampling should draw a sample immediately upstream of the chlorination point. This will eliminate the need to dechlorinate and then re-seed the sample.

13.3.2 Manual Sampling

Because grab samples are manually obtained, safe access to sampling sites should be considered in the design of treatment facilities.

13.3.3 Long Outfall Lines

Many wastewater systems are constructing long outfall lines to take advantage of secondary or equivalent permit limits.

Due to possible changes in effluent quality between the treatment facility and the outfall, a remote sampling station will be required at or near the confluence of the outfall line and the receiving stream on all outfall lines greater than one mile in length.

Dissolved oxygen, fecal coliform, and chlorine residual may have to be measured at the remote sampling station for permit compliance purposes.

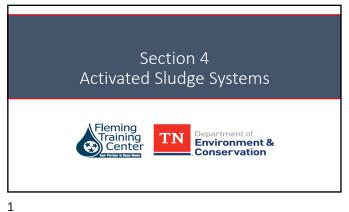
13.3.4 Sampling Schedules

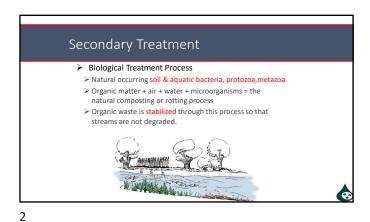
Samples must be taken and analyzed for two purposes: permit compliance and process control. Any time a new permit is issued, a sampling schedule for permit compliance will be determined by the Division of Water Pollution Control. An additional sampling program needs to be set up for process control purposes. This would include all testing required for completing the monthly operational report, as well as any other tests that might aid the operation of the plant. This schedule can be determined by the Division of Water Pollution Control, Wastewater Treatment Section or the appropriate field office once final plans are approved. The designer shall provide safe access points to collect representative influent and effluent samples of all treatment units and to collect samples of all sludge transmission lines. This makes it possible to determine the efficiency of each treatment process. Additional information about methods of analyses can be obtained from the Federal Register 40 CFR Part 136. Information about sampling locations and techniques can be obtained from the EPA Aerobic Biological Wastewater Treatment Facilities Process Control Manual and EPA's NPDES Compliance Inspection Manual.

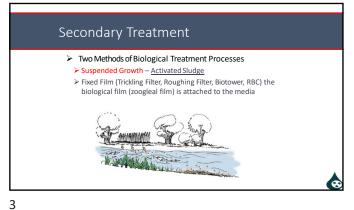
Section 4 Activated Sludge Systems







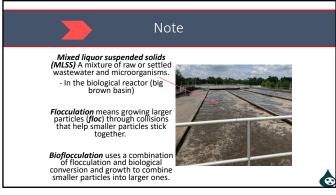




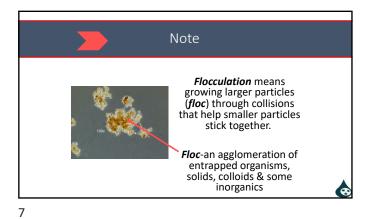
Note Activated sludge is a suspended growth treatment process because the microorganisms are not attached to a surface.

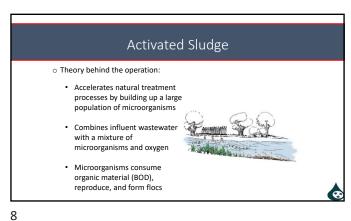
4

Activated Sludge o Most widely used biological treatment process o Wastewater is food for the mixed liquor suspended solids (MLSS), a mixture of bacteria and other microorganisms. $\circ\,$ Bacteria form $\mbox{{\bf flocs}}$ that are kept suspended in the basin by mixing and aeration. o Bioflocculation increases the size and density of particles that don't settle quickly on their own, including: Smaller particles o Soluble, biodegradable organic material



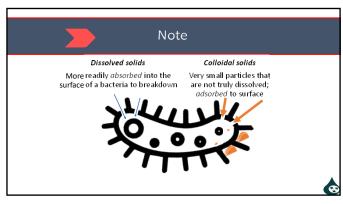
6





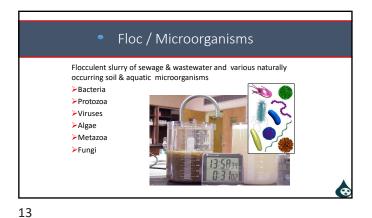
Activated Sludge Function is to remove...

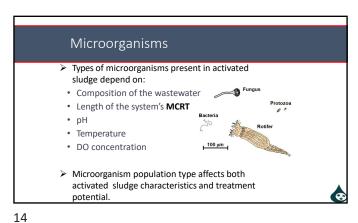
1. Soluble (*dissolved*) pollutants 2. Colloidal solids ...To produce a clear effluent that meets regulatory limits Limits can be in pounds (lbs), concentration (mg/L), or percent removals.



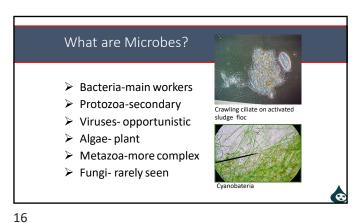




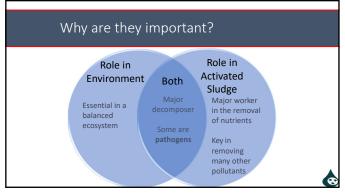


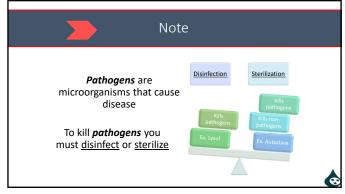


Mean Cell Residence Time (MCRT) is the measure of the average time a microorganism will be in the system.

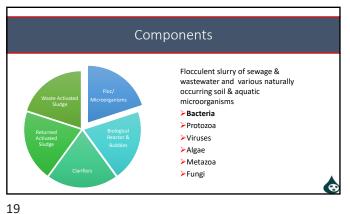


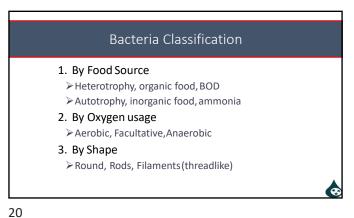
15 1

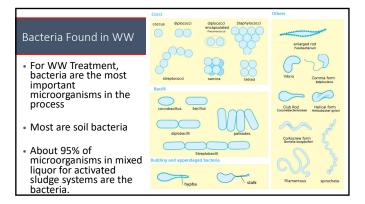




17 18

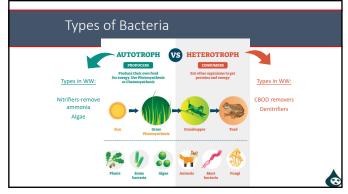






Bacteria · Binary fission is the process by which one mature cell divides into two new cells. · Generation Time: replication in 1 PURE culture: • Bacillus sp. (BOD eating bacteria) 20-30 minutes · Nitrifiers 22-48 hours • Methanogens 10-30 days

22 21



Heterotrophs Consume organic Carbon as a food source • EX. Most wastewater bacteria, Protozoa Humans · Organic food source · Carbohydrates- sugar, starch, cellulose Protein · Other organisms • All animals are heterotrophs, as are most microorganisms (the major exceptions being microscopic algae and blue green bacteria)

Require Nutrients Ex. Nitrogen, Phosphorus, micronutrients Source is the Sewage and wastewater Ideal Balance: BOD (mg/L):TKN (mg/L):P (mg/L) 100:5:1 Sometimes 100:5:1:0.5 (Fe-Iron) Domestic waste generally provides a good balance for the microorganisms, industrial waste

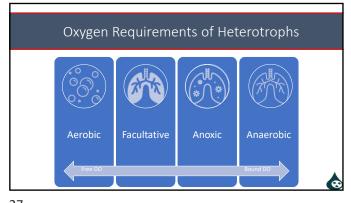
NOTE

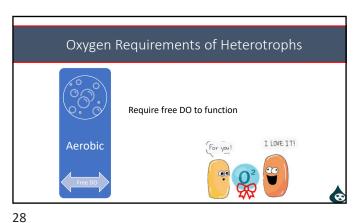
**TKN* is Total Kjeldahl Nitrogen

**TKN = Organic Nitrogen + Ammonia Nitrogen

25 26

may not, which could lead to filament growth.

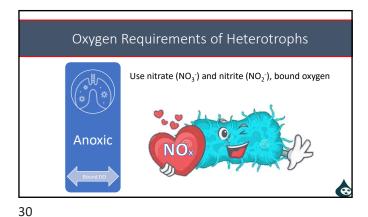


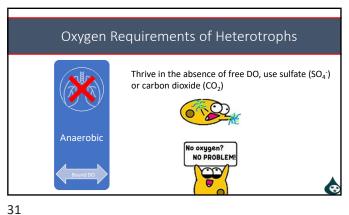


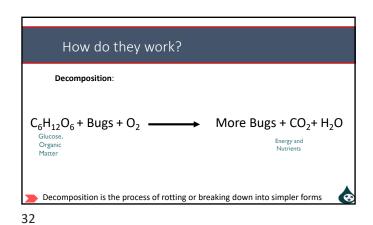
27 2

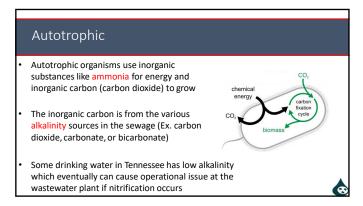


29



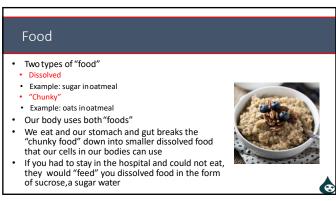


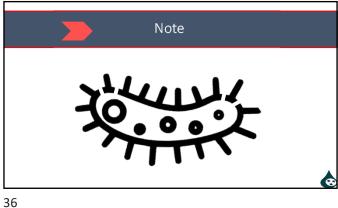




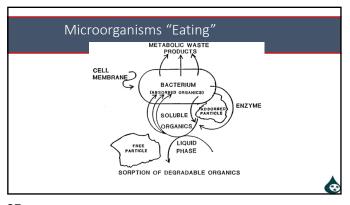
How do they work? ▶ What is the formula backwards? CO_2+H_2O+ energy \leftarrow Photosynthesis!

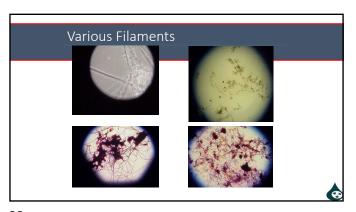
33

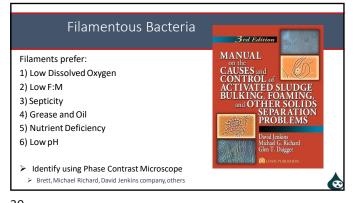




35







Nocardia

Nocardia

Nocardia

Nocardia

Nocardia

Maintaining an MCRT <1 day in warm weather

Works with pure oxygen systems

Can be very difficult in nitrifying plants

Physical removal and disposal by skimming and disposal

Spray with chlorine − on the surface or inject into RAS

Also Cationic polymers- forces the nocardia into the MLSS where is does not prefer to live

39 40

Filament Control

Identify the filament and change the plant environment

Filament have specific growth preferences, take those away and the filament goes away

Chlorination of the RAS is a old standby and often works

Polymers and other chemicals fit in certain situations

Foam can be skimmed and trapped

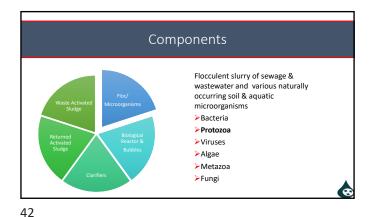
Change Mode of operation: step feed or contact stabilization lowers the solids load to the clarifier.

Contact stabilization can incubate filaments.

Selector units can be added

Anaerobic, Anoxic, Aerobic

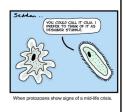
These change the F:M, DO, and growth environment



Protozoa- First Amimals

- · Single-celled animals that also reproduce by binary fission
- Have complex digestive systems that ingest organic matter, which they use as an energy and carbon
- Protozoans are much larger than bacteria, their size ranges from 10-500 microns

43



Protozoa- First Amimals

- They are an important link in the activated sludge food chain because they consume bacteria to fill a large part of their nutritional needs.
 - This seems not only to remove excess bacteria from WW, but appears to stimulate the growth of healthy bacteria, which produce floc more quickly and aid in the clarification of the
- Form cysts

44

- · Beneficial in wastewater treatment
- Indicators of health and secondary indicator of MCRT or age of system

Protozoa Found in the Activated Sludge Process Much less abundant than bacteria, but very important Require DO Flagellate has a whip-like tail and competes with bacteria Stalked ciliates – as adults, attach to something; as a "baby", has little hairs (cilia) to move around and move water and food into "mouth"

- Euglena has green algae in it that makes oxygen when the sun shines.







Protozoa - Amoeba

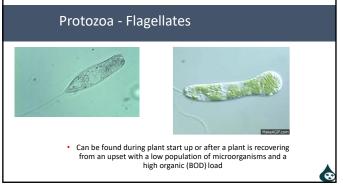
- · Young sludge indicators
- They can encyst themselves to make it through the system (unfavorable conditions)
- Look like donuts
- Can be found during plant start up or after a plant is recovering from an upset.







46 45



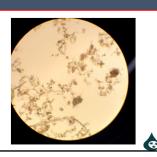
Protozoa – Free Swimming Ciliate (Paramecium) Free swimming ciliates generally are younger biomass organisms but are common in many plants Cilia covers entire shape Paramecium - 4.7 hours growth rate

47

Protozoa – Crawling Ciliates

- Resemble crabs or ladybugs
- May have some cilia but majority of body does not contain any
- · Croppers of biomass
- Cirri (A bundle or tuft of cilia serving as foot or tentacle in certain ciliate protozoa) are 4-5 cilia fused together
- · Very efficient feeders

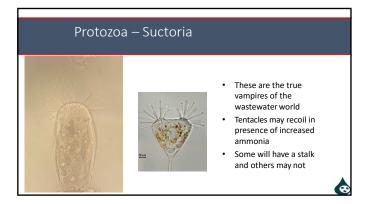


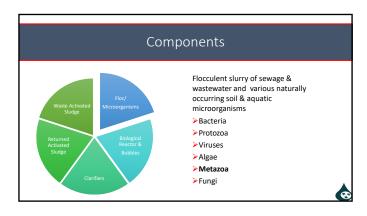


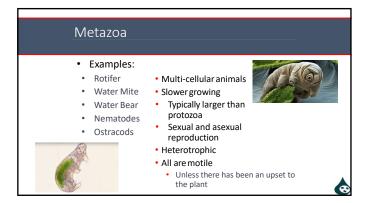
Protozoa – Stalked Ciliates

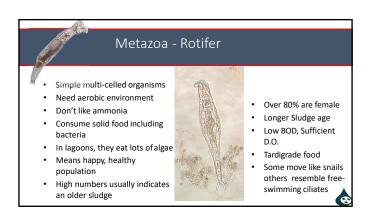
- They feed by drawing cells into their "mouth" with small cilia that create a visible twirling motion in the sample.
- · Can be individual or colonial
- · Length of stalk indicates age
- Some will have a myenome (contractile muscle fiber with in stalk)
- Size of oral opening may indicate health of system/more bacteria smaller opening and less bacteria larger, opening.
- Single (vorticella) vs colonial (epystylis) does not mean one is better than other, they are all individual species and grow based on the environment



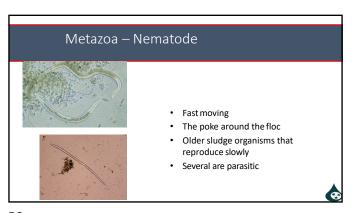


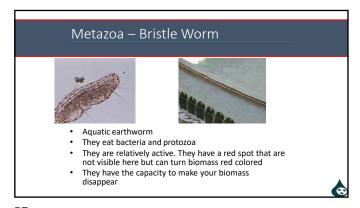


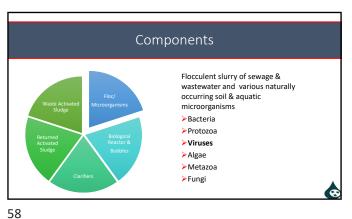




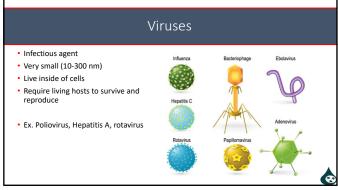


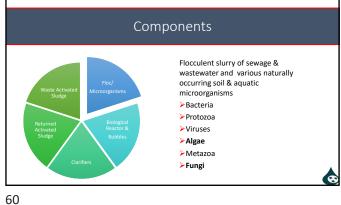


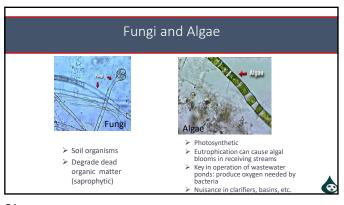


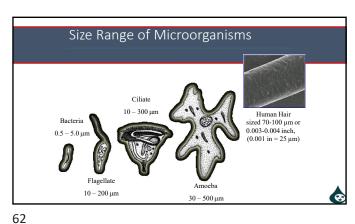


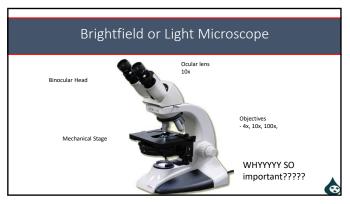
57 58

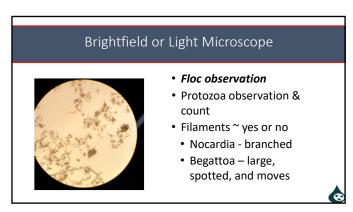






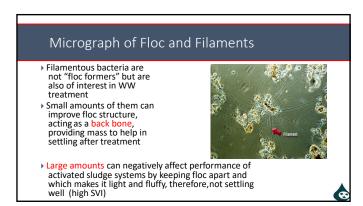




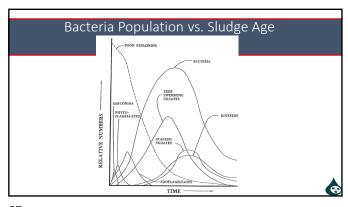


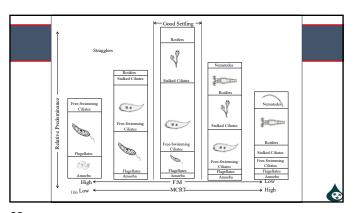
63





65 66





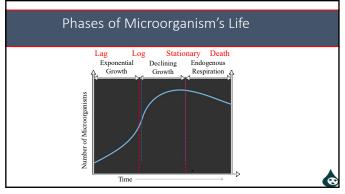
Microorganisms Predominance During a start up, after an upset amoebas, and flagellates will predominate The sludge will be young, display slow settling and leave behind straggler floc A large number of stalked ciliates, free-swimming ciliates and rotifers will indicate a stable and efficiently operated plant that produces a good settling sludge and a high quality effluent An old sludge is indicated by the predominance of rotifers and nematodes The sludge will settle at a high rate and leave pin floc behind

Microorganisms Predominance

If a conventional plant starts to see more rotifers and less free-swimming ciliates, you need to increase wasting to make old sludge go away

If an extended aeration plant has pin floc and nematodes, you are holding your sludge too long

69 70



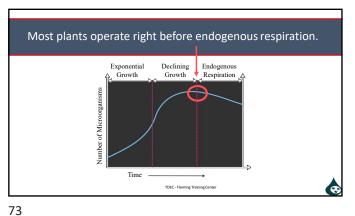
Note

> Exponential Growth – The number of microorganisms in a culture broth will grow exponentially until an essential nutrient is exhausted. Typically the first organism splits into two daughter organisms, who then each split to form four, who split to form eight, etc...

> Declining Growth – As food supply declines, the microorganisms work harder to get their food

> Reproduction rates gradually slow down

> Endogenous Respiration – There is inadequate food to maintain the biomass. Some microorganisms starve and die, others use their own stored energy to live



Treatment Plant Variables

The predominance, growth, and performance of your microbiological biomass (MLSS) is a function of:

Influent Characteristics

Influent Characteristics

Flow, amount and type of CBOD, ammonia, TSS, pH, other pollutants

Reactor Design

Shape, Feed points, Aeration, Mixing

Environment

Climate, water chemistry

Operating Conditions

F:M, MCRT/SRT, DO, RAS rates

Influent sewage and wastewater > Discharge from homes, businesses and industry > Mostly water, but there are organics from feces, paper, food scraps, grease, soaps & surfactants, industrial chemicals - we measure as CBOD > Inorganic pollutants include ammonia, metals, salts, industrial chemicals > Storm water and ground water also enter the plant, sometimes on purpose, many times from defects > We take most anything users can drain, flush, or discharge down the pipe including far too much I/I

Influent Impact and Control

Influent volume and concentration impacts plants significantly

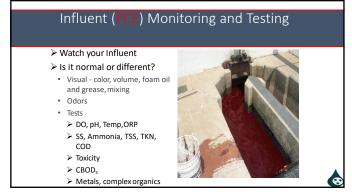
Influent control:

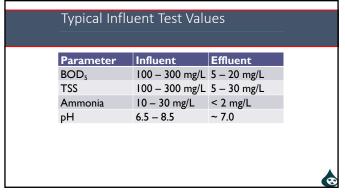
Influent volume and concentration impacts plants

Influent control:

Influent control

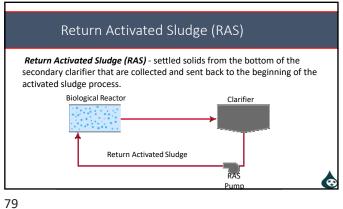
75 76





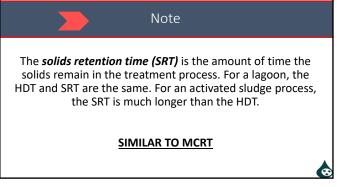
77 78

87



Return Activated Sludge (RAS)

- Enables solids to stay in the activated sludge process longer than
 - Solids retention time (SRT)
- SRT (sludge age) is independent of the amount of time water spends in the system.
- Gives microorganisms in the process more time to grow and reproduce
 - Leads to a high concentration of microorganisms
 - Reduces the time for treatment
 - Increases the load of BOD that can be processed



Internal Recycle Flows

Sources

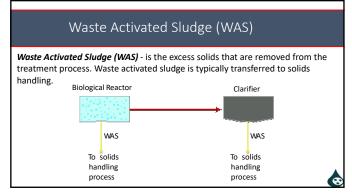
- ➤ Digester decant/supernatant
- ➤ Sludge dewatering/thicken underflow/overflow
- Clarifier skimming
- ➤ Basin dewatering
- > Sampler return
- > Wash-down water > Nutrient removal recycle



81

82

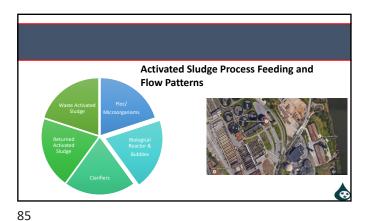
80

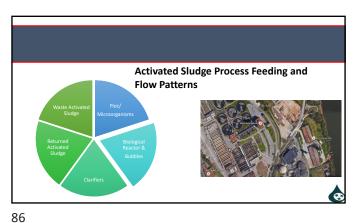


Waste Activated Sludge (WAS)

- Portion of settled solids removed from the system
- · Adjust the mass of WAS removed to maintain a target sludge age.
- Prevents excess sludge from overwhelming the secondary clarifier and escaping in the final effluent
- WAS may be removed directly from the activated sludge basin, the RAS line, or through a dedicated
- Excess sludge is transferred to solids handling.

83





Activated Sludge Process Variations

Categories:

1. Loading:

 High
 Medium
 Low
 Reactor Configuration
 Number of reactors
 Feed points
 Aeration processes
 Hydraulic detention times
 MCRT
These often overlap.

Note

Loading is the amount of organic material entering the plant

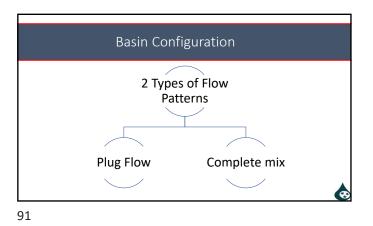
Can be calculated by: $BOD\ Loading, \frac{lbs}{day} = (Flow, MGD)(BOD, mg/L)(8.34\ lbs)$ Therease in loading Increase in organic material (BOD)

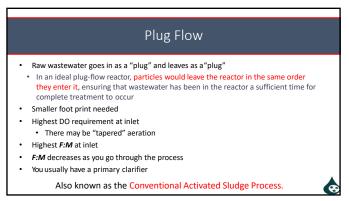
87

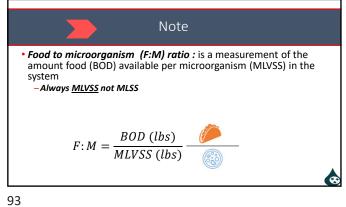
Activated Sludge Processes & Flow Patterns > Reactor Shapes > Physical Arrangement > Flow Patterns > Process Modifications > Modes of Operation > Feeding Points > Hydraulic DetentionTimes > Solids RetentionTimes

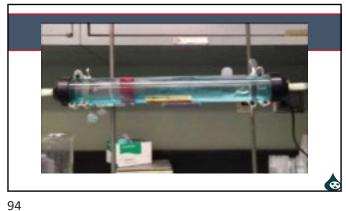
Activated Sludge Process Design Variations of the Plug-flow (conventional) activated sludge • Step Feed process have been · Contact Stabilization designed to: • Bardenpho 1. Minimize reactor Kraus sizes • Pure Oxygen 2. Reduce capital costs · Complete mix 3. Simply operations • Extended aeration 4. Adapt to site-· Oxidation ditches specific • High-rate aeration conditions

90





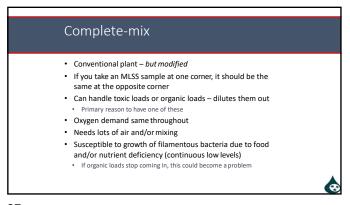


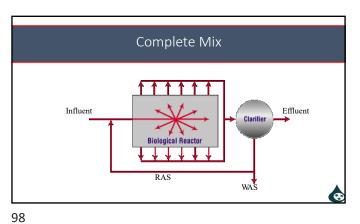


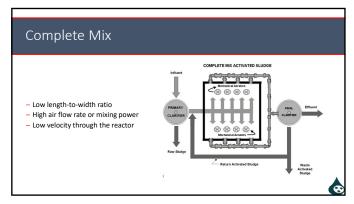
Criteria for a Plug-Flow Reactor	
High length-to width ratio	
Air flow rate minimized to meet specific treatment needs	
Fairly high wastewater velocity through the reactor	
Influent → To → Clarifier	&

	Design Parameters
Application	Domestic and Industrial
BOD Removal Efficiency	85 – 95%
AerationType	Diffused or Mechanical
MCRT	5 – 15 days
AerationTime	4 – 12 hours
MLSS	1500 – 3000 mg/L
RAS Flow	25 – 75% of influent
F:M	0.25 - 0.5 lbs BOD/d/lbs MLVSS
Organic Loading	20 - 40 lbs BOD/d/1000 ft ³

95







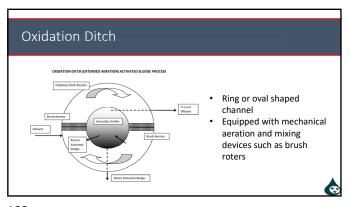


99 100

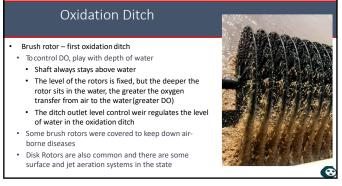
Complete Mix	Design Parameters
Application	Domestic and Industrial
BOD Removal Efficiency	85 – 95%
AerationType	Mechanical, Diffused
MCRT	5 – 15 days
AerationTime	3 – 10 hours, Ox. Ditch 18-36 hours
MLSS	2000 – 5000 mg/L
RAS Flow	25 – 100% of influent
F:M	0.2 – 0.6 lbs BOD/d/lbs MLVSS
Organic Loading	20 - 80 lbs BOD/d/1000 ft ³



101 102



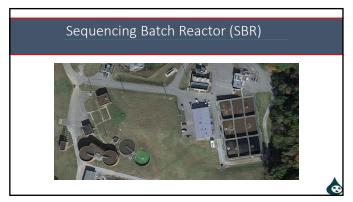


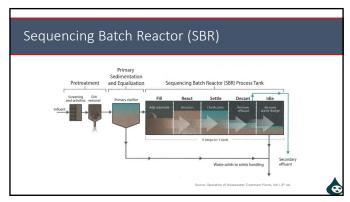


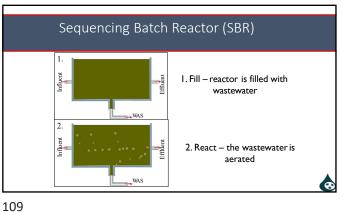
Oxidation Ditch

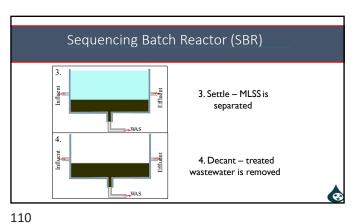
- Velocity of 1 ft/sec
- · Very low effluent BOD
- Large tank volume and high oxygen demand are disadvantages
- High MCRT and low F:M
- Low F:M filaments are common
- Energy Hog!

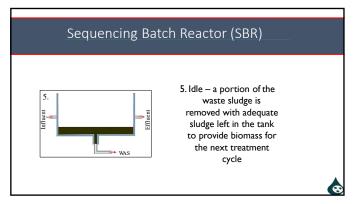
105 106

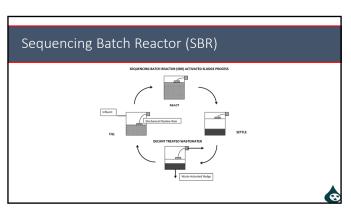




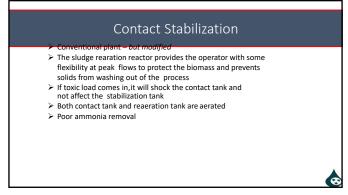


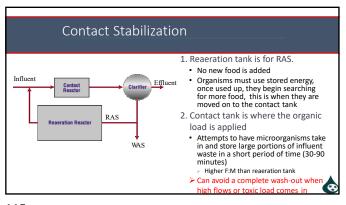


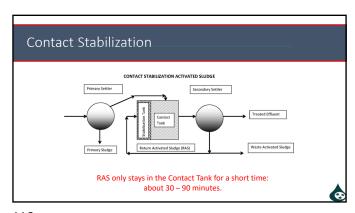


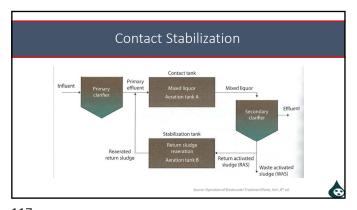


SBR De	sign Parameters
Application	Smaller Communities, There are big ones also. Cleveland TN
BOD Removal Efficiency	85 – 95%
AerationType	Diffused
MCRT	10 – 30 days
AerationTime	12 – 50 hours
MLSS	1500 – 5000 mg/L
RAS Flow	N/A
F:M	0.05 - 0.3 lbs BOD/d/lbs MLVSS
Organic Loading	25 lbs BOD/d/1000 ft ³









	ation Design Parameters
Application	Modification of Existing Plant
BOD Removal Efficiency	80 – 90%
AerationType	Diffused or Mechanical
MCRT	5 – 15 days
AerationTime	0.5 – 1.5 hour Contact
	3 – 6 hours Reaeration
MLSS	1000 - 3000 mg/L Contact
	4000 - 10000 mg/L Reaeration
RAS Flow	25 – 100% of influent
F:M	0.2 – 0.6 lbs BOD/d/lbs MLVSS
Organic Loading	30 - 75 lbs BOD/d/1000 ft ³

117 118

Bardenpho Proce	ess
Bardenpho process is named by Dr. James L. Barnardfor denitrification and phosphorus removal Used to remove between 90-95 percent of all the nitrogen present in the raw wastewater by recycling nitrate-rich mixed liquor from the aeration basin to an anoxic zone located ahead of the aeration basin Denitrification takes place in the anoxic zone in the absence of dissolved oxygen	Mary No. 19 No.

Bardenpho Process

➤ The degree of nitrate removal depends on the recycle rate

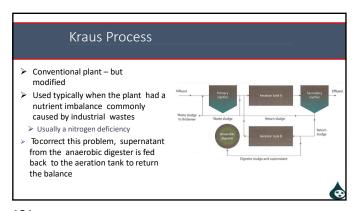
➤ Some plants have 2x, 4x, and even 6x the average dry weather flow back to the anoxic zone

➤ Usually 4x the average dry weather flow is sufficient

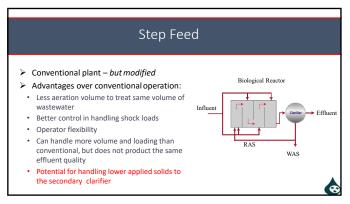
➤ If the nitrate in the effluent rises above 1 mg/L, the recycle rate is too high because not enough detention time is provided in the anoxic zone for denitrification to occur

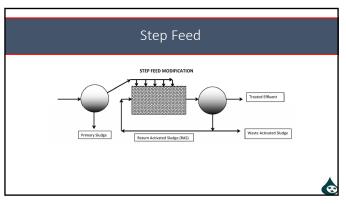
➤ If phosphorus removal is desired, a fermentation stage is added before the first anoxic zone

➤ Uses a Plug Flow/Conventional Pattern

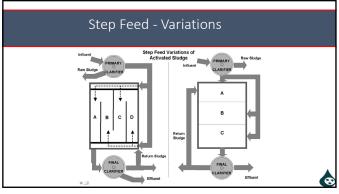


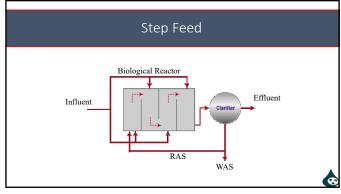




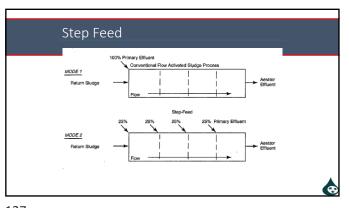


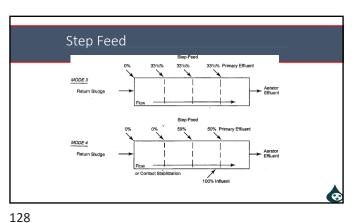
123 124

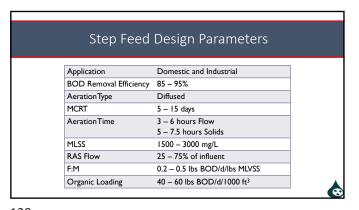


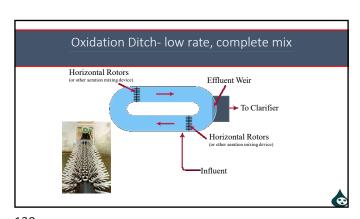


125 126

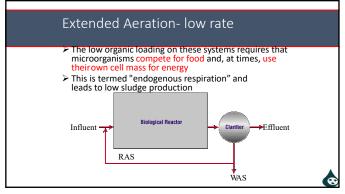


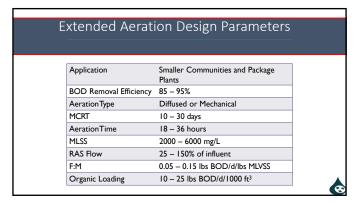


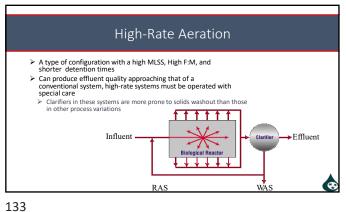


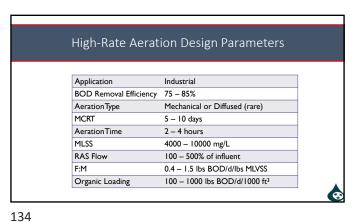


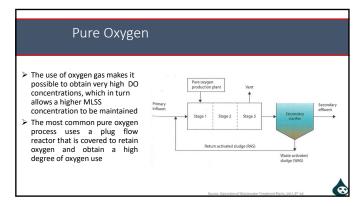
129 130

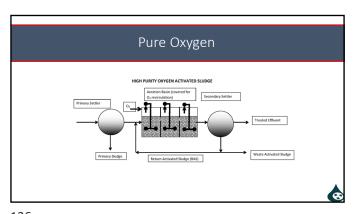




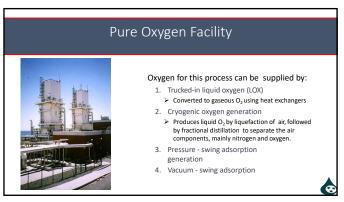




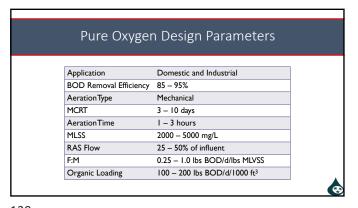




Pure Oxygen Facility ➤ Liquid oxygen is a fire hazard (comes delivered at -300ºF) > Continuously control oxygen feed rate depending on how active the microorganisms are Always has a covered tank to prevent costly pure oxygen from going off into the atmosphere (keeps it in the tank) > The wastewater, RAS, and oxygen feed gas enter the first stage of this system and flow concurrently through the reactor. \succ These systems can handle high organic loadings with shorter aeration periods because of their elevated MLSS ➤ Nitrification ability limited due to accumulation of CO₂ in gas headspace which causes low pH in mixed liquor

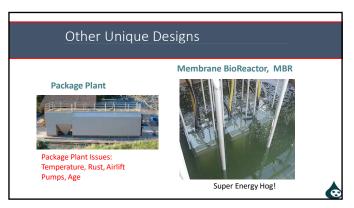


137 138

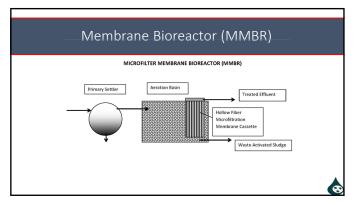


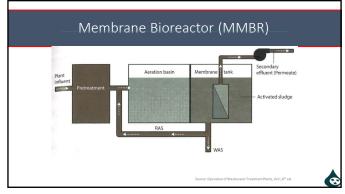






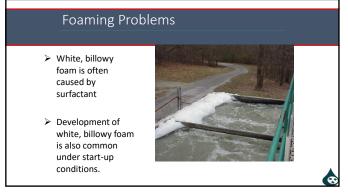
141 142











Old Sludge- High MCRT Foam

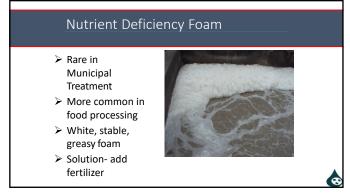
Thick, stable, often dark

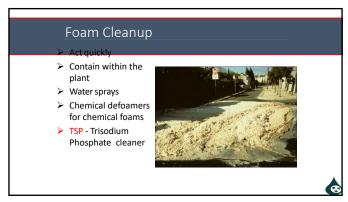
Tough to break up with water hose or spray

Generally will have Nocardia present

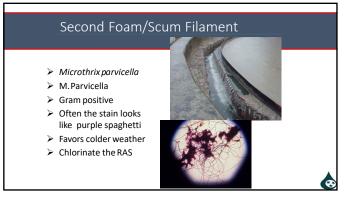
Solution-Waste!

147 148





149 150





Produce Clean Water (CleanWater Act) Remove Organic Pollutants (CBOD,other) Reduction of Pathogenic Organisms Removal of Nutrients & Inorganic Pollutants (Total Nitrogen & Phosphorus, NH₄, metals) Permit Limits- mg/L, lbs,% removal (85% monthly & 40% daily)



<u>Ac</u>	tivated Sludge Vocabulary – Part 1
1.	describes the taking in or soaking up of a substance into the body of
	another by molecular or chemical action.
2.	A mass or clump of organic material consisting of living organisms feeding on the wastes in wastewater, dead organisms, and other debris is called
3.	The biological wastewater treatment process that speeds up the decomposition of wastes, involving mixed liquor that is aerated and agitated before sedimentation, is called the
4.	The gathering of a gas, liquid, or dissolved substance on the surface or interface zone of another material is referred to as
5.	The is where raw or settled wastewater is mixed with return sludge and aerated.
6.	This type of bacteria can use either dissolved molecular oxygen or oxygen obtained from food materials such as sulfate or nitrate ions: In other words, these bacteria can live under aerobic or anaerobic conditions.
7.	The suspended solids in the mixed liquor of an aeration tank are called
8.	bacteria must have molecular (dissolved) oxygen (DO) to survive. These are also called aerobes. In contrast,bacteria do not need molecular (dissolved) oxygen to survive. These are also called anaerobes.
9.	bacteria grow in a thread-like or filamentous form and are a common
	cause of sludge bulking in the activated sludge process.
10.	The organic or volatile suspended solids in the mixed liquor of an aeration tank are called This volatile portion is used as a measure or indication of the microorganisms present.
11	
11.	An environment is oxygen deficient or lacking sufficient oxygen. Generally, it refers to an environment in which chemically bound oxygen, such as nitrate, is present.

12. A bacterial life phase that occurs when living organisms oxidize some of their own cellular mass due to an

13. When the activated sludge in an aeration tank is mixed with primary effluent or the raw wastewater and

return sludge, this mixture is then referred to as ______ as long as it is in the

inadequate amount of food in their environment is called ______.

aeration tank.

14.	he jelly-like masses of bacteria that are found in both the trickling filter and activated sludge process are
	alled masses.
Wo	d Bank:
Abs	rption
Mix	d liquor
End	genous respiration
Ana	robic
Fac	tative
Mix	d Liquor Volatile Suspended Solids (MLVSS)
Aer	pic
Aer	ion tank
Bio	ass
Zoo	eal
Ads	rption
Mix	d Liquor Suspended Solids (MLSS)
Fila	entous
Acti	ated sludge process
Anc	ic C

Activated Sludge Review Questions – Part 1

b. False

1.	In the activated sludge process, microorganisms convert organic matter to
	a. New cells, carbon dioxide and water
	b. New cells, ammonia and water
	c. Carbon dioxide, water and nitrate
	d. Carbon dioxide, water and chlorine
2.	The most basic components of the activated sludge process are
	a. Thickeners and digesters
	b. Screens and clarifiers
	c. Sand filters and chlorine contact chambers
	d. Biological reactors (aka aeration basins) and clarifiers
3.	Solids that settle to the bottom of clarifiers and are pumped back to the head of biological reactors are
	referred to as
	a. RAS
	b. WAS
	c. TSS
	d. Total residual chlorine
4.	Which combination of microbes would indicate a good settling sludge?
	a. Amoebas and nematodes
	b. Ciliates and rotifers
	c. Nematodes and paramecium
	d. Amoebas and bristle worms
5.	The process of reproduction where one mature cell divides into two new cells is known as
	a. Cellular deduction
	b. Binary fission
	c. Bacterial degradation
	d. Endogenous respiration
6.	Protozoans are
	a. Bacteria
	b. Microscopic plants
	c. Single-celled animals
	d. Worms
7.	Potential visual indicators of low DO concentrations include
	a. Presence of filamentous bacteria
	b. Turbid effluent
	c. Dark gray to black mixed liquor
	d. All of the above
8.	The required ratio of BOD:N:P:Fe in an activated sludge process is 100:10:5:0.5.
	a True

- 9. Which type of microorganism makes up about 95% of the mixed liquor in an activated sludge system?
 - a. Protozoans
 - b. Metazoans
 - c. Nematodes
 - d. Bacteria
- 10. This type of microorganism can encyst itself to move through unfavorable conditions, and is an indication of a young sludge
 - a. Amoebas
 - b. Water bears
 - c. Rotifers
 - d. Paramecium
- 11. Because it is photosynthetic, algae is key to the operation of wastewater ponds.
 - a. True
 - b. False
- 12. Which of the following conditions are favorable to the growth of filamentous bacteria?
 - a. Low DO
 - b. Nutrient deficiency
 - c. Septicity
 - d. Grease and oil
 - e. All of the above
- 13. This type of activated sludge process design has the highest oxygen demand at the influent inlet and will often utilize tapered aeration in order to supply more oxygen at the beginning of the process.
 - a. Contact stabilization
 - b. Plug Flow (aka "Conventional")
 - c. Oxidation ditch
 - d. Sequencing Batch Reactor
- 14. This type of activated sludge process design utilizes 2 tanks in the process train: the contact tank and the reaeration tank.
 - a. SBR
 - b. Step Feed
 - c. Contact Stabilization
 - d. Pure Oxygen
- 15. This type of activated sludge process design utilizes a low organic loading, which requires microorganisms to compete for food, and at times, use their own cell mass for energy (aka "endogenous respiration").
 - a. Complete mix
 - b. Plug flow
 - c. Extended aeration
 - d. High rate aeration

CHAPTER 7

Activated Sludge

7.1 General

- 7.1.1 Applicability
- 7.1.2 Process Selection
- 7.1.3 Pretreatment

7.2 <u>Types of Processes</u>

- 7.2.1 Conventional
- 7.2.2 Complete Mix
- 7.2.3 Step Aeration
- 7.2.4 Tapered Aeration
- 7.2.5 Contact Stabilization
- 7.2.6 Extended Aeration
- 7.2.7 High Rate Aeration
- 7.2.8 High Purity Oxygen
- 7.2.9 Kraus Process
- 7.2.10 Sequencing Batch Reactors (SBR)

7.3 <u>Aeration Tanks</u>

- 7.3.1 Required Volume
- 7.3.2 Shape and Mixing
- 7.3.3 Number of Units
- 7.3.4 Inlets and Outlets
- 7.3.5 Measuring Devices
- 7.3.6 Freeboard and Foam Control
- 7.3.7 Drain and Bypass
- 7.3.8 Other Considerations

7.4 <u>Aeration Equipment</u>

- 7.4.1 General
- 7.4.2 Diffused Air Systems
- 7.4.3 Mechanical Aeration Equipment
- 7.4.4 Flexibility and Energy Conservation

7.5 **Additional Details**

- 7.5.1 Lifting Equipment and Access7.5.2 Noise and Safety
- 7.6 Sequencing Batch Reactors (SBRs)
- 7.7 Oxidation Ditch
 - 7.7.1 General
 - 7.7.2 Special Details
 - 7.7.3 45 Degree Sloping Sidewall Tanks7.7.4 Straight Sidewall Tanks

ACTIVATED SLUDGE

7.1 General

7.1.1 Applicability

The activated sludge process and its various modifications may be used where sewage is amenable to biological treatment. This process requires close attention and more competent operator supervision than some of the other biological processes. A treatability study may be required to show that the organics are amendable to the proposed treatment. For example, industrial wastewaters containing high levels of starches and sugars may cause interferences with the activated sludge process due to bulking.

Toxic loadings from industries and excessive hydraulic loadings must be avoided to prevent the loss or destruction of the activated sludge mass. If toxic influents are a possibility, a properly enforced industrial pretreatment program will prove extremely beneficial to the WWTP and will be required. It takes days and sometimes weeks for the plant to recover from a toxic overload and will likely result in permit violations. Flow equalization, as detailed in Chapter 4, may be required in some instances. These requirements shall be considered when proposing this type of treatment.

7.1.2 Process Selection

The activated sludge process and its several modifications may be employed to accomplish varied degrees of removal of suspended solids and reduction of BOD and ammonia. Choice of the process most applicable will be influenced by the proposed plant size, type of waste to the treated, and degree and consistency of treatment required. All designs should provide for flexibility to incorporate as many modes of operation as is reasonably possible.

Calculations and/or documentation shall be submitted to justify the basis of design for the following:

- a. Process efficiency
- b. Aeration tanks
- c. Aeration equipment (including oxygen and mixing requirements)
- d. Operational rationale (including maintenance)
- e. Costs (capital and operating)

In addition, the design must comply with any requirements set forth in other chapters such as clarifiers, sludge processing, etc.

7.1.3 Pretreatment

Where primary settling tanks are not used, effective removal or exclusion of grit, debris, excessive oil or grease, and comminution or screening of solids shall be accomplished prior to the activated sludge process.

Where primary settling is used, provisions should be made for discharging raw sewage directly to the aeration tanks to facilitate plant start-up and operation during the initial stages of the plant's design life. Also, primary effluents are often low in D.O. This should be planned for in the design.

7.2 Types of Processes

Figure 7.1 shows the flow schematics of the major types of activated sludge processes, excluding pretreatment. The types that are simply modifications of these processes are not shown.

7.2.1 Conventional

Conventional activated sludge is characterized by introduction of influent wastewater and return activated sludge at one end of the aeration tank, a plug-flow aeration tank, and diffused aeration.

7.2.2 Complete Mix

Complete mix activated sludge is characterized by introduction of influent wastewater and return activated sludge throughout the aeration basin and the use of a completely mixed aeration tank. Complete mix aeration tanks may be arranged in series to approximate plug flow and conventional activated sludge.

7.2.3 Step Aeration

Step aeration activated sludge is characterized by introduction of the influent wastewater at two or more points in the aeration tank, use of a plug-flow aeration tank, and diffused aeration.

7.2.4 Tapered Aeration

Tapered aeration is similar to conventional activated sludge except that the air supply is tapered to meet the organic load within the tank. More air is added to the influent end of the tank where the organic loading and oxygen demand are the greatest.

7.2.5 Contact Stabilization

Contact stabilization activated sludge is characterized by the use of two aeration tanks for each process train, one to contact the influent wastewater and return activated sludge (contact tank) and the other to aerate the return activated sludge (stabilization tank) and promote the biodegradation of the organics absorbed to the bacterial flocs.

7.2.6 Extended Aeration

Extended aeration activated sludge is characterized by a low F/M ratio, long sludge age, and long aeration tank detention time (greater than 18 hours). For additional details on oxidation ditches see Section 7.7).

7.2.7 High-Rate Aeration

High-rate aeration activated sludge is characterized by high F/M ratio, low sludge age, short aeration tank detention time, and high mixed-liquor suspended solids. High-rate aeration should be followed by other BOD and suspended solids removal processes to provide secondary treatment.

7.2.8 High-Purity Oxygen

High-purity oxygen activated sludge is characterized by the use of high-purity oxygen instead of air for aeration.

7.2.9 Kraus Process

Kraus process activated sludge is characterized by use of an aeration tank to aerate a portion of the return activated sludge, digester supernatant, and digested sludge in order to provide nitrogen (ammonia) to a nitrogen-deficient wastewater.

7.2.10 Sequencing Batch Reactors (SBR)

The SBR process is a fill-and-draw, non-steady state activated sludge process in which one or more reactor basins are filled with wastewater during a discrete time period, and then operated in a batch treatment mode. SBR's accomplish equalization, aeration, and clarification in a timed sequence. For additional details see Section 7.6.

7.3 Aeration Tanks

7.3.1 Required Volume

The size of the aeration tank for any particular adaptation of the process shall be based on the food-to-microorganism (F/M) ratio, using the influent BOD (load per day) divided by the mixed-liquor volatile suspended solids. Alternatively, aeration tanks may be sized using sludge age. The calculations using the F/M ratio or sludge age shall be based on the kinetic relationships.

<u>APPENDIX 7A</u> shows the permissible range of F/M ratio, sludge age, mixed-liquor suspended solids, aeration tank detention time, aerator loading, and activated sludge return ratio for design of the various modifications of the activated sludge process. All design parameters shall be checked to determine if they fall within the permissible range for the selected F/M ratio or sludge area and the aeration tank size. Diurnal load variations and peak loadings must be considered when checking critical parameters.

7.3.2 Shape and Mixing

The dimensions of each independent mixed-liquor aeration tank or return sludge reaeration tank should be such as to maintain effective mixing and utilization of air when diffused air is used. Liquid depths should not be less than 10 feet or more than 30 feet except in special design cases. For plug-flow conditions using very small tanks or tanks with special configuration, the shape of the tank and/or the installation of aeration equipment should provide for elimination of short-circuiting through the tank.

Aerator loadings should be considered and the horsepower per 1,000 cubic feet of basin volume required for oxygen transfer should be limited to prevent excessive turbulence in the aeration basins, which might reduce activated sludge settleability.

7.3.3 Number of Units

Multiple tanks capable of independent operation may be required for operability and maintenance reasons, depending on the activated sludge process, size of the plant, and the reliability classification of the sewerage works (refer to Section 1.3.11).

7.3.4 Inlets and Outlets

7.3.4.1 Controls

Inlets and outlets for each aeration tank unit in multiple tank systems should be suitably equipped with valves, gates, stop plates, weirs, or other devices to permit control of the flow and to maintain reasonably constant liquid level. The hydraulic properties of the system should permit the maximum instantaneous hydraulic load to be carried with any single aeration tank unit out of service.

7.3.4.2 Conduits

Channels and pipes carrying liquids with solids in suspension should be designed to maintain self-cleaning velocities or should be agitated to keep such solids in suspension at all rates of flow within the design limits.

7.3.4.3 Hydraulics

Where multiple aeration tanks and secondary clarifiers are used, provisions should be made to divide the flow evenly to all aeration tanks in service and then recombine the flows, and to divide the flow evenly to all secondary clarifiers in service and then recombine the flows. Treatments plants using more than four aeration tanks and secondary clarifiers may divide the activated sludge systems into two or more process trains consisting of not less than two aeration tanks and secondary clarifiers per process train.

7.3.4.4 Bypass

When a primary settling tank is used, provisions shall also be made for discharging raw wastewater directly to the aeration tanks following pretreatment for start-ups.

7.3.5 Measuring Devices

For plants designed for less than 250,000 gallons per day, devices shall be installed for indicating flow rates of influent sewage, return sludge, and air to each aeration tank. For plants designed for greater than 250,000 gallons per day, devices shall be installed for totalizing, indicating, and recording influent sewage and returned sludge to each aeration tank. Where the design provides for all returned sludge to be mixed with the raw sewage (or primary effluent) at one location, the mixed-liquor flow rate to each aeration tank shall be measured, and the flow split in such a manner to provide even loading to each tank, or as desired by operations.

7.3.6 Freeboard and Foam Control

Aeration tanks shall have a freeboard of at least 18 inches. Freeboards of 24 inches are desirable with mechanical aerators.

Consideration shall be given for foam control devices on aeration tanks. Suitable spray systems or other appropriate means will be acceptable. If potable water is used, approved backflow prevention shall be provided on the water lines. The spray lines shall have provisions for draining to prevent damage by freezing.

7.3.7 Drain and Bypass

Provisions shall be made for dewatering each aeration tank for cleaning and maintenance. The dewatering system shall be sized to permit removal of the tank contents within 24 hours. If a drain is used, it shall be valved. The dewatering discharge shall be upstream of the activated sludge process.

Provisions shall be made to isolate each aeration tank without disrupting flow to other aeration tanks.

Proper precautions shall be taken to ensure the tank will not "float" when dewatered.

7.3.8 Other Considerations

Other factors that might influence the efficiency of the activated sludge process should be examined. Septic and/or low pH influent conditions are detrimental, particularly where primary clarifiers precede the activated sludge process or when the collection system allows the sewage to go septic. Often, the pH is buffered by the biological mass, but wide variations in the influent should be avoided and, if present, chemical addition may be necessary.

Aerobic organisms require minimum quantities of nitrogen and phosphorus. Domestic wastewater usually has an excess of nitrogen and phosphorus; however, many industrial wastewaters are deficient in these elements. A mass balance should be performed to see if the combined industrial and domestic influent contains sufficient nitrogen and phosphorus or if nutrient levels will have to be supplemented.

7.4 Aeration Equipment

7.4.1 General

Oxygen requirements generally depend on BOD loading, degree of treatment, and level of suspended solids concentration to be maintained in the aeration tank mixed liquor. Aeration equipment shall be designed to supply sufficient oxygen to maintain a minimum dissolved oxygen concentration of 2 milligrams per liter (mg/l) at average design load and 1.0 mg/l at peak design loads throughout the mixed liquor. In the absence of experimentally determined values, the design oxygen requirements for all activated sludge processes shall be 1.1 lbs oxygen per lb peak BOD₅ applied to the aeration tanks, with the exception of the extended aeration process, for which the value shall be 2.35. Aeration equipment shall be of sufficient size and arrangement to maintain velocities greater than 0.5 foot per second at all points in the aeration tank.

The oxygen requirements for an activated sludge system can be <u>estimated</u> using the following relationship:

 $O_2 = (a) (BOD) + b (MLVSS)$

 O_2 = pounds of oxygen required per day

BOD = pounds of BOD removed per day (5-day BOD)*

MLVSS = pounds of mixed liquor volatile suspended solids contained in the aeration basin

a= amount of oxygen required for BOD synthesis. "a" will range from 0.5 to 0.75 pound of oxygen per pound of BOD removed

b= amount of oxygen required for endogenous respiration or decay. "b" will range from 0.05 to 0.20 pound of oxygen per pound of MLVSS

*BOD removal shall be calculated as influent BOD5 minus soluble effluent BOD5.

For preliminary planning before process design is initiated, a rough estimate can be obtained by using 1.0 to 1.2 pounds of oxygen per pound of BOD removed (assuming no nitrification).

7.4.2 Diffused Air Systems

7.4.2.1 Design Air Requirements

The aeration equipment shall be designed to provide the oxygen requirements set forth above. Minimum requirements for carbonaceous removal are shown below. (Oxygen requirements for nitrification are <u>in addition</u> to that required for carbonaceous removal where applicable; i.e., low F/M.)

Cubic Feet of Air Available per Pound of BOD Load Applied

to Aeration Tank	
1,500	
1,500	
1,500	
400 to 1,500	
2,100	

Air required for channels, pumps, or other air-use demand shall be added to the air volume requirements.

Manufacturers' specifications must be corrected to account for actual operation conditions (use a worst case scenario). Corrections shall be made for temperatures other than 20°C and elevations greater than 2,000 feet.

7.4.2.2 Special Details

The specified capacity of blowers or air compressors, particularly centrifugal blowers, shall take into account that the air intake temperature might reach extremes and that pressure might be less than normal. Motor horsepower shall be sufficient to handle the minimum and maximum ambient temperatures on record.

The blower filters shall be easily accessible. Spare filters should be provided.

The blowers shall be provided in multiple units, arranged and in capacities to meet the maximum air demand with the single largest unit out of service. The design shall also provide for varying the volume of air delivered in proportion to the load demand of the plant.

The spacing of diffusers shall be in accordance with the oxygen and mixing requirements in the basin. If only one aeration tank is proposed, arrangement of

diffusers should permit their removal for inspection, maintenance, and replacement without de-watering the tank and without shutting off the air supply to other diffusers in the tank.

Individual units of diffusers shall be equipped with control valves, preferably with indicator markings, for throttling or for complete shutoff. Diffusers in each assembly shall have substantially uniform pressure loss. The adjustment of one diffuser should have minimal influence on the air supply rate to any other diffusers.

Flow meters and throttling valves shall be placed in each header. Air filters shall be provided as part of the blower assembly to prevent clogging of the diffuser system. Means shall be provided to easily check the air filter so that it will be replaced when needed.

7.4.3 Mechanical Aeration Equipment

Power input from mechanical aerators should range from 0.5 to 1.3 horsepower per 1,000 cubic feet of aeration tank.

The mechanism and drive unit shall be designed for the expected conditions of the aeration tank in terms of the proven performance of the equipment.

Due to the high heat loss, consideration shall be given to protecting subsequent treatment units from freezing where it is deemed necessary. Multiple mechanical aeration unit installations shall be designed to meet the maximum oxygen demand with the largest unit out of service. The design shall normally also provide for varying the amount of oxygen transferred in proportion to the load demand on the plant.

A spare aeration mechanism shall be furnished for single-unit installations. Access to the aerators shall be provided for routine maintenance.

7.4.4 Flexibility and Energy Conservation

The design of aeration systems shall provide adequate flexibility to vary the oxygen transfer capability and power consumption in relation to oxygen demands. Particular attention should be given to initial operation when oxygen demands may be significantly less that the design oxygen demand. The design shall always maintain the minimum mixing levels; mixing may control power requirements at low oxygen demands.

Dissolved oxygen probes and recording should be considered for all activated sludge designs. Consideration will be given to automatic control of aeration system oxygen transfer, based on aeration basin dissolved oxygen concentrations, provided manual back-up operation is available. A dissolved oxygen field probe and meter is to be provided for all activated sludge installations.

115

Watt-hour meters shall be provided for all aeration system drives to record power usage.

Energy conservation measures shall be considered in design of aeration systems. For diffused aeration systems, the following shall be considered:

- a. Use of small compressors and more units
- b. Variable-speed drives on positive-displacement compressors
- c. Intake throttling on centrifugal compressors
- d. Use of timers while maintaining minimum mixing and D.O. levels (consult with manufacturer's recommendations for proper cycling)
- e. Use of high-efficiency diffusers
- f. Use of separate and independent mixers and aerators

For mechanical aeration systems, the following shall be considered:

- a. Use of smaller aerators
- b. Variable aeration tank weirs
- c. Multiple-speed motors
- d. Use of timers

7.5 Additional Details

7.5.1 Lifting Equipment and Access

Provisions shall be made to lift all mechanical equipment and provide sufficient access to permit its removal without modifying existing or proposed structures.

7.5.2 Noise and Safety

Special consideration shall be given to the noise produced by air compressors used with diffused aeration systems and mechanical aerators. Ear protection may be required. Silencers for blowers may be required in sensitive areas.

Handrails shall be provided on all walkways around aeration tanks and clarifiers.

The following safety equipment shall be provided near aeration tanks and clarifiers:

Safety vests Lifelines and rings Safety poles

Walkways near aeration tanks shall have a roughened surface or grating to provide safe footing and be built to shed water.

Guards shall be provided on all moving machinery in conformance with OSHA requirements.

Sufficient lighting shall be provided to permit safe working conditions near aerations tanks and clarifiers at night.

7.6 Sequencing Batch Reactors (SBRs)

SBRs shall be designed to meet all the requirements set forth in preceding sections on activated sludge. Special consideration shall be given to the following:

- 7.6.1 A pre-aeration, flow-equalization basin is to be provided for when the SBR is in the settle and/or draw phases. If multiple SBR basins are provided, a pre-aeration basin will not be needed if each SBR basin is capable of handling all the influent peak flow while another basin is in the settle and/or draw phase.
- 7.6.2 When discharging from the SBR, means need to be provided to avoid surges to the succeeding treatment units. The chlorine contact tank shall not be hydraulically overloaded by the discharge.
- 7.6.3 The effluent from the SBRs shall be removed from just below the water surface (below the scum level) or a device which excludes scum shall be used. All decanters shall be balanced so that the effluent will be withdrawn equally from the effluent end of the reactor.
- 7.6.4 Prevailing winds must be considered in scum control.

7.7 Oxidation Ditch

7.7.1 General

The oxidation ditch is a complete-mixed, extended aeration, activated sludge process which is operated with a long detention time. Brush-rotor (or disk type) aerators are normally used for mixing and oxygen transfer. All requirements set forth in previous sections and/or chapters must be met, with the exception of those items addressed below.

7.7.2 Special Details

7.7.2.1 Design Parameters

The design parameters shall be in the permissible range as set forth in Table 7.1 for F/M, sludge age, MLSS, detention time, aerator loading, and activated sludge return ratio.

7.7.2.2 Aeration Equipment

Aeration equipment shall be designed to transfer 2.35 pounds of oxygen per pound of BOD at standard conditions. The oxygen requirement takes into account nitrification in a typical wastewater. Also, a minimum average velocity of one foot per second shall be maintained, based on the pumping rate of the aeration equipment and the aeration basin cross-sectional area.

A minimum of two aerators per basin is required.

7.7.2.3 Aeration Tank Details

a. Influent Feed Location

Influent and return activated sludge feed to the aeration tank should be located just upstream of an aerator to afford immediate mixing with mixed liquor in the channel.

b. Effluent Removal Location

Effluent from the aeration channel shall be upstream of an aerator and far enough upstream from the injection of the influent and return activated sludge to prevent short-circuiting.

c. Effluent Adjustable Weir

Water level in the aeration channel shall be controlled by an adjustable weir or other means. In calculating weir length, use peak design flow plus maximum recirculated flow to prevent excessive aerator immersion.

d. Walkways and Splash Control

Walkways must be provided across the aeration channel to provide access to the aerators for maintenance. The normal location is above the aerator. Splash guards shall be provided to prevent spray from the aerator on the walkway. Bridges should not be subject to splash from the rotors.

e. Baffles

Horizontal baffles, placed across the channel, may be used on all basins with over 6 feet liquid depth, and may be used where the manufacturer recommends them to provide proper mixing of the entire depth of the basin.

Baffles should be provided around corners to ensure uniform velocities.

7.7.3 45-Degree Sloping Sidewall Tanks

7.7.3.1 Liquid Depth

Liquid depth shall be 7 to 10 feet, depending on aerator capability, as stated by the manufacturer.

7.7.3.2 Channel Width at Water Level

The higher ratios (channel width at water level divided by aerator length) are to be used with smaller aerator lengths.

3- to 15-foot-long rotors, ratio 3.0 to 1.8.

16- to 30-foot-long rotors, ratio 2.0 to 1.3

Above 30-foot-long rotors, ratio below 1.5

7.7.3.3 Center Island

When used, the minimum width of center island at liquid level, based on aerator length, should be as follows (with center islands below minimum width, use return flow baffles at both ends):

3- to 5-foot-long rotor, 14 feet

6- to 15-foot-long rotor, 16 feet

16- to 30-foot-long rotor, 20 feet

Above 30-foot-long rotors, 24 feet

7.7.3.4 Center Dividing Walls

Center dividing walls can be used but return flow baffles at both ends are required. The channel width, W, is calculated as flat bottom plus 1/2 of sloping sidewall. Baffle radius is W/2. Baffles should be offset by W/8, with the larger opening accepting the flow and the smaller opening downstream compressing the flow.

7.7.3.5 Length of Straight Section

Length of straight section of ditch shall be a minimum of 40 feet or at least two times the width of the ditch at liquid level.

7.7.3.6 Preferred Location of Aerators

Aerators shall be placed just downstream of the bend, normally 15 feet, with the long straight section of the ditch downstream of the aerator.

7.7.4 Straight Sidewall Tanks

7.7.4.1 Liquid Depth

Liquid depth shall be 7 to 12 feet, depending on aerators.

7.7.4.2 Aerator Length

Individual rotor length shall span the full width of the channel, with necessary allowance required for drive assembly and outboard bearing.

7.7.4.3 Center Island

Where center islands are used, the width should be the same as with 45-degree sloping sidewalls, or manufacturer's recommendation.

7.7.4.4 Center Dividing Walls

When a center dividing wall is used, return flow baffles are required at both ends. Return flow baffle radius is width of channel, W, divided by 2, W/2. Baffles should be offset by W/8, with the larger opening accepting the flow and the smaller opening downstream compressing the flow.

7.7.4.5 Length of Straight Section

Length of straight section downstream of aerator shall be near 40 feet or close to two times the aerator length. In deep tanks with four aerators, aerators should be placed to provide location for horizontal baffles.

7.7.4.6 Preferred Location of Aerators

Aerators should be placed just downstream of the bend with the long straight section of the tank downstream of the aerator. Optimal placement of rotors will consider maintaining ditch center line distance between rotors close to equal.

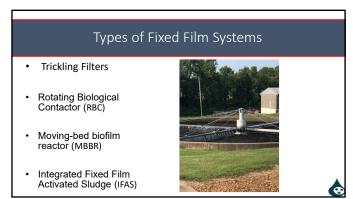
APPENDIX 7-A

Section 5 Fixed Film Systems









2

Theory of Fixed Film Operation

Microorganisms are attached to a surface over which they grow

Biomass attached to media (rock, plastic, etc.)
Recycling of settled biomass is not required
However, trickling filters often recirculate/recycle

3

5

Theory of Fixed Film Operation

Oxygen (natural or forced draft)

Wastewater

Organics/ nutrients

viscous, jelly-like substance containing bacteria

Blomass = "zoogleal mass" "Slime growth" or "Blofilm"

Filter media = rock, slag, coal, bricks, redwood blocks or molded plastic

4

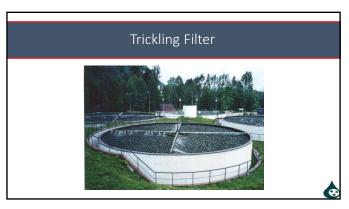
Fixed Film Systems What can this process do? Remove nutrients Removed dissolved organic solids Remove suspended organic solids Removal occurs primarily by converting soluble and colloidal material into a biological film that develops on the filter media Just like a suspended growth system!

• Simplicity
• Lower maintenance
• Lower power/electrical costs
• Less production excess biological solids
• Resistance to shock loads

6

Fixed Film Systems

- Nutrient deficiency- industrial waste (specifically food processing)
 - 100 BOD:5N:1P ratio for producing biological cells
- More sensitive to temperature drops
 - Covers, windbreaks, forced ventilation, etc.
- Low DO (RBCs)
 - Filamentous bacteria



7

8



Trickling Filter

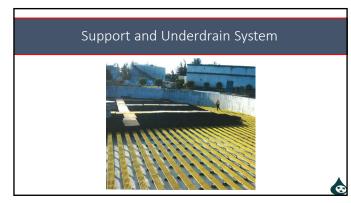
Rotating
Distributor Arm

Plastic Media

9

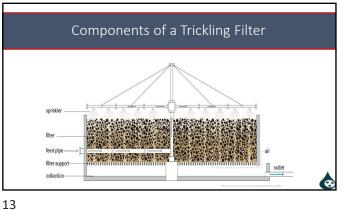
10





11

12



Components of a Trickling Filter • Usually has a rotary-type distributor that consists of two or more horizontal pipes supported a few inches above the filter media by a central column • WW is fed from column through horizontal pipes and distributed over media through orifices located along one side of pipes

• Rotation of arm is due to water-sprinkler reaction from WW flowing out orifices or by mechanical means

14

• Have quick-opening or arm dump gates at the end of each arm to permit easy flushing

Trickling Filter Side View A rotating arm sprays wastewater over a filter medium · Filter medium: rocks, plastic, or other material. Packing The water is collected at the bottom of the filter for further treatment Not really a filter, it does not work like sand or filter paper Underdrain Wastewater



15 16

What is Zoogleal Film (Biomass)?

- · Collection of bacteria, protozoa, fungi, algae, and higher animals
- •95% bacteria
- Protozoa and higher animals are "grazers"
- Can approximate viable biomass by VSS





17 18

Managing Biofilm Thickness

- •Grazing by predators
 - •Worms very important as grazers-
 - Keeps biomass healthy
 - Tunneling by worms aerates biofilm and causes excess to slough off
- Erosion (liquid shearing)
- Sloughing (weakening of biofilm)
 - Sloughings = TF slimes that have been washed off the filter media

Design Considerations

- Influent wastewater characteristics
- Degree of treatment anticipated (BOD & TSS removal)
- Temperature range of applied wastewater
- Preliminary and primary treatment processes
- Type of filter media
- Recirculation rate
- Hydraulic and organic loadings applied to the filter
- Underdrain and ventilation systems

Trickling Filter Media

 Crushed rock (river or aggregate)
 Durable & insoluble
 Locally available
 Negative: reduce the void spaces for passage of air
 Less surface area per volume for biological growth

19 20

Trickling Filter Media

Plastic media

- · Can be loaded at higher rates
- · Larger void spaces
- Lighter
 - Random packing media
 - Modular packing media
 - Vertical-flow media
 - Cross-flow media
- Often referred to as Biotower



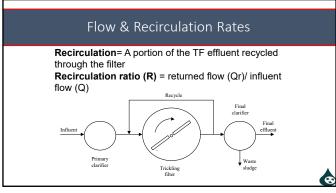
22

21

Redwood media Commercial wood media consists of rough sawn redwood slates stacked horizontally on wood spacers No longer manufactured but can be found in existing facilities

Trickling Filter Media Considerations

- The ideal filter packing is material that:
 - has a high surface area per unit of volume
 - is low in cost
 - · has a high durability
 - has a high enough porosity so that clogging is minimized
 - provides good air circulation



23 24

¹²⁸ Fixed Film

Recirculation Design Considerations

Recirculation is used to maintain a constant load on the filter and thus produce a better quality of effluent

- · Increase efficiency
- Maintain constant wetting rate and hydraulic loading
- · Dilute toxic wastes
- · Increase air flow
- Recirculation flow dilutes the strength of raw wastewater & allows untreated wastewater to be passed through the filter more than once.
- · Prevent freezing

Recirculation Design Considerations

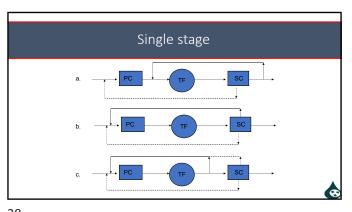
- During low-inflow periods = keep slime growths wet, minimize fly growth, and wash off excess sloughings
- Returning TF effluent to the 1°clarifier is an effective odor control measure
 - adds oxygen to incoming ww that is often septic
- A common range for recirculation ratio
- Use the lowest recirculation rate that will produce good effluent but not cause ponding

25 26

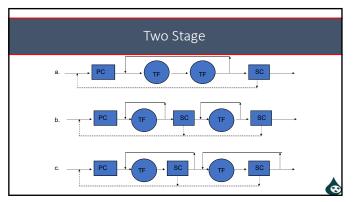
Classification of filters

Depending upon the hydraulic and organic loadings applied:

- 1. Standard rate
- 2. High rate
- Heavy flow of ww over the media = more uniform sloughing of filter growths
- 3. Roughing filters
 - Used primarily to reduce organic load on subsequent oxidation processes (ex: second stage filter or AS process)
 - Often used in plants that receive strong organic industrial



28 27



Two Stage • Two stage desirable when: • High quality effluent is required • High strength WW is treated • Cold weather operation is needed • Intermediate clarifier minimizes clogging of the second • It is often preferred to recirculate clarifier effluent • Reduces chances of solids clogging the filter media • Most solids in the TF effluent will have settled in the clarifier • Risk is to hydraulically overload the clarifier

29 30

Underdrainage and Ventilation Systems

• Two purposes:

31

- 1. to carry the filtered wastewater and the biomass lump (sloughed solids) from the filter to the final clarification process
- 2. to provide for ventilation of the filter to maintain aerobic conditions.
- •The underdrain system is generally designed to flow one-third to one-half full to permit ventilation of the system.

Ventilation System

- •In TF system:
 - · Air is supplied by natural draft or forced draft ventilation
 - •The forced draft fans have been applied to provide adequate oxygen

Secondary Clarification

- Removes excess biological solids (sloughings)
- Typically round with scraper units
- Thin sludge blanket controls denitrification
 - · Less than 1 foot suggested
 - Sloughings contain large amount of organic matter that could go septic in a deeper blanket

Abnormal Conditions

- Ponding-filter plugging
- Odors
- Filter flies
- Uncontrolled periodic sloughing
- Poor effluent quality
- · Icing on filter
 - · Decrease recirculation
- Snails



33

34

32

Odors

- Organic overloading or inadequate air circulation
- Excess sloughing of biofilm
- Controlled by:
 - · Covering filter
 - Air scrubbers
 - Masking agents



Odor Control

- · Maintain aerobic conditions in sewer and in preceding plant processes
- Check filter ventilation
- Increase recirculation ratio
- Better housekeeping: wash down distributor splash plates and wall above media

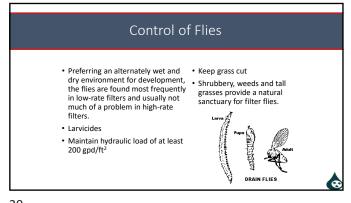
35 36

Ponding in Trickling Filters · Rake filter surface manually Ponding can cause anaerobic conditions within the trickling • Dose with chlorine at 5 mg/L (several hours) • Ensure preceding units operating • Flood filter for 24 hrs properly Increase recirculation rate = • Excess SS, scum, BOD, more oxygen and increased trash from primary sloughing clarifier can cause • Replace media problems Spray surface with high pressure water

Control of Insects, Snails, & Algae

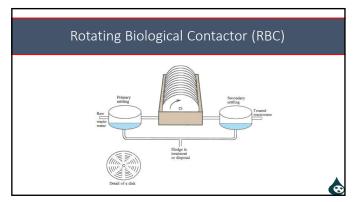
- Visually inspect for ponding
- Increase recirculation ratio
- Flush filter & chlorinate
 - Chlorinate to residual of 1.0 mg/L for several hours.
- Algae: DON'T apply herbicide

37 38



Typical Loading Rates 6-8 ft deep; 3-5 ft deep; 15-30 ft deep; 15-30 ft deep; periodically continuously continuously continuously 100-1,000 350-2,100 1,400-4,200 Hydraulic 25-100 gpd/ft² gpd/ft² gpd/ft² 25-100 lbs BOD /day/1,000 ft³ Organic (BOD) 50-300 lbs BOD BOD/ day /1,000 ft³ day/1,000 ft /day/1,000 ft **BOD Removal** 50-70% 65-85% 40-65% 80-90% Effluent BOD 20-25 mg/L 20-50 mg/L

39 40



Rotating Biological Contactor (RBC)

• Treats domestic and biodegradable industrial wastes
• Rotating steel shaft with HDPE disc media (drum)
• Mechanical or compressed air drive
• Drum rotates through WW for food then through air for oxygen

41 42

Rotating Biological Contactor (RBC)

Plants have been designed to treat flows ranging 18,000 gpd to 50 MGD, however the majority of plants treat flows of less than 5 MGD

- Advantages of RBC's over Trickling Filters:
 - Elimination of the rotating distributor
 - Elimination of ponding problems
 Elimination of filter flies
- Disadvantages:

43

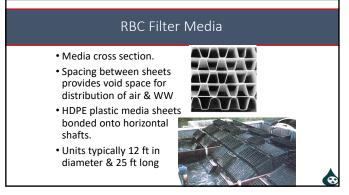
- Lack of recirculation ability
- · More sensitive to industrial wastes

Rotating Biological Contactor (RBC)

- Primary clarifier effluent enters RBC tank
- Organisms on biofilm treat WW
- Media rotates at 1.5 rpm

44

- Excess biofilm sloughs into WW and is removed in secondary clarifier
- Approximately 40% of media surface is immersed in the wastewater
- Usually the process operates on a "oncethrough" scheme, with no recycling



Stages of RBC

- The RBC is usually divided up into four or more different stages
- Each stage is separated by a removable baffle, concrete wall or cross-tank bulkhead
- Each bulkhead or baffle has an underwater orifice or hole to permit flow from one stage to the next
- Each section of media between bulkheads acts as a separate stage of treatment

45 46

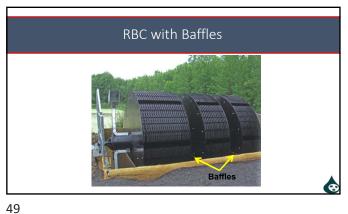
Stages of RBC

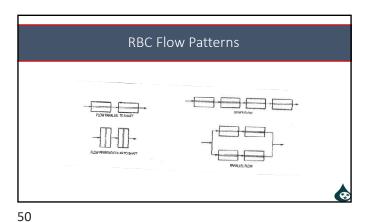
- Staging is used in order to maximize the effectiveness of a given amount of media surface area
- Organisms on the first-stage media are exposed to high levels of BOD and reduce the BOD at a high rate
- As the BOD levels decrease from stage to stage, the rate at which the organisms can remove BOD decreases and nitrification starts

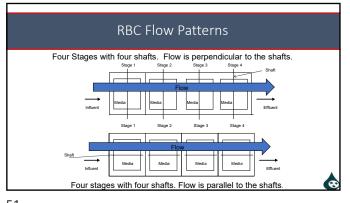
RBC Stage Arrangements

The stage of the sta

47 48

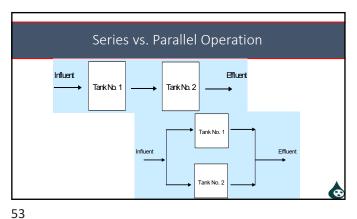






Series vs. Parallel Operation Treatment plants requiring four or more shafts of media usually are arranged so that each shaft serves as an individual stage of treatment • The shafts are arranged so the flow is perpendicular to the shafts • Plants with fewer than four shafts are usually arranged with the flow parallel to the shaft

51 52

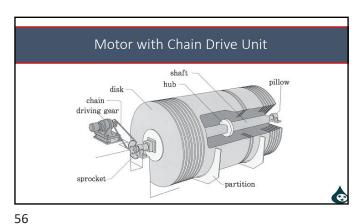


Air Driven Units · Air control valve on shaft controls inlet air supply to each unit • Course bubble air diffusers on headers on floor of concrete or steel tank force air to cause unit to rotate

54

Motor with Chain Drive Unit

- Inspection: bearing caps; roller chain alignment; belts; check for noise from bearings & drive package; main shaft bearing temperature (by hand)
- Periodically remove sludge & debris settling below media: reduces tank volume; cause septicity; scrape biofilm from media; can stall unit



55

Daily Inspection of Biomass

- Healthy = uniform, thin brown to gray, shaggy growth; no algae present
- Organic overload = heavy, shaggy brown to black
- Rusty Red color = nitrification
 - Completion of BOD removal
 - Can be irregular growth due to predator organisms



Daily Inspection of Biomass

- White slime:
 - Sulfur bacteria (Thiothrix)- poor settling sludge and low BOD removal
 - Result from industrial discharges containing sulfur compounds
 - Another cause may be sludge deposits that have accumulated in the bottom.

To remove:

Drain basin, wash out sludge, and return to service

57 58

Daily Inspection of Biomass

- Control of snails:
 - Chlorinate off line at 50-70 mg/L, rotating filter, for 2-3 days, then dechlorinate before discharging with sulfur dioxide
 - Increase pH to 10 with sodium hydroxide, caustic soda or lime for 8 hours (kills snails without harming the microbial growth). May have to repeat every 1-2 months

High Hydrogen Sulfide

- Extreme overload first stage causes low D.O thereafter
- Septic influent in collection system too long or industrial discharge
- Anaerobic sludge deposits in tank
- Low D.O due to warm weather

60

59

RBC Covers

- Protect biofilm from freezing
- Prevent rain from washing biofilm off of media
- Prevent media exposure to sunlight (& algae growth)
- Prevent UV rays from degrading media
- Provide protection for operators from the elements while maintaining equipment
- Eliminates fogging potential
- Can also enclose several units in building (must have ventilation, lights, humidity control)



61 62

Process Monitoring

- BOD: permit compliance; soluble BOD determined by filtering WW
- Suspended Solids: permit compliance
- Nitrogen: ammonia
- Phosphorus: filtered sample; BOD:N:P =100:5:1
- Dissolved Oxygen: throughout facility
- Heavy Metals
- Oil and Grease
- pH: neutral optimum

RBC Performance					
Characteristic	Range				
Hydraulic Loading					
BOD Removal	1.5 – 6 gpd/ft ²				
Nitrogen Removal	1.5 – 1.8 gpd/ft ²				
Organic Loading					
Soluble BOD	2.5 – 4 lbs BOD/day/1,000 ft ²				
BOD Removal	80 – 90%				
Effluent Total BOD	10 – 30 mg/L				
Effluent Soluble BOD	5 – 15 mg/L				
Effluent Ammonia Nitrogen	1 – 10 mg/L				
Effluent Nitrate Nitrogen	2 – 7 mg/L				

Moving Bed Biofilm Reactor (MBBR)

63 64

Moving Bed Biofilm Reactor (MBBR)

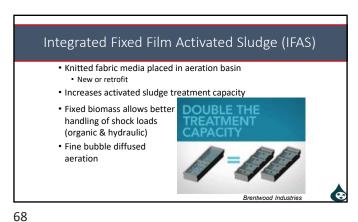


 No RAS flow & no backwash Can be put in anoxic and aerobic tanks to maximize BOD removal, denitrification and nitrification



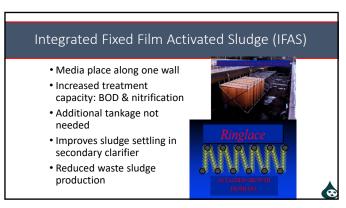
65 66





67 68





69 70



71

¹³⁶ Fixed Film

Attached Growth Vocabulary

1.	A mass or clump of organic material consisting of living organisms feeding on the wastes in wastewater, dead organisms, and other debris is referred to as
	Another name for this, used specifically when referring to trickling filters and RBCs, is
	, which is defined as the complex populations of organisms that
	form a slime growth on the media and break down the organic matter in wastewater. These slimes
	consist of living organisms feeding on the wastes in wastewater, dead organisms, silt, and other
	debris; "slime growth" is a more common term.
2.	A waste treatment process that is conducted under conditions means that
	atmospheric or dissolved oxygen is present in the aquatic environment. In contrast, an
	condition is one in which atmospheric or dissolved oxygen is <i>not</i> present
	in the aquatic environment.
3.	The rotating mechanism that distributes the wastewater evenly over the surface of a trickling filter or other process unit is called the
4.	The non-moving, cone-shaped spray nozzle used to distribute wastewater over the filter media,
	similar to a lawn sprinkling system, is called a A deflector or steel
	ball is mounted within the cone to spread the flow of water through the cone, thus creating a
	spraying action. This type of system is not as common as the rotary type and is commonly found
	only at small plants.
5.	The aerobic process in which bacteria change the ammonia and organic nitrogen in wastewater into oxidized nitrogen (usually nitrate) is called
6.	The sloughed off particles of biomass from trickling filter media that are removed from the water being treated in secondary clarifiers is referred to as
7.	Attached growth systems can be operated in two ways. When wastewater flows through one
	treatment unit and then flows through another similar unit, it is called
	If the wastewater is split and a portion flows to one
	treatment unit while the remainder flows to another similar treatment unit, this is called
^	
8.	A condition that occurs on trickling filters when the hollow spaces of media become plugged to the
	extent that water cannot pass through the filter is known as This may be the result of excessive slime growths, trash, or media breakdown.
9.	A method of increasing the efficiency of trickling filters is to add
	This is a process in which a part of the filter effluent is returned or recycled and brought into contact
	with the biological film once more.

10. The treatment process in which wastewater trickling over media enables the formation (aka slime growth) or biomass, which contains microorganisms that feed upon wastes from the water being treated, is called a	and remove
11. In a, two filters are used. Effluent from the first the second filter, either directly or after passing through a clarifier.	st filter goes to
12. The purpose of the is to carry the filtered wastewater lump (sloughed solids) from the filter to the final clarification process. In trickling fil supplied by natural draft or forced draft ventilation, the purpose of this system is to provide air flow to the filter to maintain aerobic conditions.	lters, air is
Word Bank	
Biomass	
Ponding	
Nitrification	
Parallel operation	
Two-stage filter	
Underdrain	
Fixed-spray nozzle	
Recirculation	
Aerobic	
Ventilation	
Trickling filter	
Distributor	
Series operation	
Zoogleal film	
Anaerobic	
Humus sludge	



Wastewater Technology Fact Sheet Trickling Filters

DESCRIPTION

Trickling filters (TFs) are used to remove organic matter from wastewater. The TF is an aerobic treatment system that utilizes microorganisms attached to a medium to remove organic matter from wastewater. This type of system is common to a number of technologies such as rotating biological contactors and packed bed reactors (biotowers). These systems are known as attached-growth processes. In contrast, systems in which microorganisms are sustained in a liquid are known as suspended-growth processes.

APPLICABILITY

TFs enable organic material in the wastewater to be adsorbed by a population of microorganisms (aerobic, anaerobic, and facultative bacteria; fungi; algae; and protozoa) attached to the medium as a biological film or slime layer (approximately 0.1 to 0.2 mm thick). As the wastewater flows over the medium, microorganisms already in the water gradually attach themselves to the rock, slag, or plastic surface and form a film. The organic material is then degraded by the aerobic microorganisms in the outer part of the slime layer.

As the layer thickens through microbial growth, oxygen cannot penetrate the medium face, and anaerobic organisms develop. As the biological film continues to grow, the microorganisms near the surface lose their ability to cling to the medium, and a portion of the slime layer falls off the filter. This process is known as sloughing. The sloughed solids are picked up by the underdrain system and transported to a clarifier for removal from the wastewater.

ADVANTAGES AND DISADVANTAGES

Some advantages and disadvantages of TFs are listed below.

Advantages

- C Simple, reliable, biological process.
- C Suitable in areas where large tracts of land are not available for land intensive treatment systems.
- C May qualify for equivalent secondary discharge standards.
- C Effective in treating high concentrations of organics depending on the type of medium used.
- C Appropriate for small- to medium-sized communities.
- Rapidly reduce soluble BOD₅ in applied wastewater.
- C Efficient nitrification units.
- C Durable process elements.
- C Low power requirements.
- C Moderate level of skill and technical expertise needed to manage and operate the system.

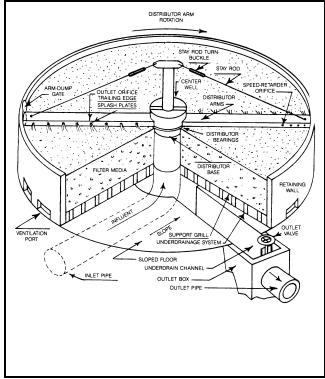
Disadvantages

- C Additional treatment may be needed to meet more stringent discharge standards.
- C Possible accumulation of excess biomass that cannot retain an aerobic condition and can impair TF performance (maximum biomass thickness is controlled by hydraulic dosage rate, type of media, type of organic matter, temperature and nature of the biological growth).
- C Requires regular operator attention.
- C Incidence of clogging is relatively high.
- C Requires low loadings depending on the medium.
- C Flexibility and control are limited in comparison with activated-sludge processes.
- C Vector and odor problems.
- C Snail problems.

DESIGN CRITERIA

A TF consists of permeable medium made of a bed of rock, slag, or plastic over which wastewater is distributed to trickle through, as shown in Figure 1. Rock or slag beds can be up to 60.96 meters (200 feet) in diameter and 0.9-2.4 meters (3 to 8 feet) deep with rock size varying from 2.5-10.2 cm (1 to 4 inches). Most rock media provide approximately 149 m²/m³ (15 sq ft/cu ft) of surface area and less than 40 percent void space. Packed plastic filters (bio-towers), on the other hand, are smaller in diameter (6 to 12 meters (20 to 40 feet)) and range in depth from 4.3 to 12.2 meters (14 to 40 feet). These filters look more like towers, with the media in various configurations (e.g., vertical flow, cross flow, or various random packings). Research has shown that cross-flow media may offer better flow distribution than other media, especially at low organic loads. When comparing vertical media with the 60 degree cross-flow media, the vertical media provide a nearly equal distribution of wastewater minimizing potential plugging at higher

organic loads better than cross flow media. The plastic medium also required additional provisions, including ultraviolet protective additives on the top layer of the plastic medium filter, and increased plastic wall thickness for medium packs that are installed in the lower section of the filter where loads increase.



Source: Metcalf & Eddy, Inc. and Tchobonaglous, 1998.

FIGURE 1 TYPICAL TRICKLING FILTER

The design of a TF system for wastewater also includes a distribution system. Rotary hydraulic distribution is usually standard for this process, but fixed nozzle distributors are also being used in square or rectangular reactors. Overall, fixed nozzle distributors are being limited to small facilities and package plants. Recently some distributors have been equipped with motorized units to control their speed. Distributors can be set up to be mechanically driven at all times or during stalled conditions.

In addition, a TF has an underdrain system that collects the filtrate and solids, and also serves as a source of air for the microorganisms on the filter. The treated wastewater and solids are piped to a

settling tank where the solids are separated. Usually, part of the liquid from the settling chamber is recirculated to improve wetting and flushing of the filter medium, optimizing the process and increasing the removal rate.

It is essential that sufficient air be available for the successful operation of the TF. It has been found that to supply air to the system, natural draft and wind forces are usually sufficient if large enough ventilation ports are provided at the bottom of the filter and the medium has enough void area.

The following four basic categories of filter design are based on the organic loading of the trickling filter.

Low-rate filters

Low-rate filters are commonly used for loadings of less than 40 kilograms five day biochemical oxygen demand (BOD₅)/100 meters cubed per day (25 lb BOD₅/1000cu ft/day). These systems have fewer problems than other filters with regards to filter flies, odors, and medium plugging because of the lower loading rate. Low-rate filters with a rock medium range in depth from 0.9 to 2.4 meters (3-8 ft.). Most low-rate filters are circular with rotary distributors, but some filters currently in use are rectangular. Both of these configurations are equipped with dosing syphons or periodic pumps to provide a high wetting rate for short intervals between rest periods. A minimum wetting rate of 0.4 liters per square meter-second (0.7 gal/sq ft/min) is maintained to prevent the high rate plastic filter medium from drying out. With a rock medium, the filters tend not to be hydraulically limited and have application limits ranging from 0.01 to 0.04 liters per square meter-second (0.02 to 0.06 gal/sq ft/min).

The sloughed solids from a low-rate filter are generally well-digested and as a result these filters yield less solids than higher rate filters. Secondary quality effluent is readily achievable if the low-rate trickling filter design incorporates filter media with bioflocculation capabilities or good secondary clarification.

Intermediate-rate filters

Intermediate rate filters can be loaded up to 64 kg BOD₅/100 m³-d (40 lb BOD₅/1000cu ft/day). In order to ensure good distribution and thorough blending of the filter and secondary effluent, the system should recirculate the trickling filter effluent. The biological solids that slough from an intermediate trickling filter are not as well digested as those using a low-rate filter.

High-rate filters

High-rate filters are generally loaded at the maximum organic loading capabilities of the filter and receive total BOD₅ loading ranging from 64 to 160 kg BOD₅/100 m³-d (40 to 100 lb. BOD₅/1000cu ft/day). Achieving a secondary quality effluent is less likely for a high-rate filter without a second-stage process. As a result, high-rate filters are often used with combined processes.

Roughing Filters

Roughing filters are designed to allow a significant amount of soluble BOD to bleed through the trickling filter. Filters of this type generally have a design load ranging from 160-480 kg BOD₅/100 m³-d (100 to 300 lb. BOD₅/1000cu ft/day).

PERFORMANCE

Recent efforts have been made to combine fixed-film reactors with suspended growth processes to efficiently remove organic materials from wastewater. For example, the combination of a trickling filter with an activated-sludge process has allowed for the elimination of shock loads to the more sensitive activated sludge while providing a highly polished effluent that could not be achieved by a trickling filter alone. Table 1 shows the BOD₅ removal rates for the four filter types discussed.

Although the TF process is generally reliable, there is still potential for operational problems. Some of the common problems are attributed to increased growth of biofilm, improper design, changing wastewater characteristics, or equipment failure. Some common problems with TF function are

discussed in the Operation and Maintenance section.

TABLE 1 BOD₅ REMOVAL RATES FOR VARIOUS FILTER TYPES

Filter Type	BOD ₅ Removal (%)
Low Rate	80 - 90
Intermediate Rate	50 - 70
High Rate	65 - 85
Roughing Filter	40 - 65

Source: Environmental Engineers Handbook, 1997.

OPERATION AND MAINTENANCE

Disagreeable Odors from Filter

Potential Cause: Excessive organic load causing anaerobic decomposition in filter.

Remedy: Reduce loading; increase BOD removal in primary settling tanks; enhance aerobic conditions in treatment units by adding chemical oxidants, preaerating, recycling plant effluent, or increasing air to aerated grit chambers; scrub off gases; use plastic media instead of rock.

Potential Cause: Inadequate ventilation.

Remedy: Increase hydraulic loading to wash out excess biological growth; remove debris from filter effluent channels, underdrains, and the top of filter media; unclog vent pipes; reduce hydraulic loading if underdrains are flooded; install fans to induce draft through filter; check for filter plugging resulting from breakdown of the medium.

Ponding on Filter Media

Potential Cause: Excessive biological growth or foreign matter in or on the filter.

Remedy: Reduce organic loading; increase hydraulic loading to increase sloughing; use high-pressure stream of water to flush filter surface; maintain 1 to 2 mg/L residual chlorine on the filter for several hours; flood filter for 24 hours; shut down filter to dry out media; replace media if necessary; remove debris.

Filter Flies (Psychoda)

Potential Cause Inadequate filter media moisture. Remedy: Increase hydraulic loading; unplug spray orifices or nozzles; use orifice opening at end of rotating distributor arms to spray filter walls; flood filter for several hours each week during fly season; maintain 1-2 mg/L residual chlorine on the filter for several hours

Potential Cause: Poor housekeeping.

Remedy: Mow area surrounding filter and remove weeds and shrubs.

Icing

Potential Cause: Low temperature of wastewater. Remedy: Decrease recirculation; use high-pressure stream of water to remove ice from orifices, nozzles, and distributor arms; reduce number of filters in service as long as effluent limits can still be met; reduce retention time in pretreatment and primary treatment units; construct windbreak or covers.

Rotating Distributor Slows Down or Stops

Potential Cause: Insufficient flow to turn distributor.

Remedy: Increase hydraulic loading; close reversing jets.

Potential Cause: Clogged arms or orifices. Remedy: Flush out arms by opening end plates; remove solids from influent wastewater; flush out orifices.

Potential Cause: Clogged distributor arm vent pipe.

Remedy: Remove material from vent pipe by rodding or flushing; remove solids from influent wastewater.

Potential Cause: Distributor arms not level. Remedy: Adjust guy wires at tie rods.

Potential Cause: Distributor rods hitting media. Remedy: Level media; remove some media.

Rotary distributors are very reliable and easy to maintain. A clearance of 15.2-22.9 centimeters (6-9 inches) is needed between the bottom of the distributor arm and the top of the medium bed to allow the wastewater from the nozzles to spread out and cover the bed uniformly. This also helps prevent ice from accumulating during freezing weather.

Care should be taken to prevent leaks. Follow the manufacturer's operation and maintenance (O&M) instructions on pumps, bearings, and motors. All equipment must be tested and calibrated as recommended by the equipment manufacturer. A routine O&M schedule should be developed and followed for any TF system. It is critical that a TF system be pilot tested prior to installation to ensure that it will meet effluent discharge permit requirements for that particular site.

Disagreeable Odors from Filter

- Excessive organic load causing anaerobic decomposition in filter—Reduce loading; increase BOD removal in primary settling tanks; enhance aerobic conditions in treatment units by adding chemical oxidants, preaerating, recycling plant effluent, or increasing air to aerated grit chambers; scrub off-gases; use plastic media instead of rock
- Inadequate ventilation—Increase hydraulic loading to wash out excess biological growth; remove debris from filter effluent channels, underdrains, and the top of filter media; unclog vent pipes; reduce hydraulic loading if underdrains are flooded; install fans to induce draft through filter; check for filter plugging resulting from breakdown of media.

Ponding on Filter Media

C Excessive biological growth—Reduce organic loading; increase hydraulic loading to increase sloughing; use high-pressure stream of water to flush filter surface (recycled water); maintain 1 to 2 mg/L residual chlorine on the filter for several hours; flood filter for 24 hours; shut down filter to dry out media; replace media if necessary; remove debris.

Filter Flies (Psychoda)

- C Inadequate moisture on filter media—Increase hydraulic loading; unplug spray orifices or nozzles; use orifice opening at end of rotating distributor arms to spray filter walls; flood filter for several hours each week during fly season; maintain 1 to 2 mg/L residual chlorine on the filter for several hours.
- C Poor housekeeping—Mow area surrounding filter and remove weeds and shrubs.

Icing

C Low temperature of wastewater—Decrease recirculation; use high-pressure stream of water to remove ice from orifices, nozzles, and distributor arms; reduce number of filters in service as long as effluent limits can still be met; reduce retention time in pretreatment and primary treatment units; construct windbreak or covers.

Rotating Distributor Slows Down or Stops

- C Insufficient flow to turn distributor—Increase hydraulic loading; close reversing jets.
- Clogged arms or orifices—Flush out arms by opening end plates; remove solids from influent wastewater; flush out orifices.
- Clogged distributor arm vent pipe—Remove material from vent pipe by rodding or flushing; remove solids from influent wastewater.
- C Distributor arms not level—Adjust guy wires at tie rods.
- C Distributor rods hitting media—Level media; remove some media.

Rotary distributors are very reliable and easy to maintain. A clearance of 15 to 23 cm (6 to 9 inches) is needed between the bottom of the distributor arm and the top of the media bed to allow the wastewater from the nozzles to spread out

and cover the bed uniformly. This also prevents ice from accumulating during freezing weather.

Care should be taken to prevent leaks. Follow the manufacturer's operation and maintenance (O&M) instructions on pumps, bearings, and motors. All equipment must be tested and calibrated as recommended by the equipment manufacturer. A routine O&M schedule should be developed and followed for any TF system. It is critical that a TF system be pilot tested prior to installation to ensure that it will meet effluent discharge permit requirements for that particular site.

COST

The cost for a TF system are summarized in Table 2. These costs include construction, labor, total O&M, and materials needed. Since every TF system is unique to its site, the overall cost will be site specific.

REFERENCES

Other Related Fact Sheets

Trickling Filter Nitrification EPA 832-F-00-015 September, 2000 Other EPA Fact Sheets can be found at the following web address:

http://www.epa.gov/owmitnet/mtbfact.htm

- 1. Liu and Liptak. 1997. Environmental Engineering Handbook. 2d ed. The CRC Press, LLC. Boca Raton Florida.
- 2. Martin, Edward J. and Edward T. Martin. Technologies for Small Water and Wastewater Systems. 1991. p. 122. New York, New York.
- 3. Metcalf & Eddy, Inc. 1991. Wastewater Engineering: Treatment, Disposal, and Reuse. 3d ed. The McGraw-Hill Companies. New York, New York.
- 4. Mulligan, T. J. and O. K. Scheible. 1990. Upgrading Small Community Wastewater Treatment Systems for Nitrification. HydroQual, Inc. Mahwah, New Jersey.
- 5. U.S. EPA, 1991. Assessment of Single-Stage Trickling Filter Nitrification. EPA 430/09-91-005, EPA Office of Municipal Pollution Control. Washington, D.C.
- 6. U.S. EPA, 1993. *Manual: Nitrogen Control*. EPA Office of Research and Development. EPA/625/R-93/010. Cincinnati, Ohio. EPA Office of Water. Washington, D.C.

TABLE 2 COST SUMMARY FOR A TRICKLING FILTER

Wastewater Flow (MGD)	Construction Cost (Millions of Dollars)	Labor (Millions of Dollars)	O&M (Millions of Dollars)	Materials (Millions of Dollars)
1	0.76	0.05	0.063	0.009
10	6.34	0.23	0.15	0.05
50	25	0.5	0.70	0.1
100	63.40	1.0	1.3	0.2

Source: Adapted from Martin and Martin, 1990.

7. Water Environment Federation (WEF). 1996. Operation of Municipal Wastewater Treatment Plants. Manual of Practice No. 11. 5th ed. vol. 2. WEF. Alexandria, Virginia.

ADDITIONAL INFORMATION

Tony Post, Plant Manager Central Wastewater Treatment 1020 Sargent Road Dallas, TX 75203

Jim Medlock, Operations Supervisor Littleton/Englewood Wastewater Treatment Plant 2900 South Platte River Drive Englewood, CO 80110

National Small Flows Clearing House at West Virginia University P.O. Box 6064 Morgantown, WV 26506

The mention of trade names or commercial products does not constitute endorsement or recommendation for use by the U.S. Environmental Protection Agency.

This fact sheet was developed in cooperation with the National Small Flows Clearinghouse whose services are greatly appreciated.

For more information contact:

Municipal Technology Branch U.S. EPA Mail Code 4204 1200 Pennsylvania Ave., NW Washington, D.C., 20460



CHAPTER 6

Fixed Film Reactors

6.1 <u>Trickling Filters</u>

- 6.1.1 General
- 6.1.2 Pretreatment
- 6.1.3 Types of Processes
- 6.1.4 Consideration For Design
- 6.1.5 Estimation of Performance
- 6.1.6 Special Details

6.2 <u>Rotating Biological Contactors</u>

- 6.2.1 General
- 6.2.2 Media
- 6.2.3 Design Loadings
- 6.2.4 Special Details

6.3 <u>Activated Biofilter</u>

- 6.3.1 General
- 6.3.2 ABF Media
- 6.3.3 Design
- 6.3.4 Special Details

FIXED FILM REACTORS

6.1 **Trickling Filters**

6.1.1 General

Trickling filters may be used for treatment of wastewater amenable to treatment by aerobic biological processes. This process is less complex and has a lower power requirement than some of the other processes.

6.1.2 Pretreatment

Trickling filters shall be preceded by effective clarifiers equipped with scum removal devices or other suitable pretreatment facilities. (See Chapters 4 & 5)

6.1.3 Types of Processes

Trickling filters are classified according to the applied hydraulic and organic loadings. The hydraulic loading is the total volume of liquid applied, including recirculation, per unit time per square unit of filter surface area. Organic loading is the total mass of BOD applied, including recirculation, per unit time per cubic unit of filter volume.

6.1.3.1 Low or Standard Rate

These are loaded at 1 to 4 million gallons per acre per day (mgad) and 5 to 25 pounds BOD per 1,000 cubic feet per day (lb BOD/1000 cu ft/day. Nitrification of the effluent often occurs.

6.1.3.2 Intermediate Rate

These are loaded at 4 to 10 mgad and 10 to 40 lb BOD/1000 cu ft/day. Nitrification is less likely to occur.

6.1.3.3 High Rate

These are loaded at 10 to 40 mgad and 25 to 300 lb BOD/1000 cu ft/day. Nitrification is not likely to occur.

6.1.3.4 Super Rate

These are loaded at 15 to 90 mgad (not including recirculation) and up to 300 lb BOD/1000 cu ft/day. Filters designed as super rate require a manufactured media. Nitrification is not likely to occur.

6.1.3.5 Roughing

These are loaded at 60 to 180 mgd (not including recirculation) and 100 lb BOD/1000 cu ft/day. Nitrification will not occur. Roughing filters shall be followed by additional treatment, and will be equipped with manufactured media.

6.1.4 Considerations for Design

The following factors should be considered when selecting the design hydraulic and organic loadings:

Characteristics of raw wastewater

Pretreatment

Type of media

Recirculation

Temperature of applied wastewater

Treatment efficiency required

The following table presents allowable ranges for the design of trickling filters. Modifications of these criteria will be considered on a case-by-case basis.

Design Loading Table					
	Low or			Super High Rate	
Operating	Standard	Intermediate		Manufactured	
Characteristics	Rate	Rate	High Rate	Media	Roughing
Hydraulic					
Loading					
Mgd/acre	1-4	4-10	10-40	15-90	60-180*
gpd/ sq ft	25-90	90-230	230-900	350-2000*	1400-4200*
Organic Loading					
lb BOD/acre-ft					
day			1000-		
1b	200-1000	700-1400	12,000		
BOD/1000ft3/day	5-25	10-40	25-300	Up to 300	100+
Depth ft	5-10	4-8	3-6	3-8	15-40
BOD Removal %	80-85	50-70	65-80	65-85	40-65
*does not include recirculation					

6.1.5. Estimation of Performance

A number of equations are available for use in estimating trickling filter performance.

Any design should evaluate several different formulas to compare the various parameters in different combinations with one another. Winter operating

conditions must be analyzed since winter operations normally result in lower efficiency than summer operations. The trickling filter design must evaluate the impacts of recirculation, air draft temperatures and medium.

6.1.5.1 Recirculation

Recirculation capability is required for all variations of the trickling filter process except roughing filters <u>provided</u> that minimum hydraulic loading rates are maintained at all times. The recirculation ratio should be in the range of 0.5 to 4.0. Recirculation should be provided for manufactured media to maintain 0.5 to 1.0 gallon per minute per square foot (gpm/sq ft) or the manufacturer's recommended minimum wetting rate at all times. Recirculation ratios greater than 4.0 should not be used to calculate effluent quality.

6.1.5.2 Staging

Staging of filters can be considered for high-strength wastes or for nitrification.

6.1.6 Special Details

6.1.6.1 Media

a.Rock, Slag, or Similar Media

Rock, slag, and similar media should not contain more than 5 percent by weight of pieces whose longest dimension is three times the least dimension. They should be free from thin, elongated and flat pieces, dust, clay, sand, or fine material and should conform to the following size and grading when mechanically graded over a vibrating screen with square openings:

Passing 4-1/2 inch screen: 100 percent by weight

Retained on 3-inch screen: 90-100 percent by weight

Passing 2-inch screen: 0-2 percent by weight

Passing 1-inch screen: 0 percent by weight

Hand-picked field stone should be as follows:

Maximum dimension of stone: 5 inches

Minimum dimension of stone: 3 inches

Material delivered to the filter site should be stored on wood-planked or

other approved clean hard-surfaced areas. All material should be rehandled at the filter site, and no material should be dumped directly into the filter. Crushed rock, slag, and similar media should be rescreened or forked at the filter site to remove all fines. Such material should be placed by hand to a depth of 12 inches above the tile underdrains, and all materials should be carefully placed so as not to damage the underdrains. The remainder of the material may be placed by means of belt conveyors or equally effective methods approved by the engineer. Trucks, tractors, or other heavy equipment should not be driven over the filter during or after construction.

b.Manufactured Media

Application of manufactured media should be evaluated on a case-by-case basis. Suitability should be evaluated on the basis of experience with installations handling similar wastes and loadings.

Media manufactured from plastic, wood, or other materials are available in many different designs. They should be durable, resistant to spalling or flaking, and relatively insoluble in wastewater. They are generally applied to super high rate and roughing filter designs.

6.1.6.2 Underdrainage System

a. Arrangement

Underdrains with semicircular inverts or equivalent should be provided and the underdrainage system should cover the entire floor of the filter. Inlet openings into the underdrains should have an unsubmerged gross combined area equal to at least 15 percent of the surface area of the filter.

b.Slope

The underdrains should have a minimum slope of 1 percent. Effluent channels should be designed to produce a minimum velocity of 2 feet per second at average daily rate of application to the filter.

c.Flushing

Provision should be made for flushing the underdrains and effluent channel.

In small filters, use of a peripheral head channel with vertical vents is acceptable for flushing purposes. Inspection facilities should be provided.

d.Ventilation

The underdrainage system, effluent channels, and effluent pipe shall be designed to permit free passage of air. The size of drains, channels, and pipe should be such that not more than 50 percent of their cross-sectional area will be submerged under the design hydraulic loading. Provision should be made in the design of the effluent channels to allow for the possibility of increased hydraulic loading.

6.1.6.3 Dosing Equipment

a.Distribution

The sewage shall be distributed over the filter by rotary distributors or other suitable devices which will permit reasonably uniform distribution to the surface area. At design average flow, the deviation from a calculated uniformly distributed volume per square foot of the filter surface should not exceed plus or minus 10 percent at any point. Provisions must be made to spray the side walls to avoid growth of filter flies.

b.Application

Sewage may be applied to the filters by siphons, pumps, or by gravity discharge from preceding treatment units when suitable flow characteristics have been developed. Application of sewage should be practically continuous. Intermittent dosing shall only be considered for low or standard rate filters. In the case of intermittent dosing, the dosing cycles should normally vary between 5 and 15 minutes, with distribution taking place approximately 50 percent of the time. The maximum rest should not exceed 5 minutes, based on the design average flow.

c. Hydraulics

All hydraulic factors involving proper distribution of sewage on the filters should be carefully calculated. For reaction-type distributors, a minimum head of 24 inches between the low-water level in the siphon chamber and center of the arms should be required. Surge relief to prevent damage to distributor seals, should be provided where sewage is pumped directly to the distributors.

d. Clearance

A minimum clearance of 6 inches between medium and distributor arms should be provided. Greater clearance is essential where icing occurs.

e. Seals

The use of mercury seals is prohibited in the distributors of newly constructed trickling filters. If an existing treatment facility is to be modified, any mercury seals in the trickling filters shall be replaced with oil or mechanical seals.

6.1.6.4 Recirculation Pumping

Low-head, high-capacity pumps are generally used. Submersible pumps are commonly used. A means to adjust the flow is recommended in order to maintain constant hydraulic operation.

6.1.6.5 Waste Sludge Equipment

Pumps for trickling filter sludge should be capable of pumping material up to 6-percent solids (or more if needed) when pumping directly to the digester. Time clock controlled on-off control is desirable. When secondary sludge is pumped to the primary clarifier, the sludge pumps should be designed to pump material with low solid concentrations and high flow rates.

6.1.6.6 Miscellaneous Features

a. Flooding

Consideration should be given to the design of filter structures so that they may be flooded.

b. Maintenance

All distribution devices, underdrains, channels, and pipes should be installed so that they may be properly maintained, flushed, or drained.

c. Flow Measurement

A means shall be provided to measure recirculated flow to the filter.

6.2 Rotating Biological Contactors

6.2.1 General

6.2.1.1 Description

This section presents the requirements for fixed-film reactors using either partially submerged vertical media rotated on a horizontal shaft or other designs with similar concepts.

January 2016 6-7 Design Criteria Ch. 6

6.2.1.2 Applicability

Rotating biological contactors (RBC) may be used for treatment of wastewater amenable to treatment by aerobic biological processes. The process is especially applicable to small communities. These requirements shall be considered when proposing this type of treatment.

6.2.1.3 Pretreatment

Primary clarifiers or fine screens should be placed ahead of the RBC process to minimize solids settling in the RBC tanks. (See Chapters 4 & 5)

6.2.2 Media

6.2.2.1 Description

Typical media consists of plastic sheets of various designs with appropriate spacings to maximize the surface area, allow for entrance of air and wastewater, the sloughing of excess biological solids and prevention of plugging. The medium is mounted on a horizontal steel shaft. Other similar systems will be considered on a case-by-case basis.

6.2.2.2 Types

Two types of medium are currently available.

a. Standard Density

Standard-density medium is available in sizes up to 100,000 square feet (sq ft) per shaft. It should be used for all secondary treatment applications.

b. High Density

High-density medium is available in sizes up to 150,000 sq ft per shaft. It should be used only for nitrification or effluent polishing where the influent BOD is sufficiently low to ensure that plugging of the medium will not occur.

6.2.3 Design Loadings

6.2.3.1 RBC Media

Design loadings should be in terms of total organic loading expressed as pounds BOD₅ per day per 1000 square feet of media surface area (lb BOD₅/day/1000 sq. ft.). The development of design loadings should consider influent BOD, soluble BOD, effluent BOD, flows, temperature, and the number of treatment stages. The design loading should generally range between 2.5 and 3.5 lb BOD₅/day/1000 sq. ft.

6.2.3.2 Final Clarifiers

The following requirements are in addition to those set forth in Chapter 5, "Clarifiers."

The overflow rate should be less than or equal to 600 gpd/sq ft at the average daily design flow.

6.2.4 Special Details

6.2.4.1 Enclosures

Enclosures should be provided for the RBC medium to prevent algae growth on the medium and minimize the effect of cold weather. Enclosures may be either fabricated individual enclosures or buildings enclosing several shafts. Buildings may be considered for installations with several shafts or, where severe weather conditions are encountered, to promote better maintenance.

a. Fabricated Individual Enclosures

Enclosures should be made of fiberglass or other material resistant to damage from humidity or corrosion. The exterior of the enclosures should be resistant to deterioration from direct sunlight and ultraviolet radiation. Access points should be provided at each end of the enclosure to permit inspection of shafts and to perform operation and maintenance. Enclosures shall be removable to allow removal of the shaft assemblies. Access around enclosures shall be sufficient to permit suitable lifting equipment access to lift covers and shafts.

b. Buildings

Adequate space should be provided to allow access to and removal of shafts from enclosures. Buildings should be designed with provisions to remove shafts without damage to the structure. Buildings should be designed with adequate ventilation and humidity control to ensure adequate atmospheric oxygen is available for the RBC shafts, provide a safe environment for the operating staff to perform normal operation and maintenance, and minimize the damage to the structure and equipment from excess moisture.

6.2.4.2 Hydraulic Design

The RBC design should incorporate sufficient hydraulic controls, such as weirs, to ensure that the flow is distributed evenly to parallel process units. RBC tank design should provide a means for distributing the influent flow evenly across each RBC shaft. Intermediate baffles placed between treatment stages in the RBC system should be designed to minimize solids deposition. The RBC units should be designed with flexibility to permit series or parallel operation.

6.2.4.3 Dewatering

The design should provide for dewatering of RBC tanks.

6.2.4.4 Shaft Drives

The electric motor and gear reducer should be located to prevent contact with the wastewater at peak flow rates.

6.2.4.5 Recycle

Effluent recycle should be provided for small installations where minimum diurnal flows may be very small. Recycle should be considered in any size plant where minimum flows are less than 30% of the average design flow.

6.2.4.6 Access

Access shall be allowed for lifting equipment to provide maintenance in the event of a failure.

6.3 Activated Biofilter

6.3.1 General

6.3.1.1 Description

The activated biofilter (ABF) process is a combination of the trickling filter process using artificial media and the activated sludge process.

6.3.1.2 Applicability

The activated biofilter process may be used where wastewater is amendable to biological treatment. This process requires close attention and competent operating supervision, including routine laboratory control. These requirements should be considered when proposing this type of treatment. The process is more adaptable to handling large seasonal loading variations, such as those resulting from seasonal industries or changes in population, than are some of the other biological processes. Where significant quantities of industrial wastes are anticipated, pilot plant testing should be considered.

6.3.2 ABF Media

Artificial media are used in the trickling filter portion of the process to allow high BOD and hydraulic loadings and permit recycle of activated sludge through the trickling filter without plugging. Either wood or plastic artificial medium may be used. Medium depth typically ranges from 7 to 25 feet.

6.3.3 Design

6.3.3.1 General

Calculations shall be submitted to justify the basis of design of the ABF tower pump station, ABF tower, aeration basin, aeration equipment, secondary clarifiers, activated sludge return equipment, and waste sludge equipment.

6.3.3.2 ABF Tower Pump Station

The ABF tower pump station shall be designed to pump the peak influent flow plus the maximum design ABF tower recirculation and return activated sludge flows. Application of wastewater to the ABF tower should be continuous.

January 2016 6-11 Design Criteria Ch. 6

6.3.3.3 ABF Tower

The ABF tower shall be designed based on organic loading expressed as pounds of influent BOD per 1,000 cubic feet per day (lb BOD/1,000 cu ft/day). The organic loading should be established using data from similar installations or pilot plant testing. A minimum hydraulic wetting rate should be maintained and be expressed as gallons per minute per square foot (gpm/sq ft).

Typical values for organic loading range from 100 to 350 lb BOD/1,000 cu ft/day (4,300 to 15,000 pounds BOD per acre-foot per day), and hydraulic wetting rates range from 1.5 to 5.5 gpm/sq ft, including recirculations and return flows.

6.3.3.4 Aeration Basin

The aeration basin should be designed in accordance with Chapter 7, "Activated Sludge," based on the food-to-microorganism (F/M) ratio expressed as pounds of influent BOD per day per pound of mixed liquor volatile suspended solids (MLVSS). The F/M ratio should be based on the influent total BOD to the ABF tower or the estimated soluble BOD leaving the ABF tower. Designs using total BOD to the ABF tower should be based on data from similar installations or pilot plant testing. Designs using the estimated soluble BOD leaving the ABF tower should use typical F/M ratios (presented in Chapter 7, "Activated Sludge"). Estimate of BOD removal in the ABF tower should be based on similar installations or pilot plant testing. Calculations of mixed-liquor suspended solids should include the influent suspended solids and solids sloughing from the ABF tower in addition to growth of activated sludge due to removal of soluble BOD. Determination of aeration basin volume should include consideration of aeration basin power levels (using aeration equipment horsepower) expressed as horsepower per 1,000 cubic feet of basin Aeration basin power levels should be limited to prevent volume. excessive turbulence, which may cause shearing of the activated sludge floc. Aeration prior to the ABF tower may also be considered.

6.3.3.5 Aeration Equipment

Oxygen requirements should be estimated as outlined in Chapter 7, "Activated Sludge," for the ABF tower effluent plus the oxygen requirements of the sloughed solids from the ABF tower.

6.3.3.6 Secondary Clarifiers

Secondary clarifiers should be equipped with rapid sludge withdrawal mechanisms and be designed in accordance with Chapter 5, "Clarifiers," and Chapter 7, "Activated Sludge."

6.3.3.7 Return Sludge Equipment

Return sludge equipment should be designed in accordance with Chapter 5, "Clarifiers."

6.3.3.8 Waste Sludge Equipment

Waste sludge equipment should be designed in accordance with Chapter 12, "Sludge Processing and Disposal."

6.3.3.9 ABF Tower Recirculation

ABF tower recirculation should normally be provided. At a minimum, recirculation capacity should meet the requirements for the minimum hydraulic wetting rate.

6.3.4 Special Details

6.3.4.1 ABF Tower

The ABF tower dosing equipment and underdrainage system should be designed in accordance with Section 6.1.6.3 "Dosing Equipment." Fixed or rotating distributors may be used. In addition, the design of the ABF tower should incorporate a skirt around the top to prevent spray from falling to the ground around the tower.

6.3.4.2 Maintenance Provisions

All distribution devices, underdrains, channels, and pipes should be installed so that they may be properly maintained, flushed, and drained.

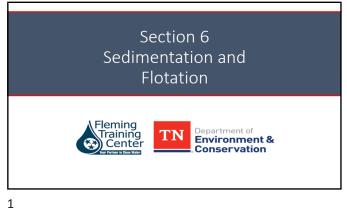
6.3.4.3 Flow Measurement

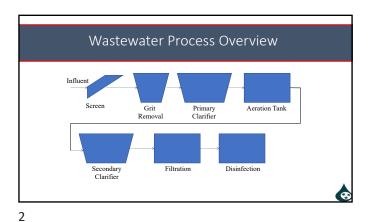
Devices should be provided to permit measurement of flow to the ABF towers, ABF tower recirculation, return activated sludge, and waste activated sludge flows.

Section 6 Sedimentation and Flotation









Sedimentation & Flotation

- Raw or untreated wastewater contains materials (solids) that easily settle to the bottom or float to the surface when the velocity is slowed
- Collection systems are designed to maintain a certain velocity (2 ft/sec) to keep solids from settling out
- In primary clarifier, velocity slowed to 1 − 2 ft/min

3

Note **Flotation** = The process of raising suspended matter to the surface of the liquid in a tank where it forms a scum layer that can be removed by skimming. The suspended matter is raised by aeration, gas, chemicals, electrolysis, heat, or bacterial decomposition Sedimentation = The process of settling and depositing of suspended matter carried by water or wastewater. Usually occurs by gravity when the velocity of the liquid is reduced below the point at which it can transport the suspended material.

4

6

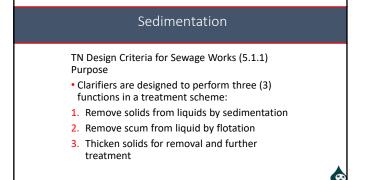
Sedimentation and Flotation

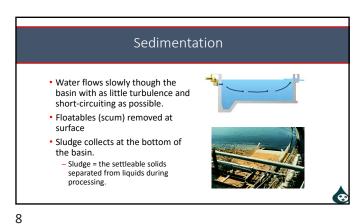
Sedimentation

- · Settling of solids out of suspension due to gravity.
 - Suspended particles include clay, silt, particles in natural state or modified by treatment (biological floc/sloughings)
- Occurs in a rectangular, square or round basin.

Sedimentation Other common names: -Sedimentation and floatation unit -Settling tank -Sedimentation tank –Clarifier • Primary (1°) Clarifier = comes after preliminary treatment and • Secondary (2°) Clarifier (can also be called Final Clarifier) = follows treatment, usually found after biological process

7





Factors Affecting Sedimentation

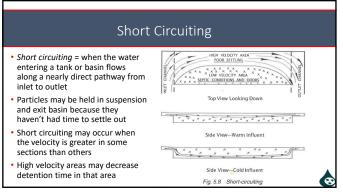
• Temperature
• Short circuits
• Detention time**
• Weir overflow rates**
• Surface loading rate**

• Surface loading rate**

**Mathematical ways to check clarifier performance

As water temperature increases, the settling of particles increases.
As the water temperature decreases, so does the settling rate.

9



Short Circuiting

Can be prevented by weir plates, port openings and proper design of the inlet channel

Different layers with different temperatures can cause short-circuiting when a warm influent flows across the top of cold water and vise-versa

Can be prevented by weir plates, port openings and proper design of the inlet channel

11 12

Detention Time

- Wastewater should remain in the clarifier long enough to allow sufficient time for solid particles to fall or settle out
- Detention times are usually 2.0 to 3.0 hours
- The efficiency of a clarifier depends on the velocity and the detention time

Detention Time

- Detention $Time = \frac{Volume}{Flow}$
- DT, hrs = (Volume of Tank, gal)(24)
 Flow, gpd
- The formula will calculate theoretical detention time, actual detention time is often less and measured by the use of dyes, tracers, or floats

13

14

Weir Overflow Rate

- The number of gallons of wastewater that flow over one lineal foot of weir per day
 - -Lineal = the length in one direction of a line
- The number of lineal feet of weir in relation to flow is important to prevent short circuiting or high velocities (which could pull settled solids into the effluent)

Weir overflow rate =
$$\frac{\text{Flow rate, GPD}}{\text{Weir length, ft}}$$

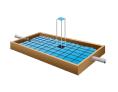
_ .

Surface Loading Rate

- · Also called Surface Overflow Rate
- The number of gallons going through the settling tank each day for each square foot of surface area in the tank
- Also defined as the loading across the surface of your
- settling tank

 Depends on the nature of the solids and the treatment





15

16

Solids Loading Rate

- "Solids Loading" refers to the amount of solids removed daily by a clarifier for each ft² of clarifier liquid surface area
- Expressed in pounds per day per ft² (lbs/day/ft²)
- Depend on the nature of the solids and treatment requirements
- $SLR = \frac{\left(Solids\ Applied, lbs/_{day}\right)}{\left(Surface\ area,\ ft^2\right)}$
- If solids loading goes above design criteria, you could expect an increase in effluent solids

Primary Clarifiers

- Immediately follows preliminary treatment
- First clarifier in plant
 - *TN Design Criteria 6.1.2 Pretreatment: "Trickling filters shall be preceded by effective clarifiers equipped with scum removal devices or other suitable pretreatment facilities."
- Some plants don't have one
- Most important function: to remove as much settleable and floatable material as possible

17

ft/min

Sludge tends to be more dense The primary clarifier settled sludge is wasted to the digesters, which puts a tremendous load of untreated volatile organic food to the digester. If there is an excessive dissolved oxygen drop across the primary clarifier, the sludge wasting rate should be increased.

Primary Clarifiers

• Long detention times cause:

- Solids to become septic

- Solids to float to the surface

- High suspended solids level in primary effluent

- Odors in primary effluent

• A good example of normal operation is:

- Sludge collectors running constantly

- Raw sludge pump runs for 10 minutes each hour

- At start of pumping cycle, raw sludge has 7% solids and at the end has 5% solids

- Tank and floor has a moderate sludge blanket

19 20

	rinnar	<i>r</i> Clarifiers
Water Quality Indicator	Expected Removal Efficiency	
Settleable Solids	95 – 99 %	
Suspended Solids	40 – 60 %	
Total Solids	10 – 15 %	
BOD	20 – 50 %	Note: Soluble BOD cannot be
Bacteria	25 – 75 %	removed by primary clarifiers.

Primary Clarification

Scum to Solids
Handling Process

Influent from screens and/or grit removal system

Primary Clarifier

Effluent to aeration tank
Primary sludge to solids handling process

21

• Usually located after a biological process - Activated Sludge, Trickling Filters, Rotating Biological Contactors • Purpose: to remove the additional solids (and microorganisms) created during the biological treatment • Cleaner effluent than primary effluent • Must remove enough solids from bottom before they becomes septic or gasification occurs

Trickling Filter Clarifiers

• Settles out "sloughings"

— Slime washed off the filter media

— Quite high in BOD and will lower the effluent quality unless it is removed

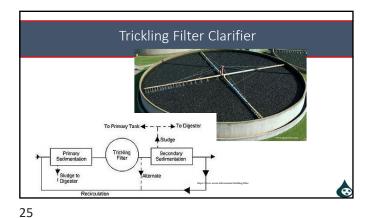
• Loading rates for secondary clarifiers used after trickling filters:

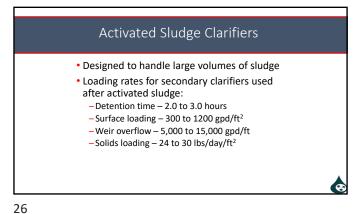
— Detention time – 2.0 to 3.0 hours

— Surface loading – 800 to 1200 gpd/ft²

— Weir overflow – 5,000 to 15,000 gpd/ft

23 24





• RAS to aeration tank & WAS to solids handling - The pumps used to remove sludge from these clarifiers are usually centrifuge type with variable-speed controls or large airlift type. - RAS rates can range from 15-150% of the plant influent flow - If return rates are too high, turbulence in the tank can upset the sludge blanket.

During a period of high flow caused by rain fall or periods of hydraulic overloading, operators should decrease WAS
 This will retain the microorganisms in the aeration basins for a quicker recovery if there is a washout.

 Hydraulic flow variations will have the most severe impact upon the activated sludge process.

27

SVI indicates settleability:

- SVI>100: light, fluffy; cone shaped blanket

- SVI<100: more dense; bell shaped blanket

- Desirable: 50-150 mL/g

Fig. 5.12 Activated sludge setting near center olge of clarifier (book-shaped pathern)

Fig. 5.13 Activated sludge setting near center origin of clarifier (book-shaped pathern)

Fig. 5.13 Activated sludge setting near center origin of clarifier (book-shaped pathern)

Fig. 5.13 Activated sludge setting near center origin of clarifier (book-shaped pathern)

Fig. 5.13 Activated sludge setting near center origin of clarifier (book-shaped pathern)

Fig. 5.13 Activated sludge setting near center origin of clarifier (book-shaped pathern)

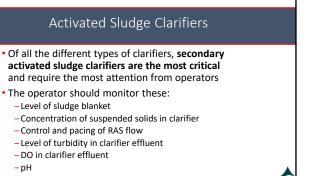
• SVI stands for Sludge Volume Index

This Is a process control parameter to describe the settling characteristics of sludge in the aeration tank in Activated Sludge Process

It is used to determine the recycle rate of sludge

29 30

165



Gasification

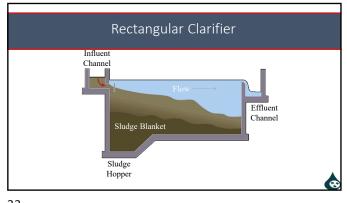
• Indication of sludge septicity

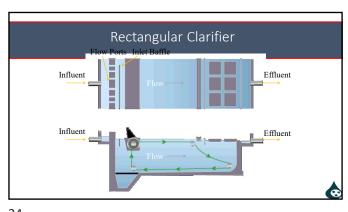
- Make sure accumulated settled solids are removed from bottom of clarifier before septicity and gasification take place

• Do not confuse with Denitrification -nitrogen gas bubbles rising to surface

- Secondary Clarifiers

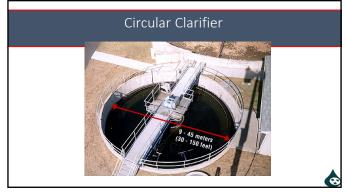
31 32

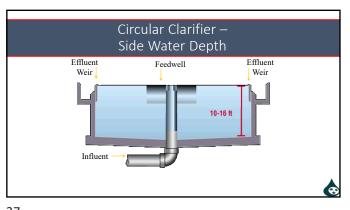


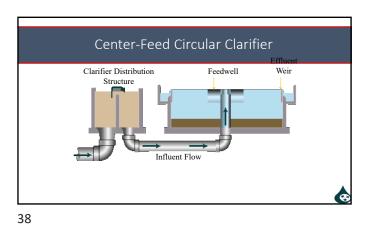


33

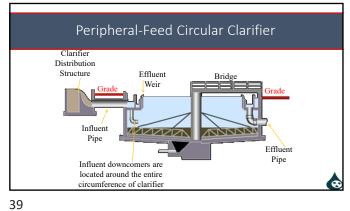






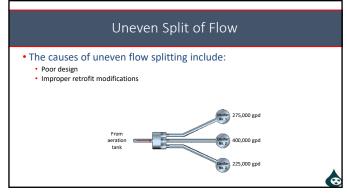


37

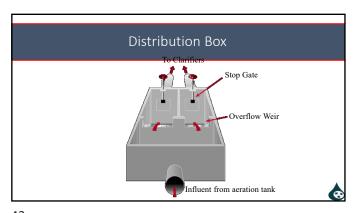


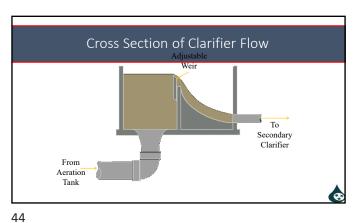






41





43

Plotation Processes

After 1° clarification, some suspended solids that neither settle not float always remain

Colloids and emulsions are two forms of solids that are difficult to remove by sedimentation

Colloids are very small, finely divided solids that remain dispersed in liquid for a long time

An emulsion is a liquid mixture of two or more liquid substances not normally dissolved in one another

Usually grease, oil or fat

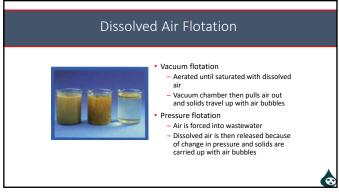
Pumping air into mixture of emulsions and colloids to cause suspended material to float to surface where it can be skimmed off

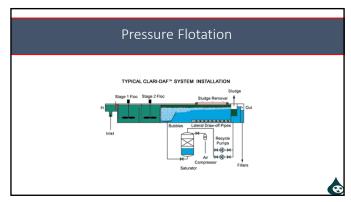
• Flocculation = gathering together of fine particles after coagulation to form larger particles, clumping makes it easier to separate solids from water

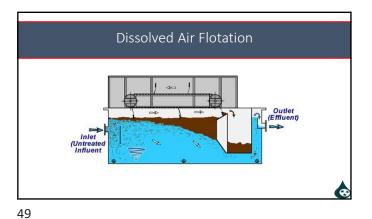
• Particles flocculated with air or coagulants and carried to surface by air bubbles

— Coagulant = a chemical that causes very fine particles to clump (floc) together into larger particles

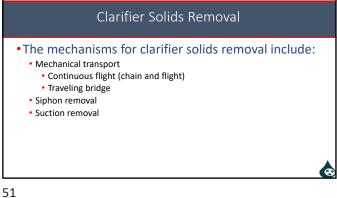
45 46



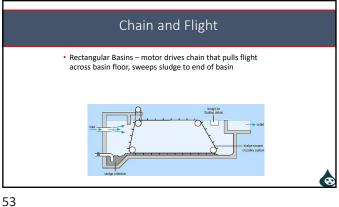


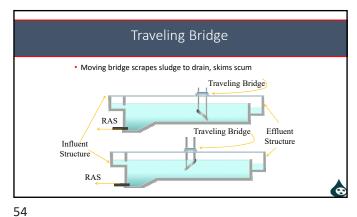


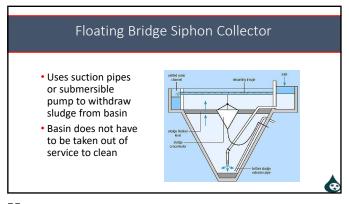
Factors Affecting DAFs Type of sludge: heavier primary sludges harder to treat · Age of feed sludge: older sludges float more readily Solids loading: 10-24 lbs/day/ft² • Hydraulic loading: 0.5-1.5 gpm/ft² • Air to solids ratio: 0.01-0.10 lb/lb Recycle rate: 100-200% • Blanket depth: decreasing scraper speed concentrates sludge

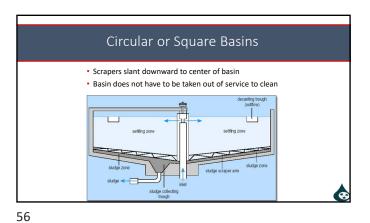




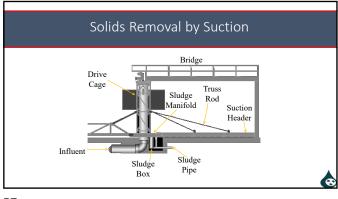


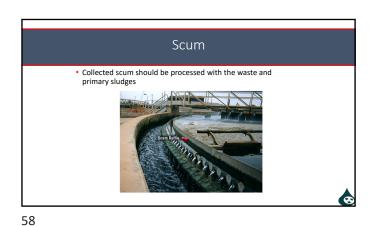






55

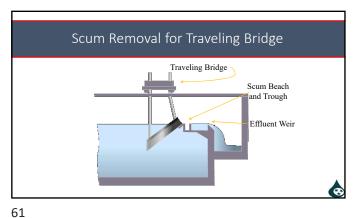




57





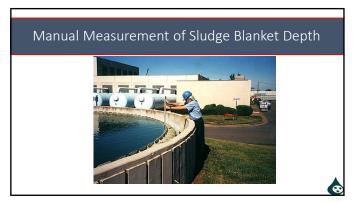


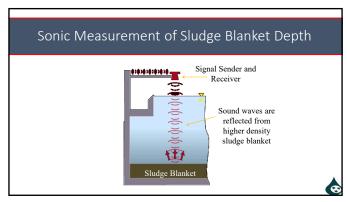
Clarifier Monitoring Clarifier monitoring and control systems include sludge blanket monitoring and drive mechanism torque control. The continuous data being provided by these systems are very useful for process control.

Clarifier Monitoring Sludge blanket levels Suspended solids concentration in clarifier effluent Control of return sludge flows • Turbidity in clarifier effluent • DO levels in clarifier effluent • pH

Monitoring the Process · Primary clarifier: Imhoff cone Secondary clarifier: Settleometer; centrifuge spins Turbidity test also · Visually checking for floc carry-over Visual check of how far floc particles are visible from inlet

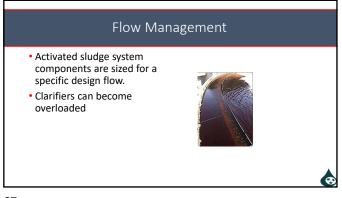
64 63

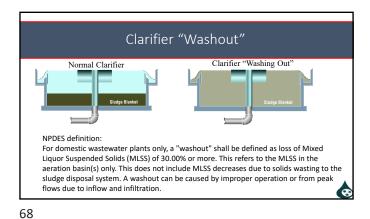




65 66

171





67

Operators need to minimize the impacts of peak flows on plant performance.

Peak Flows

Francisco

Franci

Flow Management

Operators must use:

-Past history;

• "March snow melts"

• "August thunderstorms"

-Weather forecasts

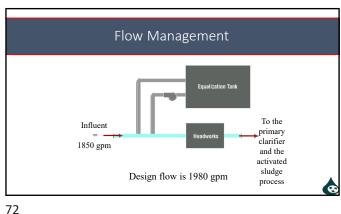
• "Hurricane Henry to hit"

to help them predict when high flows may occur.

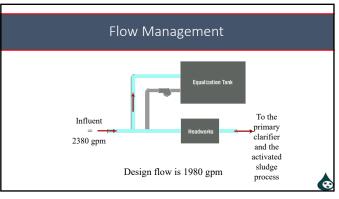
69

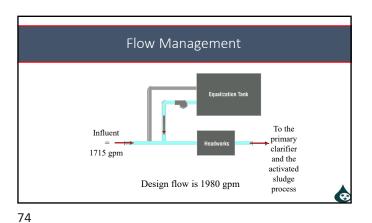
Flow Management
High flows can be managed by using:

Flow-equalization basins
Storage lagoons
Alternate process modes such as contact stabilization or step feed.



71





73

Some plants have storage lagoons for wet weather flows.

Stored wastewater is pumped to the head of the plant when flow rates decrease.

A chain-and-flight system consists
of 2 continuous parallel loops of

A. True
B. False

75

A chain-and-flight system consists
of 2 continuous parallel leans of

A. True

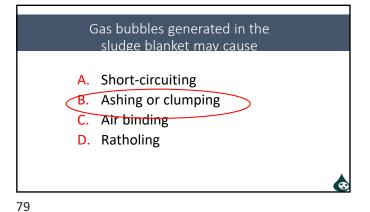
B. False

Gas bubbles generated in the sludge blanket may cause

A. Short-circuiting
B. Ashing or clumping
C. Air binding
D. Ratholing

77

78



Primary clarifiers are capable of removing 100% of the influent TSS

A. True
B. False

Primary clarifiers are capable of removing 100% of the influent TSS

A. True

B. False

Primary Clarifiers can only remove the settleable portion of TSS and BOD

A facility has 3 secondary clarifiers. Sludge blanket depts are1 ft, 1.2 ft, and 3 ft. What

A. Sludge is being removed faster from 3rd clarifier
B. The RAS pump on the 1st clarifier has failed
C. Uneven flow distribution feeding the clarifiers
D. WAS is only being removed from the 2nd clarifier

A facility has 3 secondary clarifiers. Sludge blanket depts are1 ft,
1.2 ft, and 3 ft. What is the most likely cause for the
differences?

A. Sludge is being removed faster from 3rd clarifier
B. The RAS pump on the 1rd clarifier has failed
Uneven flow distribution feeding the clarifiers

Hydraulic detention time can be

A. True

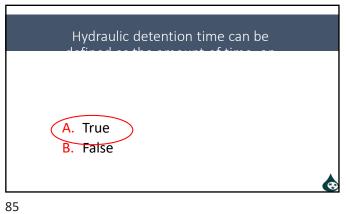
B. False

WAS is only being removed from the 2nd clarifier

83

81

80





<u>Sedimentation and Flotation Vocabulary</u>

1.	The particles that settle to the floor of a clarifier are called
2.	is the term used to describe the clouds of billowing sludge that
	occur throughout secondary clarifiers when the sludge does not settle properly.
3.	Sludge in primary clarifiers must be removed at regular intervals to prevent the sludge from turning
4.	is the gathering together of fine particles after coagulation
	to form larger particles by a process of gentle mixing. This clumping together makes it easier to separate the solids from the wastewater by settling, skimming, draining, or filtering.
5.	Large clumps of sludge floating to the surface of the water in a primary clarifier would indicate is occurring due to anaerobic decomposition.
6.	A chemical that causes very fine particles to clump or floc together into larger particles is a This makes it easier to separate the solids from the liquids by
	settling, skimming, draining, or filtering. They can be used as part of the flotation process.
7.	The clarifier that follows other types of treatment, usually a biological reactor, is the
	Its main function is to remove the additional solids that were converted to settleable form in the treatment processes that followed the primary clarifier.
8.	is a condition that occurs in tanks or basins when the velocity
	of water flow is greater in some sections than in others. This is an undesirable situation since it may result in shorter contact time, detention times, reaction times, or settling rates.
9.	Simply put, is defined as the hydraulic loading across the
	surface of your settling tank.
10.	
	remain dispersed in a liquid for a long time due to their small size and electrical charge. DAF systems are designed to remove these particulates from wastewater.
11.	refers to the amount of solids removed daily by a
	clarifier for each square foot (ft ²) of clarifier liquid surface area.
12.	Wastewater must remain in a clarifier long enough to allow sufficient time for particles to settle out. On average, the is 2-3 hours for a settling tank.
13.	Scraper boards made from rot-resistant wood or plastic that are used to collect and move settled sludge or floating scum are called

14. T	he anoxic process of nitrite	or nitrate ions being reduce	ed to nitrogen gas and producing		
n	itrogen bubbles is called		This condition can lead to		
			bles attaching to the biological floc and		
fl	oating the floc to the surfac	e.			
			d to control flow from settling tanks and		
С	larifiers to ensure a uniform	flow rate and avoid short-o	circuiting.		
16. D	Defined as the number of gallons of wastewater that flow over one lineal foot of weir per day,				
tl	ne	is gener	rally lower in secondary clarifiers than in		
р	rimary clarifiers.				
17. T	he first clarifier in the plant	that comes immediately aft	ter preliminary treatment (bar screen,		
C	omminutor, or grit channel)	is the	Its main function		
is	to remove settleable and f	loatable solids.			
18. S	edimentation tank effluent	troughs consisting of overfl	ow weir plates are called		
19. T	he	is a calculation	that indicates the tendency of activated		
sl	ludge solids to thicken or be	ecome concentrated during	the sedimentation/thickening process.		
20. T	he	process involves	s pumping air into wastewater to cause		
	ne suspended solids to adhe ff.	ere to bubbles and float to t	he surface, where they can be skimmed		
21. T	he slime that is washed off	the filter media in a trickling	g filter, which is generally quite high in		
В	OD, is called				
Word Ba	<u>nk:</u>				
Chart size	witing	Cludge Volume Index (CVII)	[lights		
Short circ	urung	Sludge Volume Index (SVI)	Flights		
Bulking		Colloids	Primary clarifier		

Woı

Bulking	Colloids	Primary clarifier
Launders	Secondary clarifier	Septic
Coagulant	Sludge	Weir overflow rate
Flotation	Weir	Solids loading rate
Flocculation	Sloughings	Sludge gasification
Denitrification	Surface loading rate	Detention time (aka Retention Time)

CHAPTER 5

Clarifiers

5.1	General	Critoria
J.1	General	Ciliciia

- 5.1.1 Purpose
- 5.1.2 Number of Units
- 5.1.3 Arrangements
- 5.1.4 Tank Configurations
- 5.1.5 Flow Distribution

5.2 <u>Design Loading</u>

- 5.2.1 Primary Clarifiers
- 5.2.2 Intermediate Clarifiers
- 5.2.3 Final Clarifiers
- 5.2.4 Weir Loading Rates
- 5.2.5 Depth/Detention Time

5.3 <u>Design Details</u>

- 5.3.1 Inlets
- 5.3.2 Submerged Surfaces
- 5.3.3 Weir Troughs
- 5.3.4 Freeboard

5.4 Sludge and Scum Removal

- 5.4.1 Scum Removal
- 5.4.2 Sludge Removal
- 5.4.3 Sludge Removal Piping
- 5.4.4 Sludge Removal Control
- 5.4.5 Sludge Hopper

5.5 <u>Protective and Service Facilities</u>

- 5.5.1 Operator Protection
- 5.5.2 Mechanical Maintenance Access
- 5.5.3 Electrical Fixtures and Controls

5.6 Operability, Flexibility, and Reliability

- 5.6.1 Scum Removal
- 5.6.2 Overflow Weirs
- 5.6.3 Unit Dewatering
- 5.6.4 Hydraulics
- 5.6.5 Sludge Removal5.6.6 Other Design Considerations

CLARIFIERS

5.1 General Criteria

5.1.1 Purpose

Clarifiers (sedimentation basins, settling tanks) are designed to perform three (3) functions in a treatment scheme:

- A. Remove solids from liquids by sedimentation
- B. Remove scum from liquid by flotation
- C. Thicken solids for removal and further treatment

Specific application of clarifier functions will be dependent upon the treatment process employed. This chapter does not attempt to set criteria for all types of clarifiers. If a unique clarifier is proposed, the design engineer shall submit operational and design data justifying its use.

5.1.2 Number of Units

Multiple units capable of independent operation shall be provided in all facilities where design flows exceed 250,000 gallons per day. Otherwise, the number of units required shall satisfy reliability requirements (see Section 1.3.11). Facilities not having multiple units shall include other methods to assure adequate operability and flexibility of treatment.

5.1.3 Arrangements

Clarifiers shall be arranged for greatest operating and maintenance convenience, flexibility, economy, continuity of maximum effluent quality, and ease of installation of future units.

5.1.4 Tank Configurations

Consideration should be given to the probable flow pattern in the selection of tank size and shape and inlet and outlet type and location.

5.1.5 Flow Distribution

Effective flow measuring devices and control appurtenances (i.e., valves, gates, splitter boxes, etc.) shall be provided to permit proper proportion of flow to each unit (see Section 13.2.1).

5.2 Design Loading

5.2.1 Primary Clarifiers

Primary clarifier designs are primarily based upon surface overflow rate. The following criteria are recommended for design:

	Hydraulic Loading Rate	Surface Overflow Rate
--	-------------------------------	-----------------------

Average Design Flow 800-1200 gpd/sq. ft. Peak Design Flow 2000-3000 gpd/sq. ft.

If WAS is returned to the primary then

Hydraulic Loading Rate Surface Overflow Rate

Average Design Flow 600-800 gpd/sq. ft. Peak Design Flow 1200-1500 gpd/sq. ft.

Primary clarifier sizing shall be calculated for both flow conditions and the larger surface area derived shall be utilized. A properly designed primary clarifier should remove 30 to 35% of the influent BOD. However, anticipated BOD removal for wastewater containing high quantities of industrial wastewater should be determined by laboratory tests and considerations of the quantity and characteristics of the wastes.

5.2.2 Intermediate Clarifiers

Surface overflow rates for intermediate clarifiers should be based upon the following criteria:

Maximum

Hydraulic Loading Kate	Surface Overflow Rate

Average Design Flow 1000 gpd/sq. ft. Peak Design Flow 2500 gpd/sq. ft.

5.2.3 Final Clarifiers

Final clarifier designs shall be based upon the type of secondary treatment application used. Surface overflow and solids loading rates shall be the general basis for clarifier designs. Pilot studies of biological treatment is recommended when unusual wastewater characteristics are evident or when the proposed loading exceeds those noted in this section.

Table 5-1 depicts the criteria established for final clarifier surface overflow and solids loading rates. In activated sludge systems, the surface overflow rate for final clarifiers should be based on influent wastewater flows and not include return activated sludge flows (RAS). Solids loading rate criteria assume sludge recycle is 100% of the average design flow and the design mixed liquor suspended solids (MLSS) concentration.

TABLE 5-1 FINAL CLARIFIER DESIGN PARAMETERS				
	Maximum Surface Overflow Rate gpd/sq.ft.		Solids Loading Rate lbm/day-sq.ft.	
Type of Process	Average Design Flow	Peak Design Flow	Average Design Flow	Peak Design Flow
Trickling Filter	600	1200	25	40
Activated Sludge	800 (600 for plants less than 1 MGD)	1200	30	50
Extended Aeration	400	1000	25	35
Nitrification	400	800	25	35
Pure Oxygen	700	1200	25	40

5.2.4 Weir Loading Rates

Weir loadings should not exceed 15,000 gallons per day per linear feet (gpd/li ft).

5.2.5 Depth/Detention Time

The sidewater depth (SWD) for clarifier designs associated with design surface overflow rates should dictate the hydraulic detention time of the clarifier. For design purposes, the following criteria in Table 5-2 are established specific to clarifier application:

TABLE 5-2					
CLARIFIER DEPTH					
T					
Type of Process	Diameter [ft]	Minimum Sidewater Depth [ft]			
*Primary	-	8			
Trickling Filter	-	10			
**Activated Sludge	Less than 40	11			
-	40-70	12			
	71-100	13			
	101-140	14			
	Over 140	15			

^{*}The hydraulic detention time in primary clarifiers is not recommended to be greater than 2.5 hours as a function of the surface overflow rate and SWD, since septic conditions resulting in poor performance and odor conditions can occur.

^{**}For rectangular-shaped clarifiers following activated sludge treatment, the recommended SWD shall be no less than 12 feet at the shallow end.

5.3 Design Details

5.3.1 Inlets

Inlets should be designed to dissipate the influent velocity, to distribute the flow equally in both the horizontal and vertical vectors, and to prevent short-circuiting. Channels should be designed to maintain an inlet velocity of at least one (1) foot per second at one-half the design flow. Corner pockets and dead ends should be eliminated and corner fillets or channeling used where necessary. Provisions shall be made for elimination or removal of floating materials in inlet structures having submerged ports.

5.3.2 Submerged Surfaces

The tops of troughs, beams, and similar submerged construction elements shall have a minimum slope of 1.75 vertical to 1 horizontal. The underside of such structures should have a slope of 1 to 1 to prevent accumulation of scum and solids.

5.3.3 Weir Troughs

Weir troughs shall be designed to prevent submergence at maximum design flow, and to maintain a velocity of at least one (1) foot per second at one-half design flow.

5.3.4 Freeboard

Walls of clarifiers shall extend at least six (6) inches above the surrounding ground surface and shall provide not less than twelve (12) inches of freeboard.

5.4 Sludge and Scum Removal

5.4.1 Scum Removal

Effective scum collection and removal facilities, including baffling ahead of the outlet weirs, shall be provided for all clarifiers. Provisions may be made for discharge of scum with sludge; however, other provisions may be necessary to dispose of floating materials which may adversely affect sludge handling and disposal. The unusual characteristics of scum which may adversely affect pumping, piping, sludge handling and disposal, should be recognized in the design. Scum piping should be glass lined or equivalent. Precautions should be taken to minimize water content in the scum.

5.4.2 Sludge Removal

Sludge collection and withdrawal facilities shall be designed to assure rapid removal of the sludge. Provisions shall be

made to permit continuous sludge removal from settling tanks. Final clarifiers in activated sludge plants shall be provided with positive scraping devices. Suction withdrawal should be provided for activated sludge plants designed for the reduction of nitrogenous oxygen demand.

5.4.3 Sludge Removal Piping

Each sludge hopper shall have an individually valved sludge withdrawal line at least six (6) inches in diameter if pumped and at least eight (8) inches in diameter if gravity flow is used. This does not apply to air lift methods of sludge removal, as this should be determined by the sludge removal rate. Static head available for sludge withdrawal shall be at least thirty (30) inches, as necessary, to maintain a three (3) feet per second velocity in the withdrawal pipe. Clearance between the end of the withdrawal line and the hopper walls shall be sufficient to prevent "bridging" of the sludge. Adequate provisions shall be made for rodding or back-flushing individual pipe runs.

***Air lift type sludge removal will not be approved for removal of primary sludges.

5.4.4 Sludge Removal Control

Sludge wells equipped with telescoping valves or other appropriate equipment shall be provided for viewing, sampling and controlling the rate of sludge withdrawal. A means for measuring the sludge removal rate and sludge return rate shall be provided. Sludge pump motor control systems shall include time clocks and valve activators for regulating the duration and sequencing of sludge removal. Gravity flow systems should have back-up pumping capabilities.

5.4.5 Sludge Hopper

The minimum slope of the side walls shall be 1.75 vertical to 1 horizontal. Hopper wall surfaces should be made smooth with rounded corners to aid in sludge removal. Hopper bottoms shall have a maximum dimension of two (2) feet. Extra-depth sludge hoppers for sludge thickening are not acceptable.

5.5 Protective and Service Facilities

5.5.1 Operator Protection

All clarifiers shall be equipped to enhance safety for operators. Such features shall appropriately include machinery cover lift lines, stairways, walkways, handrails and slip-resistant surfaces.

5.5.2 Mechanical Maintenance Access

The design shall provide for convenient and safe access to routine maintenance items such as gear boxes, scum removal mechanisms, baffles, weirs, inlet stilling baffle area, and effluent channels.

5.5.3 Electrical Fixtures and Controls

Electrical fixtures and controls in enclosed settling basins shall meet the requirement of the National Electrical Code. The fixtures and controls shall be located so as to provide convenient and safe access for operation and maintenance. Adequate area lighting shall be provided.

5.6 Operability, Flexibility, and Reliability

5.6.1 Scum Removal

- 5.6.1.1 A method of conveying scum across the water surface to a point of removal should be considered, such as water or air spray. Baffles should be designed to ensure capture of scum at minimum and maximum flow rates.
- 5.6.1.2 Facilities designed for flows of 0.1 MGD and greater should have mechanical scum removal equipment.
- 5.6.1.3. Scum holding tanks may be provided, with a method of removing excess water.
- 5.6.1.4 Large scum sumps should have a mixing device (pneumatic, hydraulic, or mechanical) to keep the scum mixed while being pumped.
- 5.6.1.5 Manual scum pump start-stop switches should be located adjacent to scum holding tanks.

5.6.2 Overflow Weirs

- 5.6.2.1 Since closely spaced multiple overflow weirs tend to increase hydraulic velocities, their spacing should be conservative.
- 5.6.2.2 Center-feed, peripheral draw-off clarifiers shall not have the overflow weir against the clarifier sidewall. Weir placement shall be 1/10 diameter or greater toward the center.
- 5.6.2.3 The up-flow rate shall not be greater than the surface overflow rate at any location within the solids separation zone of a clarifier.

- 5.6.2.4 Overflow weirs should be of the notched type; straight edged weirs will not be approved.
- 5.6.2.5 Overflow weirs shall be adjustable for leveling.

5.6.3 Unit Dewatering

- 5.6.3.1 The capacity of dewatering pumps should be such that the basin can be dewatered in 24 hours; eight hours is preferable.
- 5.6.3.2 The contents of the basin should be discharged to the closest process upstream from the unit being dewatered that can accept the flow.
- 5.6.3.3 Consideration shall be given to the need for hydrostatic pressure relief devices to prevent flotation of structures.

5.6.4 Hydraulics

- 5.6.4.1 Lift/pump stations located immediately upstream of secondary clarifiers shall have flow-paced controls to reduce shock loadings.
- 5.6.4.2 Square clarifiers with circular sludge withdrawal mechanisms shall be designed such that corner hydraulic velocities do not cause sludge carry-over.

5.6.5 Sludge Removal

- 5.6.5.1 When two or more clarifiers are used, provisions shall be made to control and measure the rate of sludge withdrawal from each clarifier.
- 5.6.5.2 Consideration should be given to removing activated sludge from the effluent end of rectangular clarifiers.
- 5.6.5.3 Consideration shall be given to chlorination of return activated sludge and digester supernate. Sufficient mixing and contact time should be provided.

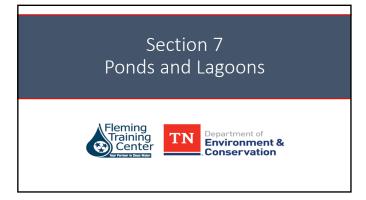
5.6.6 Other Design Considerations

- 5.6.6.1 Designs should consider the possible need for future modifications to add chemicals such as flocculants.
- 5.6.6.2 A method of foam control should be considered for all inlet channels and feed wells in activated sludge systems.

Section 7 Ponds and Lagoons







Advantages of Ponds

- · Economical to operate
- · Capable of handling high flows
- Adaptable to changing loads
- Accumulate sludge at a rate of 0.2 lbs per lb of BOD (much lower than conventional facilities where the accumulation rate is 0.5 lbs to 1.0 lbs of solids per lb of BOD removed.)

1

Advantages of Ponds

• Have an increased potential design life
• Serve as wildlife habitat
• Consume little energy
• Adaptable to land application

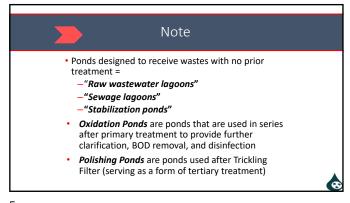
Disadvantages of Ponds

- · May produce odors
- Require large land areas
- · Are affected by climactic conditions
- May have high suspended solids levels in effluent
- · Might contaminate groundwater

3

4

2



Types of Lagoons

- Aerobic

- Anaerobic

- Anaerobic

- Facultative

- Unaerated or Aerated

Types of Bacteria in Stabilization Lagoons

- Anaerobic

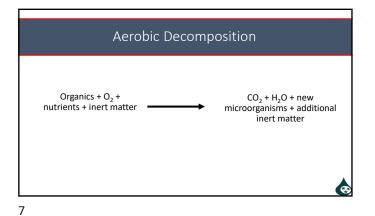
- Facultative

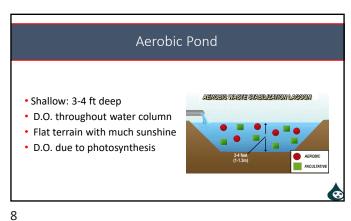
Aerobic

Anaerobic

- Facultative

6





Aerobic Pond

- Organic matter is used as food by aerobic bacteria, their waste product is carbon dioxide
 - The carbon dioxide and ammonia in the wastewater are important for algal growth
- By using sunlight for energy in the process of photosynthesis, the algae use the carbon dioxide (CO₂) in the water to produce free oxygen (O₂), making it available to the aerobic bacteria that inhabit the pond.

Algae

- Algae are simple microscopic plants
- Algae live on carbon dioxide and other nutrients in the wastewater.
- During the day, algae use ${\rm CO_2}$, which raises the pH, while at night they produce ${\rm CO_2}$ and the pH is lowered.
- At night, algae use up the O₂ by respiration and produce CO₂.
- The alternate use and production of oxygen and carbon dioxide can result in diurnal (daily) variations of both pH and DO.
- Each pound of algae in a healthy pond is capable of producing 1.6 pounds of oxygen on a normal summer day.

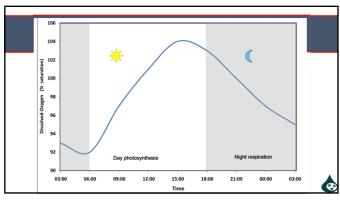
9

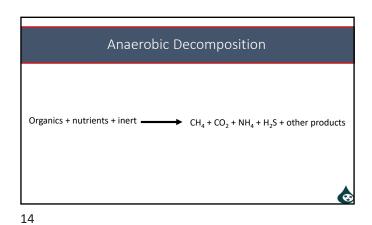
10

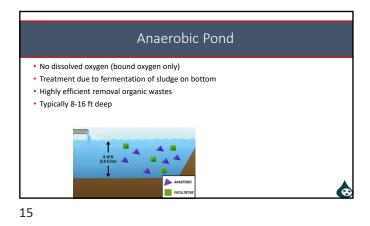
Photosynthesis Process of converting carbon dioxide (CO2) and inorganic substances into oxygen and additional plant material Plants with chlorophyll (and cyanobacteria) Uses sunlight as energy source All green plants grow by this process

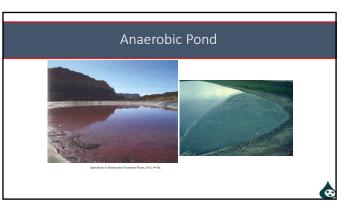
Photosynthesis vs. Respiration $CO_2 + H_2O \longleftrightarrow O_2 + CH_2O$ Respiration

Algae produce oxygen during periods of sunlight and consume oxygen during the night

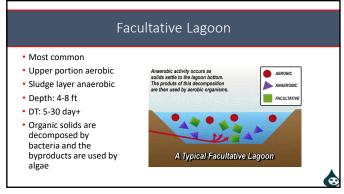


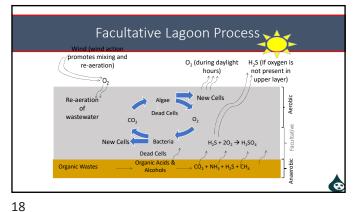


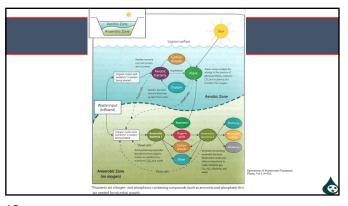


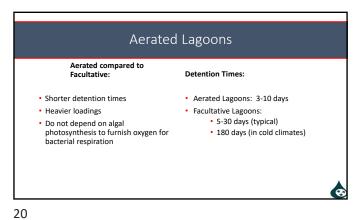


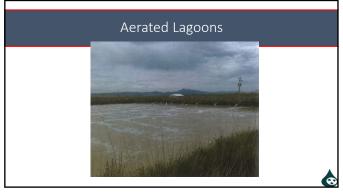
16

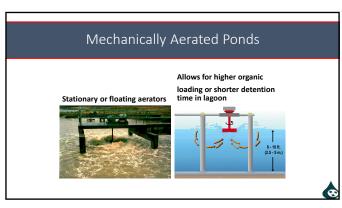




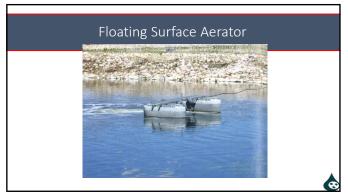


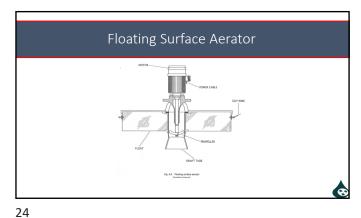


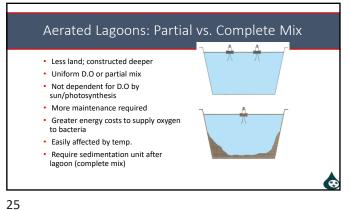


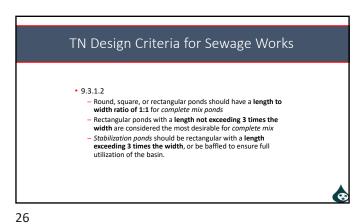


21 22





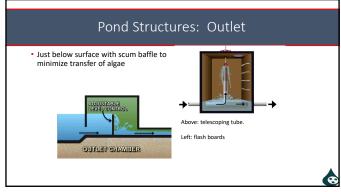




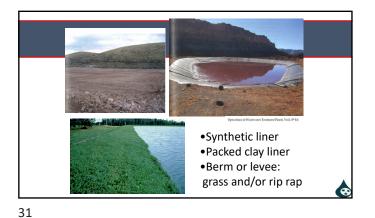


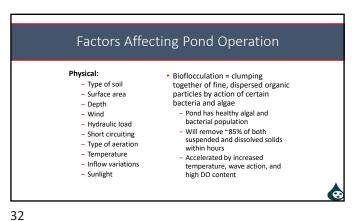
Турі	ical La	goon D	esign	
Parameter	Aerobic	Facultative	Anaerobic	Aerated
Size, acres	<10, multiples	2-10 multiples	0.5-2.0	2-10, multiples
Operation	Series or Parallel	Series or Parallel	Series	Series or Parallel
Detention Time, days	10-40	5-30*	20-50	3-10
Depth, ft	3-4	4-8	8-16	6-20
pH	6.5-10.5	6.5-8.5	6.5-7.2	6.5-8.0
Temperature Range, °C	0-30	0-50	6-50	0-30
Optimum Temperature, $^{\circ}\mathrm{C}$	20	20	30	20
BOD5 Loading, lb/ac/d	54-110	45-160	180-450	
BOD5 Removal, %	80-95	80-95	50-85	80-95
*180 days in cold climates				





Ponds/Lagoons



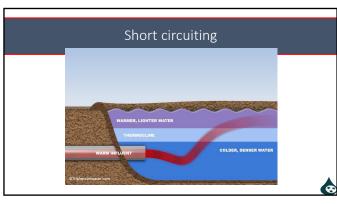


In winter, the pond is cooler than the incoming sewage. The warmer sewage rises and rides over the surface causing a short circuit.

In summer, the pond is warmer than the incoming sewage.

Cypentium of Theorems Thanks, Yad I, Pr 64

Copentium of Theorems Thanks, Yad I, Pr 64



33 34

Pond depth less than 3 feet Complete sunlight penetration May be completely aerobic until enough solids collect Discharges from shallow, aerobic ponds contain large amounts of algae Can become infested with filamentous algae and mosses Pond depth 4 feet or more Greater heat conservation – encourages biological activity Provides physical storage of dissolved oxygen Prevents tule and cattail growth

Factors Affecting Pond Operation

• Biochemical:

-Organic loading rate

-pH

-Dissolved oxygen

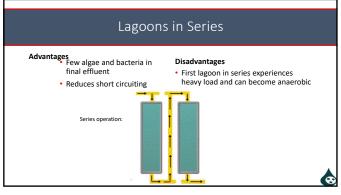
-Alkalinity

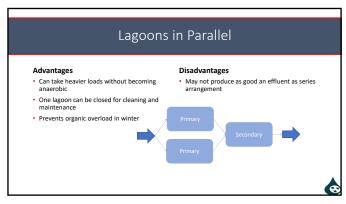
• Microbiological: bacteria, algae, etc.

Two types of operation Series = wastewater flows into one primary cell, then into the next, and so on Produces higher quality effluent Parallel = distribution chambers or splitter boxes evenly divide wastewater influent streams into both primary cells

PRINCEST PROBLEM TO PR

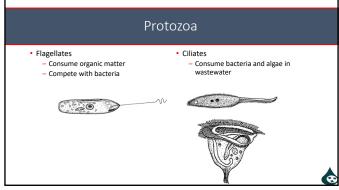
37





39 40

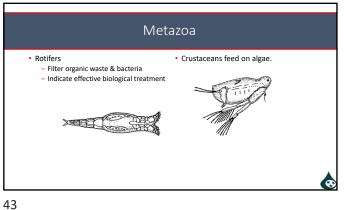


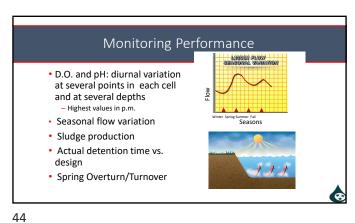


41 42

Ponds/Lagoons

38





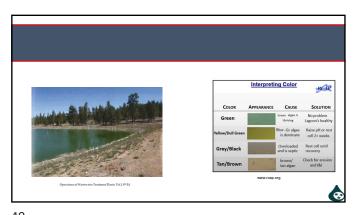
Overturn/Turnover Mixing of all layers in a reservoir when the water temperatures become similar from May occur in Spring and/or Fall • Spring: surface water warms to similar temp as bottom • Fall: surface water cools to similar temp as bottom Wind plays a role

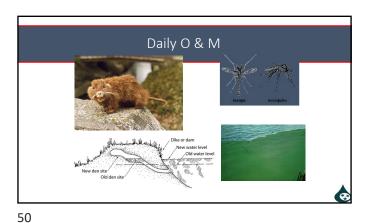
Overturn/Turnover Epilimnion, Thermocline, Hypolimnion Thermocline = The middle, transitional layer of a reservoir that shows rapid temperature change Separates the warm surface waters from the cold, denser waters at the bottom

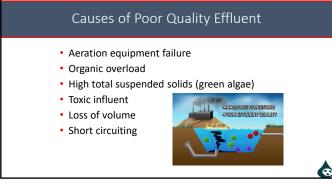
45 46

	Sampling and Analysis
• 1	pH and DO most important
	pH, temperature, and DO several times a week (and occasionally at night)
	Sparkling, deep green color indicates a high pH and good DO
	 Dull green, gray, or colorless indicates pH and DO are too low
• 9	Samples should be collected from same point or location – 4 corners, 8 ft. from water's edge and 1 ft. deep
• (Grab samples: temp, pH, DO, chlorine residual
• (Composite samples: BOD and suspended solids

Daily Operation & Maintenance Block sunlight: reduce Agitation with water jets Control of scum & green algae activity; odors; avian botulism & rakes manually mats of blue-green bacteria Pull out young plants; maintain min. 3 ft depth; Mosquito breeding Weeds ground; scum accumulation; hinders circulation riprap; raise & lower water level Nuisance; disease Mosquito larvicide; Insects addition Gambusia (mosquito fish) Trap out; lower water level to expose den Muskrats. Destroy berm walls by groundhogs, turtles







Low D.O. in Lagoon

• Low algae growth

• Excess scum

• Aeration problems

• Organic overload

• Short circuiting

51

53

Odors in Lagoons

• Causes: overloading; poor housekeeping

- Facultative ponds can have seasonal (spring and fall) odors due to turnover

• Treatment methods:

- Add aeration

- Feed sodium nitrate as oxygen source

- Housekeeping- manual scum and algae removal

- Masking agents

- Chlorination

Lagoon Safety

• Never work around a lagoon alone
• Never perform maintenance from a boat
• Never take a boat onto the lagoon alone





Polishing Pond • Design Criteria: Secondary Effluent Quality: Organic Loading: -20-25 lbs BOD/ac/day • BOD -< 30 ppm Hydraulic Loading: –2350-2990 gpd/ac SS -< 30 ppm Total Nitrogen Water Depth -5-6.5 ft -< 15 ppm Total Phosphorous -< 6 ppm



Ponds and Lagoons Vocabulary

1.	Raw Wastewater Lagoons, which are also referred to as,	are ponds
	designed to receive wastes with no prior treatment.	
2.	A is used after a trickling filter plant, and it serves as a form	n of
	tertiary treatment.	
3.	The phenomenon known as is the almost spontaneous mixin layers of water in a reservoir due to similar water temperature from top to bottom. This tain the fall/winter when the surface waters cool to the same temperature as the bottom was also in the spring when the surface waters warm to the same temperature as the insulated layer.	kes place iters; and
4.	When distribution chambers or splitter boxes evenly divide wastewater influent streams in primary cells of a lagoon system, it is said to be in operation.	to both
5.	Characterized by having dissolved oxygen consistently distributed throughout their water of the control of the daylight hours who photosynthesis takes place.	
6.	In, where no DO is present, degradation of wastes occurs via fermentation at the pond bottom. Methane, hydrogen sulfide, and carbon dioxide are bype this process.	
7.	In a pond with a healthy algal and bacterial population, a phenomenon known as can occur, in which certain bacteria and algae will cause the cl together of fine, dispersed organic particles. This results in faster and more complete settli organic solids in wastewater.	
8.	When ponds are used in series (after a primary treatment) in order to provide additional clarification, BOD removal, and disinfection, they are referred to as	
9.	The most common type of pond is the, which is divided into	2 layers.
10.	The process in which organisms (with the aid of chlorophyll) convert carbon dioxide and incomposition oxygen and additional plant material, using sunlight for energy, is called All green plants grow by this process.	organic
11.	are microscopic plants containing chlorophyll that produce o during the sunlight hours and use oxygen during the night hours. Their biological activities pH, DO, and alkalinity of the pond.	
12.	The exact opposite equation of photosynthesis, plants use oxygen and produce carbon diox during At night in a pond, algae are using up the oxygen (that v produced by photosynthesis earlier in the day) during this reaction.	

13.	When wastewater flows into one primary cell, then into the next primary cell, and so on, this set-up called aoperation. This type of lagoon is used when a higher quality ffluent is required because the quality of the effluent improves as it gets transported through each						
	lagoon.						
14.	The transitional middle layer of a pond or reservoir that shows a rapid temperature change is called						
	the It separates the warm surface waters from the den	ser cold					
	waters at the bottom.						
Wc	ord Bank						
Sta	abilization ponds						
Res	spiration						
Oxi	kidation ponds						
Pol	lishing pond						
Pho	otosynthesis						
The	ermocline						
Par	rallel						
Aer	erobic ponds						
Ana	naerobic ponds						
Fac	cultative pond						
Alg	gae						
Ser	ries						
Bio	oflocculation						
Ove	verturn/Turnover						

CHAPTER 9

Ponds and Aerated Lagoons

9.1	General
	9.1.1 Applicability9.1.2 Supplement to Engineering Report9.1.3 Effluent Requirements
9.2	<u>Design Loadings</u>
	9.2.1 Stabilization Ponds 9.2.2 Aerated Lagoons
9.3	Special Details
	9.3.1 General 9.3.2 Stabilization Ponds 9.3.3 Aerated Lagoons
9.4	Pond Construction Details
	9.4.1 Liners 9.4.2 Pond Construction 9.4.3 Prefilling 9.4.4 Utilities and Structures Within Dike Sections
9.5	Hydrograph Controlled Release (HCR) Lagoons
9.6	Polishing Lagoons
9.7	<u>Operability</u>
9.8	<u>Upgrading Existing Systems</u>

PONDS AND AERATED LAGOONS

9.1 General

This chapter describes the requirements for the following biological treatment processes:

a. Stabilization ponds

b. Aerated lagoons

Additionally, this chapter describes the requirements for use of hydraulic control release lagoons for effluent disposal.

A guide to provisions for lagoon design is the EPA publication Design Manual - Municipal Wastewater Stabilization Ponds, EPA-625/1-83-015.

9.1.1 Applicability

In general, ponds and aerated lagoons are most applicable to small and/or rural communities where land is available at low cost and minimum secondary treatment requirements are acceptable. Advantages include potentially lower capital costs, simple operation, and low O&M costs.

9.1.2 Supplement to Engineering Report

The engineering report shall contain pertinent information on location, geology, soil conditions, area for expansion, and any other factors that will affect the feasibility and acceptability of the proposed treatment system.

The following information should be submitted in addition to that required in the Chapter 1 section titled "Engineering Report and Preliminary Plans":

- a. The location and direction of all residences, commercial development, and water supplies within 1/2 mile of the proposed pond
- b. Results of the geotechnical investigation performed at the site
- c. Data demonstrating anticipated seepage rates of the proposed pond bottom at the maximum water surface elevation
- d. A description, including maps showing elevations and contours, of the site and adjacent area suitable for expansion
- e. The ability to disinfect the discharge is required.

January 2016 9-2 Design Criteria Ch. 9

9.1.3 Effluent Requirements

See Chapter 1, Section 1.1.

9.2 **Design Loadings**

9.2.1 **Stabilization Ponds**

Stabilization ponds are facultative and are not artificially mixed or aerated. Mixing and aeration are provided by natural processes. Oxygen is supplied mainly by algae.

Design loading shall not exceed 30 pounds BOD per acre per day on a total pond area basis and 50 pounds BOD per acre per day to any single pond (from Middlebrooks).

9.2.2 Aerated Lagoons

An aerated lagoon may be a complete-mix lagoon or a partial-mix aerated lagoon. Complete-mix lagoons provide enough aeration or mixing to maintain solids in suspension. Power levels are normally between 20 and 40 horsepower per million gallons. The partial-mix aerated lagoon is designed to permit accumulation of settleable solids on the lagoon bottom, where they decompose anaerobically. The power level is normally 4 to 10 horsepower per million gallons of volume.

BOD removal efficiencies normally vary from 80 to 90 percent, depending on detention time and provisions for suspended solids removal.

The aerated lagoon system design for minimum detention time may be estimated by using the following formula; however, for the development of final parameters, it is recommended that actual experimental data be developed.

$$\frac{Se}{So} = \frac{1}{1 + 2.3K_1^t}$$

where:

t = detention time, days

 K_1 = reaction coefficient, complete system per day, base 10

For complete treatment of normal domestic sewage, the K₁ value will be assumed to be:

 $K_1 = 1.087$ @20°C for complete mix

 $K_1 = 0.12$ @20°C for partial mix

Se = effluent BOD_5 , mg/l

So = influent BOD₅, mg/l

January 2016 9-3 Design Criteria Ch. 9 The reaction rate coefficient for domestic sewage that includes significant quantities of industrial wastes, other wastes, and partially treated sewage should be determined experimentally for various conditions that might be encountered in the aerated ponds. Conversion of the reaction rate coefficient to temperatures other than 20 degrees C should be according to the following formula:

$$K_1 = K_{20} \cdot 1.036 (T-20)$$
 (T = temperature in degrees C)

The minimum equilibrium temperature of the lagoon should be used for design of the aerated lagoon. The minimum equilibrium temperature should be estimated by using heat balance equations, which should include factors for influent wastewater temperature, ambient air temperature, lagoon surface area, and heat transfer effects of aeration, wind, and humidity. The minimum 30-day average ambient air temperature obtained from climatological data should be used for design.

Additional storage volume shall be considered for sludge storage and partial mix in aerated lagoons.

Sludge processing and disposal should be considered.

9.3 Special Details

9.3.1 General

9.3.1.1 Location

a. Distance from Habitation

A pond site should be located as far as practicable from habitation or any area that may be built up within a reasonable future period, taking into consideration site specifics such as topography, prevailing winds, and forests. Buffer zones between the lagoon and residences or similar land use should be at least 300 feet to residential property lines, and 1000 feet to existing residence structures.

b. Prevailing Winds

If practical, ponds should be located so that local prevailing winds will be in the direction of uninhabited areas. Preference should be given to sites that will permit an unobstructed wind sweep across the length of the ponds in the direction of the local prevailing winds.

January 2016 9-4 Design Criteria Ch. 9

Surface Runoff c.

Location of ponds in watersheds receiving significant amounts of runoff water is discouraged unless adequate provisions are made to divert storm water around the ponds and protect pond embankments from erosion.

d. Water Table

The effect of the ground water location on pond performance and construction must be considered.

Ground Water Protection e.

Ground Water Protection's main emphasis should be on site selection and liner construction, utilizing mainly compacted clay. Proximity of ponds to water supplies and other facilities subject to contamination and location in areas of porous soils and fissured rock formations should be critically evaluated to avoid creation of health hazards or other undesirable conditions. The possibility of chemical pollution may merit appropriate consideration. wells to monitor potential ground water pollution may be required and should be designed with proper consideration to water movement through the soil as appropriate.

An approved system of ground water monitoring wells or lysimeters may be required around the perimeter of the pond site to facilitate ground water monitoring. The use of wells and/or lysimeters will be determined on a case-by-case basis depending on proximity of water supply and maximum ground water levels. This determination will be at the site approval phase (see Section 1.1).

A routine ground water sampling program shall be initiated prior to and during the pond operation, if required.

f. **Floodwaters**

Pond sites shall not be constructed in areas subject to 25-year flooding, or the ponds and other facilities shall be protected by dikes from the 25-year flood.

January 2016 9-5 Design Criteria Ch. 9

9.3.1.2 Pond Shape

The shape of all cells should be such that there are no narrow or elongated portions. Round, square, or rectangular ponds should have a length to width ratio near 1:1 for complete mix ponds. Rectangular ponds with a length not exceeding three times the width are considered most desirable for complete mix aerated lagoons. However, stabilization ponds should be rectangular with a length exceeding three times the width, or be baffled to ensure full utilization of the basin. No islands, peninsulas, or coves are permitted. Dikes should be rounded at corners to minimize accumulations of floating materials. Common dike construction should be considered whenever possible to minimize the length of exterior dikes.

9.3.1.3 Recirculation

Recirculation of lagoon effluent may be considered. Recirculation systems should be designed for 0.5 to 2.0 times the average influent wastewater flow and include flow measurement and control.

9.3.1.4 Flow Measurement

The design shall include provisions to measure, total, and record the wastewater flows.

9.3.1.5 Level Gauges

Pond level gauges should be located on outfall structures or be attached to stationary structures for each pond.

9.3.1.6 Pond Dewatering

All ponds shall have emergency drawdown piping to allow complete draining for maintenance.

Sufficient pumps and appurtenances should be available to facilitate draining of individual ponds in cases where multiple pond systems are constructed at the same elevation or for use if recirculation is desired

9.3.1.7 Control Building

A control building for laboratory and maintenance equipment should be provided.

January 2016 9-6 Design Criteria Ch. 9

9.3.1.8 General Site Requirements

The pond area shall be enclosed with an adequate fence to keep out livestock and discourage trespassing, and be located so that travel along the top of the dike by maintenance vehicles is not obstructed. A vehicle access gate of width sufficient to accommodate mowing equipment and maintenance vehicles should be provided. access gates shall be provided with locks. Cyclone-type fences, 5 to 6 feet high with 3 strands of barbed wire, are desirable, with appropriate warning signs required.

9.3.1.9 Provision for Sludge Accumulation

Influent solids, bacteria, and algae that settle out in the lagoons will not completely decompose and a sludge blanket will form. This can be a problem if the design does not include provisions for removal and disposal of accumulated sludge, particularly in the cases of anaerobic stabilization ponds and aerated lagoons. The design should include an estimate of the rate of sludge accumulation, frequency of sludge removal, methods of sludge removal, and ultimate sludge handling and disposal. Abandoning and capping of the lagoon is an acceptable solution (Re: The Division of Solid Waste Management guidelines for abandonment of a lagoon). However, the design life shall be stated in the report.

9.3.2 Stabilization Ponds

9.3.2.1 Depth

The primary (first in a series) pond depth should not exceed 6 feet. Greater depths will be considered for polishing ponds and the last ponds in a series of 4 or more.

9.3.2.2 Influent Structures and Pipelines

a. Manholes

A manhole should be installed at the terminus of the interceptor line or the force main and should be located as close to the dike as topography permits; its invert should be at least 6 inches above the maximum operating level of the pond to provide sufficient hydraulic head without surcharging the manhole.

January 2016 9-7 Design Criteria Ch. 9

b. Influent Pipelines

The influent pipeline can be placed at zero grade. The use of an exposed dike to carry the influent pipeline to the discharge points is prohibited, as such a structure will impede circulation.

c. Inlets

Influent and effluent piping should be located to minimize short-circuiting and stagnation within the pond and maximize use of the entire pond area.

Multiple inlet discharge points shall be used for primary cells larger than 10 acres.

All gravity lines should discharge horizontally onto discharge aprons. Force mains should discharge vertically up and shall be submerged at least 2 feet when operating at the 3-foot depth.

d. Discharge Apron

Provision should be made to prevent erosion at the point of discharge to the pond.

9.3.2.3 Interconnecting Piping and Outlet Structures

Interconnecting piping for pond installations shall be valved or provided with other arrangements to regulate flow between structures and permit variable depth control.

The outlet structure can be placed on the horizontal pond floor adjacent to the inner toe of the dike embankment. A permanent walkway from the top of the dike to the top of the outlet structure is required for access.

The outlet structure should consist of a well or box equipped with multiple-valved pond drawoff lines. An adjustable drawoff device is also acceptable. The outlet structure should be designed so that the liquid level of the pond can be varied from a 3.0- 5.0 foot depth in increments of 0.5 foot or less. Withdrawal points shall be spaced so that effluent can be withdrawn from depths of 0.75 foot to 2.0 feet below pond water surface, irrespective of the pond depth.

The lowest drawoff lines should be 12 inches off the bottom to control eroding velocities and avoid pickup of bottom deposits. The overflow from the pond shall be taken near but below the water surface. A two-foot deep baffle may be helpful to keep algae from the effluent. The structure should also have provisions for draining the pond.

January 2016 9-8 Design Criteria Ch. 9

A locking device should be provided to prevent unauthorized access to level control facilities. An unvalved overflow placed 6 inches above the maximum water level shall be provided.

Outlets should be located nearest the prevailing winds to allow floating solids to be blown away from effluent weirs.

The pond overflow pipes shall be sized for the peak design flow to prevent overtopping of the dikes.

9.3.2.4 Minimum and Maximum Pond Size

No pond should be constructed with less than 1/2 acre or more than 40 acres of surface area.

9.3.2.5 Number of Ponds

A minimum of three ponds, and preferably four ponds, in series should be provided (or baffling provided for a single cell lagoon design configuration) to insure good hydraulic design. The objective in the design is to eliminate short circuiting.

9.3.2.6 Parallel/Series Operation

Designs, other than single ponds with baffling, should provide for operation of ponds in parallel or series. Hydraulic design should allow for equal distribution of flows to all ponds in either mode of operation.

9.3.3 Aerated Lagoons

9.3.3.1 Depth

Depth should be based on the type of aeration equipment used, heat loss considerations, and cost, but should be no less than 7 feet. In choosing a depth, aerator erosion protection and allowances for ice cover and solids accumulation should be considered.

9.3.3.2 Influent Structures and Pipelines

The same requirements apply as described for facultative systems, except that the discharge locations should be coordinated with the aeration equipment design.

January 2016 9-9 Design Criteria Ch. 9

9.3.3.3 Interconnecting Piping and Outlet Structures

a. Interconnecting Piping

The same requirements apply as described for facultative systems.

b. Outlet Structure

The same requirements apply as described for facultative systems, except for variable depth requirements and arrangement of the outlet to withdraw effluent from a point at or near the surface. The outlet shall be preceded by an underflow baffle.

9.3.3.4 Number of Ponds

Not less than three basins should be used to provide the detention time and volume required. The basins should be arranged for both parallel and series operation. A settling pond with a hydraulic detention time of 2 days at average design flow must follow the aerated cells, or an equivalent of the final aerated cell must be free of turbulence to allow settling of suspended solids.

9.3.3.5 Aeration Equipment

A minimum of two mechanical aerators or blowers shall be used to provide the horsepower required. At least three anchor points should be provided for each aerator. Access to aerators should be provided for routine maintenance which does not affect mixing in the lagoon. Timers will be required.

9.4 Pond Construction Details

9.4.1 Liners

9.4.1.1 Requirement for Lining

The seepage rate through the lagoon bottom and dikes shall not be greater than a water surface drop of 1/4 inch per day. (Note: The seepage rate of 1/4 inch per day is 7.3×10^{-6} cm/sec coefficient of permeability seepage rate under pond conditions.) If the native soil cannot be compacted or modified to meet this requirement, a pond liner system will be required.

If a lagoon is proposed to be upgraded, it must be shown that it currently meets the 1/4-inch per day seepage rate before approval will be given.

January 2016 9-10 Design Criteria Ch. 9

9.4.1.2 General

Pond liner systems that should be evaluated and considered include (1) earth liners, including native soil or local soils mixed with commercially prepared bentonite or comparable chemical sealing compound, and (2) synthetic membrane liners.

The liner should not be subject to deterioration in the presence of the wastewater. The geotechnical recommendations should be carefully considered during pond liner design.

Consideration should also be given to construct test wells when required by the Department in any future regulations, or when industrial waste is involved.

9.4.1.3 Soil Liners

The thickness and the permeability of the soil liners shall be sufficient to limit the leakage to the maximum allowable rate of 1/4 inch per day. The evaluation of earth for use as a soil liner should include laboratory permeability tests of the material and laboratory compaction tests. The analysis should take into consideration the expected permeability of the soil when compacted in the field. All of the soil liner material shall have essentially the same properties.

The analysis of an earth liner should also include evaluation of the earth liner material with regard to filter design criteria. This is required so that the fine-grained liner material does not infiltrate into a coarser subgrade material and thus reduce the effective thickness of the liner.

If the ponds are going to remain empty for any period of time, consideration should be given to the possible effects on the soil liners from freezing and thawing during cold weather or cracking from hot, dry weather. Freezing and thawing will generally loosen the soil for some depth. This depth is dependent on the depth of frost penetration.

The compaction requirements for the liner should produce a density equal to or greater than the density at which the permeability tests were made. The minimum liner thickness should be 12 inches, to ensure proper mixing of bentonite with the native soil. The soil should be placed in lifts no more than 6 inches in compacted thickness. The moisture content at which the soil is placed should be at or slightly above the optimum moisture content.

Construction and placement of the soil liner should be inspected by a qualified inspector. The inspector should keep records on the uniformity of the earth liner material, moisture contents, and the densities obtained.

Bentonite and other similar liners should be considered as a form of earth liner. Their seepage characteristics should be analyzed as previously

January 2016 9-11 Design Criteria Ch. 9

mentioned, and laboratory testing should be performed using the mixture of the native or local soil and bentonite or similar compound.

In general, the requirements for bentonite or similar compounds should include the following: (1) The bentonite or similar compound should be high swelling and free flowing and have a particle size distribution favorable for uniform application and minimizing of wind drift; (2) the application rate should be least 125 percent of the minimum rate found to be adequate in laboratory tests; (3) application rates recommended by a supplier should be confirmed by an independent laboratory; and (4) the mixtures of soil and bentonite or similar compound should be compacted at a water content greater than the optimum moisture content.

9.4.1.4 Synthetic Membrane Liners

Requirements for the thickness of synthetic liners may vary due to the liner material, but it is generally recommended that the liner thickness be no less than 20 mils; that is, 0.020 inch. There may be special conditions when reinforced membranes should be considered. These are usually considered where extra tensile strength is required. The membrane liner material should be compatible with the wastewater in the ponds such that no damage results to the liner. PVC liners should not be used where they will be exposed directly to sunlight. The preparation of the subgrade for a membrane liner is important. The subgrade should be graded and compacted so that there are no holes or exposed angular rocks or pieces of wood or debris. If the subgrade is very gravelly and contains angular rocks that could possibly damage the liner, a minimum bedding of 3 inches of sand should be provided directly beneath the liner. The liner should be covered with 12 inches of soil. This includes the side slope as well. No equipment should be allowed to operate directly on the liner. Consideration should be given to specifying that the manufacturer's representative be on the job supervising the installation during all aspects of the liner placement. An inspector should be on the job to monitor and inspect the installation.

Leakage must not exceed 1/4-inch per day.

9.4.1.5 Other Liners

Other liners that have been successfully used are soil cement, gunite, and asphalt concrete.

The performance of these liners is highly dependent on the experience and skill of the designer. Close review of the design of these types of liners is recommended.

January 2016 9-12 Design Criteria Ch. 9

9.4.2 Pond Construction

9.4.2.1 General

Ponds are often constructed of either a built-up dike or embankment section constructed on the existing grade, or they are constructed using a cut and fill technique. Dikes and embankments shall be designed using the generally accepted procedures for the design of small earth dams. The design should attempt to make use of locally available materials for the construction of dikes. Consideration should also be given to slope stability and seepage through and beneath the embankment and along pipes.

9.4.2.2 Top Width

The minimum recommended dike top width should be 12 feet on tangents and 15 feet on curves to permit access of maintenance vehicles. The minimum inside radius of curves of the corners of the pond should be 35 feet.

9.4.2.3 Side Slopes

Normally, inside slopes of either dikes or cut sections should not be steeper than 3 horizontal to 1 vertical. Outer slopes should not be steeper than 2 horizontal to 1 vertical. However, in many instances, the types of material used, maintenance considerations, and seepage conditions can indicate that other slopes should be used.

9.4.2.4 Freeboard

There should be sufficient freeboard to prevent overtopping of the dike from wave action and strong winds. A minimum of one foot is required.

9.4.2.5 Erosion Control

Erosion control should be considered for the inside slopes of the dike to prevent the formation of wavecut beaches in the dike slope. In the event that earth liners or membrane liners with earth cover are used, consideration should be given to erosion protection directly beneath aeration units. If the currents are strong enough, considering the type of material used for the earth cover, erosion pads may be necessary beneath the aeration units. Erosion control should also be considered wherever influent pipes empty into the pond.

If a grass cover for the outer slopes is desired, they should be fertilized and seeded to establish a good growth of vegetative cover. vegetative cover will help control erosion from runoff. Consideration should also be given to protection of the outer slopes in the event that flooding occurs. The erosion protection should be able to withstand the currents from a flood.

January 2016 9-13 Design Criteria Ch. 9

9.4.3 Prefilling

The need to prefill ponds in order to determine the leakage rate shall be determined by the Department and incorporated into the plans and specifications. The strongest consideration for prefilling ponds will be given to ponds with earth liners. Ponds in areas where the surrounding homes are on wells will also be given strong consideration for prefilling.

9.4.4 Utilities and Structures Within Dike Sections

Pipes that extend through an embankment should be bedded up to the springline with concrete. Backfill should be with relatively impermeable material. No granular bedding material should be used. Cutoff collars should be used as required. No gravel or granular base should be used under or around any structures placed in the embankment within the pond. Embankments should be constructed at least 2 feet above the top of the pipe before excavating the pipe trench.

9.5 Hydrograph Controlled Release (HCR) Lagoons

All lagoons requirements apply to HCR lagoons with the following additional concerns:

HCR lagoons control the discharge of treated wastewater in accordance with the stream's assimilative capacity. Detention times vary widely and must be determined on a case-by-case basis.

HCR sites require much receiving stream flow pattern characterization. For this purpose, EPA Region IV has developed a computer design program. The Division of Water Pollution Control can assist in sizing the HCR basin using this program. HCR sites may be more economical if the design is combined with summertime land application. Their design is more economical if summer/winter or monthly standards are available.

The design and construction of the in-stream flow measurement equipment are critical components of an HCR system. The United States Geological Survey (USGS) should be contacted during the design phase. The USGS also has considerable construction experience concerning in-stream monitoring stations, although construction need not necessarily be done or supervised by the USGS.

January 2016 9-14 Design Criteria Ch. 9

9.6 **Polishing Lagoons**

Polishing lagoons following activated sludge are not permissible in Tennessee due to the one-cell algae interference.

9.7 **Operability**

Once a pond is designed, little operation should be required. However, to avoid NPDES permit violations, pond flexibility is needed. Operation flexibility is best facilitated by the addition of piping and valves to each pond which allows isolation of its volume during an algal bloom.

9.8 **Upgrading Existing Systems**

There are approximately sixty existing lagoons in Tennessee which were built utilizing standards and criteria from the 1960 period. Most are single- or double-cell units which need upgrading. Many are required to meet tertiary standards. The upgrade case should, in general, utilize the guidance in this chapter or proven configurations. It is noted, however, that there are many lagoon combinations available, such as complete-mix pond, partial-mix pond, stabilization pond, HCR pond and marsh-pond (wetlands)concepts. combination of these alternatives should be based upon the effluent permit design standards as well as site economics.

January 2016 9-15 Design Criteria Ch. 9

Section 8 Disinfection





Section 8 Disinfection



1

3



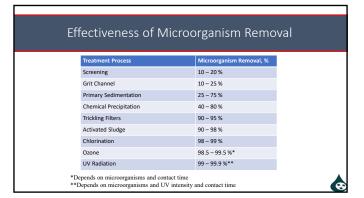
Disinfection

- The MAIN purpose of disinfection is to destroy pathogenic microorganisms and thus prevent spread of disease
- Pathogenic = disease-causing
- Ultimate measure of effectiveness is bacteriological result

2

Removal of Pathogenic Microorganisms

- Wastewater treatment removes some of the pathogenic microorganisms through these processes:
 - Physical removal through sedimentation and filtration
 - Natural die-off in an unfavorable environment
 - Destruction by chemicals introduced for treatment purposes



Disinfection vs. Sterilization

Disinfection is the destruction of all pathogenic microorganisms

Chlorination of wastewater is considered adequate when the
Fecal coliform count has been reduced to 200 cfu*/100 mL or less

E. coli count has been reduced to 126 cfu/100 mL or less

Sterilization is the destruction of ALL microorganisms



*cfu = colony forming unit

• The main objective of disinfection is to prevent the spread of disease by protecting:

- Public water supplies

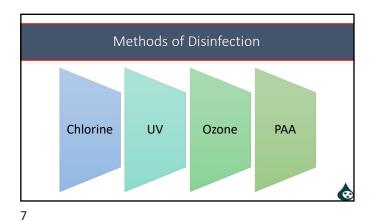
- Receiving waters used for recreational purposes

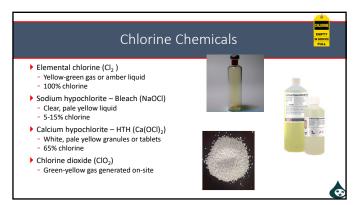
• Protect water where human contact is likely

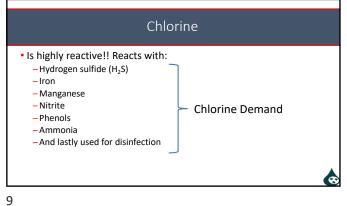
- Fisheries and shellfish growing areas

- Irrigation and agricultural waters

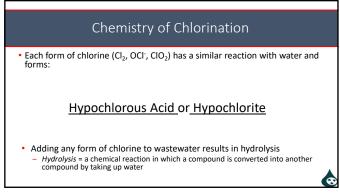
- Receiving waters that are a source of beneficial water reuse

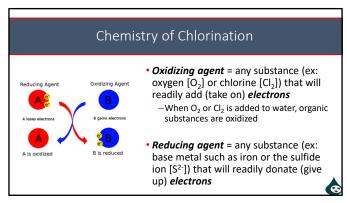






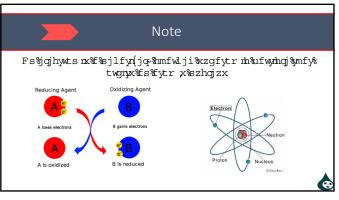
Note Chlorine demand is the difference between the amount of chlorine added to water and the amount of residual remaining after a given contact time. Demand = Dose - Residual Chlorine demand may change with dosage, time, temperature, pH, and the nature/amount of impurities in the water

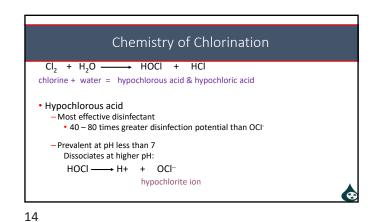




11 12

8





13

Chlorine Dioxide (ClO₂): Chemistry · Made onsite and very unstable 2NaClO₂ + Cl_2 2NaCl + 2ClO₂ Sodium Sodium Chlorine Chlorine Chlorite Chloride Dioxide $ClO_{3}^{-} + ClO_{2}^{-} + 2H^{+}$ 2ClO₂ + H20 Chlorite Hydrogen Chlorine Water Chlorate dioxide Ion

16

18

15

17

Chlorine Dose

Chlorine Dose = Chlorine Demand + Chlorine Residual

Chlorine Residual = Combined Chlorine forms + Free Chlorine

Free chlorine residual = the residual formed after the chlorine demand has been met

Combined chlorine residual = residual chlorine produced by the reaction of chlorine with substances in the water (it can be combined with ammonia, organic nitrogen, or both)

Chloramines and Chlororganics

It is still available to oxidize organic matter and kill bacteria, but not as effective as free residual

• Ammonia (NH₃) is present in all domestic wastewater
• When chlorine is added to water with NH₃, the NH₃ reacts with HOCl to form:

- Monochloramine

- Dichloramine

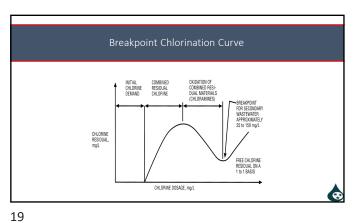
- Trichloramine

- Trichloramine

• Breakpoint chlorination occurs when the chlorine to ammonia ratio exceeds ~ 8:1

- At this point the Cl₂ has oxidized the NH₃ to nitrate or other end products

Disinfection



Chlorine Residual • Must use approved method · Limits are in NPDES permit Microorganism population usually estimated by determining MPN (Most Probable Number) -Coliform group of organisms as indicator organisms

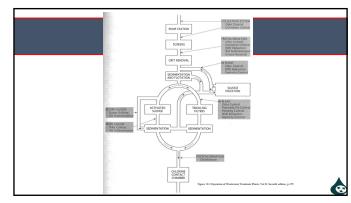
20

Factors Influencing Disinfection Injection point and method of mixing ▶ Design or shape of contact chamber ▶ Contact time Most contact chambers are designed to give 30 min contact time ► Effectiveness of upstream processes • The lower the SS, the better the disinfection ▶ Temperature Dose and type of chemical ▶ Numbers and types of microorganisms

Chlorine Demand • Chlorine demand can be caused by environmental factors such Temperature -pH – Alkalinity -Suspended solids - Biochemical and chemical oxygen demand -Ammonia nitrogen compounds

21

Chlorine Dosages for Residual	Adequate Chlorine		
Application Points for Chlorination:	Application	Dosage Range, mg/L	
Collection system	Collection System – Slime control	1 - 15	
 Prechlorination 	Treatment – Grease Removal	1 - 10	
Plant chlorination	Activated Sludge – Bulking	1 - 10	
Chlorination before filtration	Digester – Supernatant	20 - 150	
	Disinfection – Raw Wastewater	10 - 130	
Post-chlorination	Disinfection – Primary Clarifier Effluent	5 - 20	
	Disinfection – Trickling Filter Effluent	3 - 20	
	Disinfection – Activated Sludge Effluent	2 - 8	_
	Disinfection – Advanced Treatment	1-5	3



24 23

224

Prechlorination

- The addition of chlorine to wastewater at the entrance to the treatment plant, ahead of settling units and prior to the addition of other chemicals
 - -Aids in:
 - Odor control
 - Decrease BOD load
 - Settling
 - · Oil removal



Note

Ns執mj和t頭hyts%~xyjr?

Odor control
— Aeration may be most cost efficient

Corrosion control
BOD control
— Decrease the load imposed on the STP

25 26

Plant Chlorination

- Chlorine can be added to wastewater during treatment
 - The point of application depends on the desired results
- Emergency measure only, use extreme care when chlorinating in the treatment process because you may interfere or inhibit biological treatment processes
- Aids in:

27

- Control of odors
- Corrosion
- Sludge bulkingDigester foam
- Filter flies
- Trickling Filter Ponding



Chlorination Before Filtration

- Kills algae and other large biological organisms in water or in filters
 - -Biological growth may cause filters to clog which would cause the need to backwash more frequently

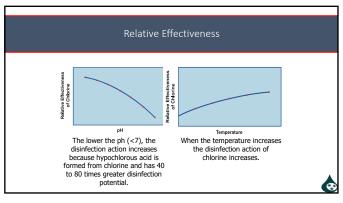
Post-chlorination

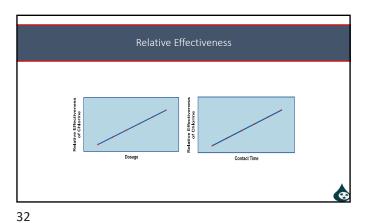
- Post-chlorination is defined as the addition of chlorine to municipal or industrial wastewater following other treatment processes
 - Point of application should be before a Chlorine Contact Chamber or Basin and after the final clarifier
 - -Sole purpose is disinfection
 - A highly nitrified effluent can be difficult to disinfect, adding 1.5 mg/L of ammonia to the effluent of the nitrification process can correct the problem

Design Criteria (10.2.2.4-5):
 Minimum 30:1 length to width ratio
 The total length of the channel created by the baffles should be 30 times the distance between the baffles
 15 min. detention time at daily peak design flow
 30 min. detention time at average design flow

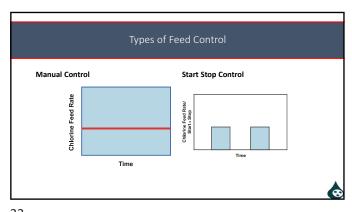
29 30

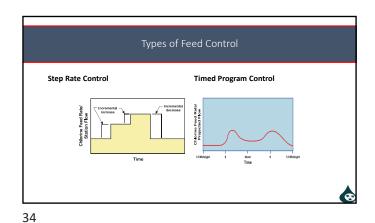
225



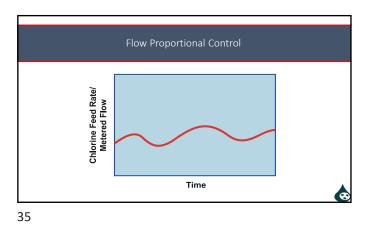


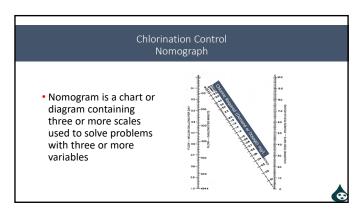
31

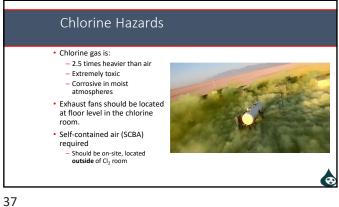


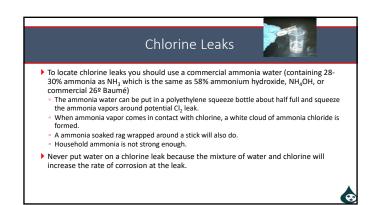


33









Chlorine Leaks • To shut down a gas chlorination system for maintenance: -Turn off the chlorine gas supply -Wait for the rotameter ball to drop to 0 lbs -Turn off the injector water supply to insure that all gas has been expelled

Physiological Response to Chlorine Gas Parts of Chlorine Gas per Million Parts of Air by Volume (ppm) 60-min inhalation without serious effects Throat irritation 30 Dangerous from ½ - 1 hour 40 Death after a few deep breaths 1,000 *OSHA regs specify that exposure to chlorine shall at NO time exceed 1 ppn

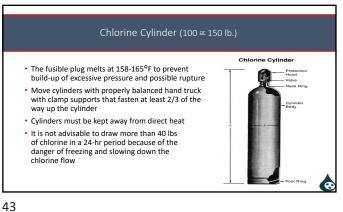
40 39

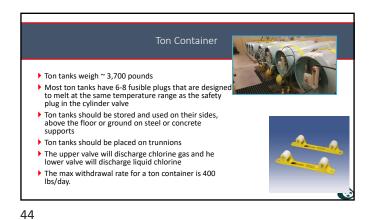


Chlorine These containers under normal conditions of temperature and pressure contain chlorine as a liquid and a gas form. If you take chlorine from the bottom of the container, it will be liquid - If you take chlorine from the top of the container, it will be gas Liquid chlorine expands in volume by 460 times as a gas at atmospheric

227

42







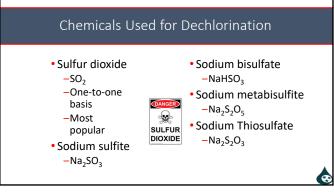
Chlorinator Vacuum fed (safer) Used to establish a feed rate in pounds per day Components include: Differential regulating valve
- V-Notch orifice with plug positioner
- Rotameter

45 46

Evaporator Installed where large amounts of chlorine are An evaporator is a hot water heater surrounding a steel tank and the liquid chlorine is evaporated to gas at 110-120°F

Dechlorination • Dechlorination is the physical or chemical removal of all traces of residual chlorine remaining after the disinfection process and prior to the discharge of the effluent to the receiving waters Removal methods: Aeration Sunlight -Long detention time Chemicals

47 48



Sulfur Dioxide (SO₂)

- Colorless gas with a characteristic pungent odor
- · Not flammable or explosive
- Not corrosive unless in a moist environment (can form sulfuric
- Detecting for sulfur dioxide leaks is done the same way for chlorine by using ammonia vapor dispenser or ammonia soaked

49

50

SO₂ Chemical Reaction

- · Reacts almost instantaneously
- Conversion of all active positive chlorine ions to the nonactive negative chloride ions
- Organic materials present may require extra SO₂
- Excess SO₂ dosage should be avoided because it will lead to:
 - 1. reduction in DO
 - 2. drop in pH
 - 3. increase in BOD/COD



- The typical application point is just before discharge into receiving stream
- This allows for maximum time for disinfection to take place





51

52

Physiological Response to Sulfur Dioxide Concentration Lowest concentration immediately irritating to throat 8-12 ppm 20 ppm Lowest concentration causing coughing Maximum allowable concentration for 8-hr exposure 10 ppm Maximum allowable concentration for 1-hr exposure 50-100 ppm Tolerable (briefly) 150 ppm 400-500 ppm Immediately dangerous concentration OSHA 8-hour TWA (Time Weighted Average) is 2 ppm and the 15-minute STEL (Short Term Exposure Limit) is 5 ppm

Ultraviolet Radiation

- Ultraviolet radiation is commonly referred to as ultraviolet light or
- With growing concern with safety of chlorine handling and the possible health effects of chlorination by-products, UV is gaining popularity
- UV disinfection is a practical alternative to chlorine disinfection



229

Ultraviolet Radiation A UV system transfers electromagnetic energy from a mercury arc lamp to an organism's genetic material. When UV radiation penetrates the cell wall of an organism, it destroys the cell's ability to reproduce UV radiation, generated by an electrical discharge through mercury vapor, penetrates the genetic material of microorganisms and retards

UV – System Components

- · Mercury arc lamps
- Ballast
- -to provide power
- Reactor

56

58

- -Single or multiple banks mounted in a
- Source of UV can either be low-pressure or medium pressure mercury arc lamp with low or high intensities.



55

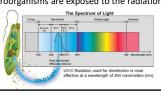
Ultraviolet Radiation

- The effectiveness of a UV system depends on:
 - Characteristics of the WW
 - Intensity of the UV radiation

their ability to reproduce

Amount of time the microorganisms are exposed to the radiation

Reactor configuration



UV – System Components

- The optimum wavelength to effectively inactivate microorganisms is in the range of 250-270 nm.
- The intensity of the radiation emitted from the lamp dissipates as the distance from the lamp increases.
- Low-pressure lamps emit essentially monochromatic light at a wavelength of 253.7 nm.
- \bullet Standard lengths of the low-pressure lamps are 0.75 and 1.5 meters with diameters of 1.5-2.0 cm.
- The ideal lamp wall temperature is between 95-122º

Low Pressure UV Lamps

- Lamp assemblies mounted in a rack(s) that are immersed in
- Can be enclosed in a vessel or in an open channel

 Enclosed in vessels in pressure systems
- Placed either horizontal and parallel to flow or vertical and perpendicular to flow
- · Number of lamps determines water depth in channel

UV – System Components

- Medium-pressure lamps are generally used for large facilities
- They have approximately 15-20 times the germicidal UV intensity of low-pressure lamps
- The medium-pressure lamp disinfect faster and has greater penetration capability because of its higher intensity.
- However, these lamps operate at higher temperatures with higher energy consumption

59

57

61

63

UV Operation

- Lamp output declines as they age
 - Operators must monitor output and replace bulbs that no longer meet design standards
- Turbidity and flow must be monitored
 - -Suspended particles can shield microorganisms from the UV light
 - Flows should be somewhat turbulent to ensure complete exposure of all organisms to the bulbs
- UV light does NOT leave a residual like chlorine
 - Bacteriological tests must be run frequently to ensure adequate disinfection is taking place
 - Microorganisms that were not killed may be able to heal themselves

Typical UV Lamp Configurations Closed vessel lamp arrangements are more typically found in drinking water plants Wastewater plants normally have UV bulbs placed in an open channel either horizontal or perpendicular to flow

Safety with UV Systems

- The light from a UV lamp can cause serious burns to your eyes
- · Always take precautions to protect your eyes and skin
- NEVER look into the uncovered sections of the UV chamber without protective glasses
- UV lamps contain mercury vapor, which is a hazardous substance that can be released if the lamp is broken

Maintenance

Quartz sleeves

62

64

- Cleaning frequency depends on water quality and treatment chemicals
- Dip modules in nitric acid or phosphoric acid for 5 minutes to remove scale
- -Cleaned by removing modules from channel or by in-channel cleaning
- -In-channel cleaning requires back-up channel and greater volume of cleaning solution
 - Precautions should be taken to protect concrete walls of channel from being damaged

Maintenance

- UV lamps
 - Service life ranges from 7,500 20,000 hours
 - Depends on

 - Level of suspended solids Frequency of on/off cycles
 - · Operating temperature of lamp electrodes
 - Lamp output drops 30-40% in first 7,500 hours
 - Lamp electrode failure is most common cause of lamp
 - Do not throw used lamps in garbage can
 - Must be disposed properly due to mercury content

UV - Advantages

- Effective at inactivating most viruses, spores and cysts
- · Physical process rather than a chemical disinfectant
 - Eliminates the need to generate, handle, transport or store toxic/hazardous or corrosive chemicals
- No residual effect that can be harmful to humans or aquatic life
- User-friendly for operators
- Shorter contact time when compared with other disinfectants
 - Approximately 20-30 seconds with low-pressure lamps
- · Requires less space than other methods

65

67

69

UV - Disadvantages

- Low dose may not effectively inactivate some viruses, spores or cysts
- Organisms can sometimes repair and reverse the destructive effects of UV through a "repair mechanism" known as photo reactivation, or in the absence of light known as "dark repair"
- Preventive maintenance program is necessary to control fouling of tubes
- Turbidity and TSS in the WW can render UV disinfection ineffective
 - UV disinfection with low-pressure lamps is not as effective for secondary effluent with TSS levels above 30 mg/L
- Not as cost-effective as chlorination, bust costs are competitive when chlorination and dechlorination is used and fire codes are met

Ozone

• Ozone forms naturally in the atmosphere

$$O_2$$
 + Energy $\rightarrow O + O$
 $O + O_2 \rightarrow O_3$

- Wastewater disinfection systems typically produce ozone by electrical methods

 Extremely dry air containing oxygen molecules (O₂)exposed to high-voltage discharge creates ozone (O₃)
- Very strong oxidant and virucide

68

70

 Ozone is generated on-site because it is unstable and decomposes to elemental oxygen in a short amount of time after generation.

æ

Ozonation

- Ozone's increased use as a disinfectant is being spurred by increasing regulations around the world on the discharge of pharmaceuticals and endocrine-disrupting pollutants
- Research into ozone's efficacy in eliminating these pollutants and producing safe reuse water may lead to more common use of ozone

Effects of Ozone on Bacteria

Sterilization principle



- Direct oxidation/destruction of cell wall
- Reactions with radical byproducts of ozone decomposition
- Damage to nucleic acids (purines and pyrimidines) inside the cell, which alters genetic material and prevents cell replication
- It is generally believed that the bacteria are destroyed by cell lysis

Ozone

- Ozone is fed into a down-flow contact chamber to transfer ozone from the gas bubble into the bulk liquid while providing sufficient contact time for disinfection
- Because it is consumed quickly, it must be contacted uniformly in a near plug flow contactor
- Residual ozone measured by the iodometric method
- · Dissolved ozone measured by Indigo test

Compression and purpose of the state production of the

71 72

Ozone

- · Effectiveness depends on:
 - -Susceptibility of the target organisms
 - –Contact time

73

- –Concentration of ozone
- The key process control guidelines are dose, mixing, and contact time



74

Safety

- Ozone is a toxic gas and is a hazard to plants and animals
- · When ozone breaks down in the atmosphere, the resulting pollutants can be very harmful
- Ozone contactors must have a system to collect ozone off-gas.
 - -Ozone generating installations must include a thermal or catalytic ozone destroyer

Ozone - Advantages

Maintenance

-Should be done by a factory representative or an operator trained by

· Inspect electrical equipment and pressure vessels monthly

· Conduct a yearly preventive maintenance program

Lubricate moving parts according to manufacturer's

- More effective than chlorine in destroying viruses and bacteria
- · Short contact time (10-30 min)

the manufacturer

recommendations

- No harmful residues left in water
- No re-growth of microorganisms
- Except for those protected by particulates in water Generated on-site

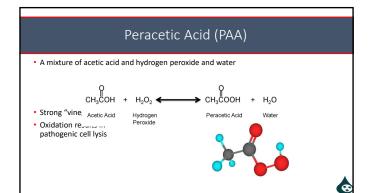
76

- Fewer safety problems associated with shipping and handling
- Elevates DO levels in effluent
 - Can eliminate needs for post aeration
 - Can raise DO levels in receiving stream

75

Ozone - Disadvantages

- · Low dose may not effectively inactivate some viruses, spores and cysts
- · More complex technology
- Requiring more complex equipment and efficient contacting systems
- Requiring corrosive-resistant materials such as stainless steel
- Not economical for WW with high levels of solids, BOD, COD or total organic carbon
- Extremely irritating and possibly toxic to humans at concentrations of 1 ppm or greater
- · Cost can be high in capital and power intensiveness



77 78

233

Disinfection

Peracetic Acid (PAA) - Advantages

- · Alternative to chlorine
 - No disinfection byproducts (DBPs) that could be toxic to aquatic life
 - THMs, HAAs
- No removal step (ex: dechlorination)
- Simple to operate
- Chlorine contact chambers can often be retrofitted
- Safety in transportation/storage
- Lower freezing point/more stable than chlorine

79

Peracetic Acid (PAA) - Disadvantages

- More expensive
- PAA seems to be less effective for spores, viruses and protozoa (Giardia and Cryptosporidium)
- Can present an oxygen demand

à

80

Peracetic Acid (PAA)

- Effectiveness depends on:
 - -Susceptibility of the target organisms
 - -Contact time
 - -Concentration of PAA





Peracetic Acid (PAA)

- Approval Process for Tennessee:
 - -Tennessee does not have numeric water quality criteria
 - Bench-scale, partial pilot scale or full scale pilot test to determine the
 efficacy of the disinfection within the PAA concentration restriction
 imposed by the WET test results in the receiving stream using a specific
 PAA formulation
 - We recommend you contact the division early in the process to understand the specific expectations

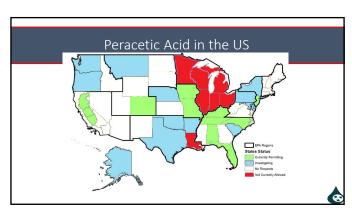
82

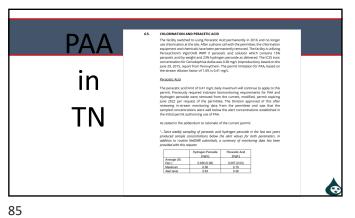
Peracetic Acid - Limits

- There is not currently a water quality criteria so limits are site specific based on the study results.
- Monitor and Report

81

- Hydrogen Peroxide
- Peracetic Acid
- The is a 1 mg/L limit published by the industries







Disinfection Vocabulary

	causing a, such as Typhoid.		
2.	The destruction of all pathogenic microorganisms is called, which is		
	not to be confused with, in which all microorganisms		
	(pathogenic and nonpathogenic) are destroyed.		
3.	Elemental chlorine (Cl ₂), which is in a liquid or gaseous form, is also known as		
	It combines with water to form hypochlorous (HOCl) and hydrochloric		
	(HCl) acids. In wastewater, it will combine with ammonia or nitrogen (or other organic compounds to form combined chlorine compounds.		
4.	is the concentration of residual chlorine that is produced		
	by the reaction of chlorine with substances in the water (ex: combined with ammonia, organic		
	nitrogen, or both as a chloramine) and yet is still available to oxidize organic matter and kill bacteria		
	although it is not as effective as free residual.		
5.	Any substance, such as oxygen (O_2) or chlorine (Cl_2) , that will readily add (take on) electrons is called		
	an When O_2 or Cl_2 is added to water or wastewater,		
	organic substances are oxidized. The opposite is a Reducing Agent.		
6.	The residual formed after the chlorine demand has been met is		
7.	The addition of chlorine to the plant discharge or effluent, following plant treatment, is called .		
8.	The concentration of chlorine present in water after the chlorine demand has been satisfied is the Expressed in terms of total chlorine residual, it includes		
	both the free and combined/chemically bound chlorine residuals.		
9.	Any substance, such as base metal (iron) or the sulfide ion (S ² -),that will readily donate (give up)		
	electrons is called a The opposite is an Oxidizing Agent.		
10.	The demand by inorganic and organic materials is referred to as		
	In other words, it is the difference between the amount of chlorine added to water or wastewater		
	and the amount of residual chlorine remaining after a given contact time.		
11.	The addition of chlorine in the collection system, at the headworks, or prior to any other treatments		
	processes (mainly for odor and corrosion control) is called		

13.	This alternate type of disinfection is more effective than chlorine, leaves no harmful residuals, and is generated onsite by exposing oxygen molecules to an energy source and converting them to an unstable gas:				
14.	The process of adding chlorine to water to kill disease-causing organisms is known as Generally the purpose is disinfection, but frequently it is used to accomplish other biological or chemical results.				
15.	5 uses ultraviolet light to destroy microorganisms by damaging their genetic material.				
<u>W</u>	ord Bank:				
Chlorination		Waterborne disease			
Pat	hogenic	Free chlorine			
Residual chlorine (aka Chlorine residual)		Disinfection			
Oxidizing agent		Prechlorination			
Combined chlorine residual		Reducing agent			
Postchlorination		Ozonation			
Free chlorine residual		Sterilization			
UV	disinfection	Breakpoint Chlorination			
Chl	orine demand				

CHAPTER 10

Disinfection

10.1 General

- 10.1.1 Requirement for Disinfection
- 10.1.2 Methods of Disinfection
- 10.1.3 Dechlorination

10.2 **Chlorination**

- 10.2.1 General
- 10.2.2 Design Considerations
- 10.2.3 Design Details
- 10.2.4 Safety

Alternate Methods 10.3

- 10.3.1 Ozonation
- 10.3.2 Ultraviolet Disinfection

DISINFECTION

10.1 General

10.1.1 Requirement for Disinfection

Proper disinfection of treated wastewater before disposal is required for all plants (with the exception of some land application systems) to protect the public health.

Disinfection as a minimum shall:

- a. Protect public water supplies
- b. Protect fisheries and shellfish waters
- c. Protect irrigation and agricultural waters
- d. Protect water where human contact is likely

10.1.2 Methods of Disinfection

10.1.2.1 Chlorination

Chlorination using dry chlorine (see definition in following section) is the most commonly applied method of disinfection and should be used unless other factors, including chlorine availability, costs, or environmental concerns, justify an alternative method.

10.1.2.2 Ozonation

Ozonation may be considered as an alternative to chlorination for the reasons described above. Ozonation is considered as Developmental Technology, and should only be considered for very large installations.

10.1.2.3 Other

Other potential methods of disinfection, such as by ultraviolet light, are available and their application will be considered on a case-by-case basis.

10.1.3 Dechlorination

Capability to add dechlorination should be considered in all new treatment plants. Dechlorination of chlorinated effluents shall be provided when permit conditions dictate the need.

10.2 Chlorination

10.2.1 General

10.2.1.1 Forms of Chlorine

a. Dry Chlorine

Dry chlorine is defined as elemental chlorine existing in the liquid or gaseous phase, containing less than 150 mg/l water. Unless otherwise stated, the word "chlorine" wherever used in this section refers to dry chlorine.

b. Sodium Hypochlorite

Sodium hypochlorite may be used as an alternative to chlorine whenever dry chlorine availability, cost, or public safety justifies its use. The requirements for sodium hypochlorite generation and feeding will be determined on a case-by-case basis.

c. Other

Other chlorine compounds such as chlorine dioxide or bromine chloride may be used as alternatives to chlorine whenever cost or environmental concerns justify their use. The acceptability of other chlorine compounds will be determined on a case-by-case basis.

10.2.1.2 Chlorine Feed Equipment

Solution-feed vacuum-type chlorinators are generally preferred for large installations. The use of hypochlorite feeders of the positive displacement type may be considered. Dry chlorine tablet type feeders may also be considered for small flows, into large streams.

Liquid chlorine evaporators should be considered where more than four 1-ton containers will be connected to a supply manifold.

10.2.1.3 Chlorine Supply

a. Cylinders

Cylinders should be considered where the average daily chlorine use is 150 pounds or less. Cylinders are available in 100-pound or 150-pound sizes.

b. Containers

The use of 1-ton containers should be considered where the average daily chlorine consumption is over 150 pounds.

c. Large-Volume Shipments

At large installations, consideration should be given to the use of truck or railroad tank cars, or possibly barge tank loads, generally accompanied by gas evaporators.

10.2.1.4 Chlorine Gas Withdrawal Rates

The maximum withdrawal rate for 100- and 150- pound cylinders should be limited to 40 pounds per day per cylinder.

When gas is withdrawn from 2,000-pound containers, the withdrawal rate should be limited to 400 pounds per day per container.

10.2.2 Design Considerations

10.2.2.1 General

Chlorination system designs should consider the following design factors:

Flow

Contact time

Concentration and type of chlorine residual

Mixing

pН

Suspended solids

Industrial wastes

Temperature

Concentration of organisms

Ammonia concentration

10.2.2.2 Capacity

Required chlorinator capacities will vary, depending on the use and point of application of the chlorine. Chlorine dosage should be established for each individual situation, with those variables affecting the chlorine reaction taken into consideration. For normal wastewater, the following dosing capacity may be used as a guideline.

Type of Treatment	Dosage Capacity* (mg/l)
Prechlorination for Odor Control	20-25
Activated Sludge Return	5-10
Trickling Filter Plant Effluent (non-nitrified)	3-15
Activated Sludge Plant Effluent (non-nitrified)	2-8
Tertiary Filtration Effluent	1-6
Nitrified Effluent	2-6
Stabilization Pond Effluent	Up to 35

^{*} Based on Average Design Flow.

The design should provide adequate flexibility in the chlorination equipment and control system to allow controlled chlorination at minimum and peak flows over the entire life of the treatment plant. Special consideration should be given to the chlorination requirements during the first years of operation to ensure the chlorination system is readily operable at less than design flows without overchlorination. Chlorination equipment should operate between 25% and 75% of total operating range, to allow for adjusting flexibility at design average flow.

10.2.2.3 Mixing

The mixing of chlorine and wastewater can be accomplished by hydraulic or mechanical mixing.

Hydraulic mixing is preferred in smaller plants over mechanical mixing and should be done according to the following criteria.

a. Pipe Flow:

A Reynolds Number of greater than or equal to 1.9×10^4 is required.

Pipes up to 30 inches in diameter: chlorine injected into center of pipe.

Pipes greater than 30 inches in diameter: chlorine injected with a grid-type diffuser.

Chlorine applied at least 10 pipe diameters upstream from inlet to contact tank.

b. Open channel flow:

A hydraulic jump with a minimum Froude Number of 4.5 is necessary to provide adequate hydraulic mixing. Point of chlorine injection must be variable because jump location will change with changes in flow.

When mechanical mixing must be used, the following criteria apply:

Use where Reynolds Number for pipe flow is less than 1.9 X 10⁴ or for open channel flow without a hydraulic jump.

A mixer-reactor unit is necessary that provides 6 to 18 seconds contact.

Inject chlorine just upstream from mixer.

Mixer speed a minimum of 50 revolutions per minute (rpm).

Jet Chlorinators may be used in a separate chamber from the contact chamber.

The contact chamber shall conform to Section 10.2.2.4 with an average design flow minimum detention time reduced to 15 minutes and a peak detention time of 7.5 minutes.

10.2.2.4 Contact Period

Contact chambers shall be sized to provide a minimum of 30 minutes detention at average design flow and 15 minutes detention at daily peak design flow, whichever is greater. Contact chambers should be designed so detention times are less than 2 hours for initial flows.

10.2.2.5 Contact Chambers

The contact chambers should be baffled to minimize short-circuiting and backmixing of the chlorinated wastewater to such an extent that plug flow is approached. It is recommended that baffles be constructed parallel to the longitudinal axis of the chamber with a minimum length-to-width ratio of 30:1 (the total length of the channel created by the baffles should be 30 times the distance between the baffles). Shallow unidirectional contact chambers should also have cross-baffles to reduce short-circuiting caused by wind currents.

Provision shall be made for removal of floating and settleable solids from chlorine contact tanks or basins without discharging inadequately disinfected effluent. To accomplish continuous disinfection, the chlorine contact tank should be designed with duplicate compartments to permit draining and cleaning of individual compartments. A sump or drain within each compartment, with the drainage flowing to a raw sewage inlet, shall be provided for dewatering, sludge accumulation, and maintenance. Unit drains shall not discharge into the outfall pipeline. Baffles shall be provided to prevent the discharge of floating material.

A readily accessible sampling point shall be provided at the outlet end of the contact chamber.

In some instances, the effluent line may be used as chlorine contact chambers provided that the conditions set forth above are met.

10.2.2.6 Dechlorination

a. Sulfur Dioxide

Sulfur dioxide can be purchased, handled, and applied to wastewater in the same way as chlorine. Sulfur dioxide gas forms sulfurous acid, a strong reducing agent, when combined with water. When mixed with free and combined chlorine residuals, sulfurous acid will neutralize these active chlorine compounds to the nontoxic chloride ion.

Sulfur dioxide dosage required for dechlorination is 1 mg/l of SO₂ for 1 mg/l of chlorine residual expressed as Cl₂. Reaction time is essentially

instantaneous. Detention time requirements are based on the time necessary to assure complete mixing of the sulfur dioxide.

b. Other Methods

For very small treatment systems, detention ponds should be considered for dechlorination.

Design rationale and calculations shall be submitted upon request to justify the basis of design for all major components of other dechlorination processes.

10.2.2.7 Sampling, Instrumentation, and Control

For treatment facility designs of 0.5 mgd and greater, continuously modulated dosage control systems should be used. The control system should adjust the chlorine dosage rate to accommodate fluctuations in effluent chlorine demand and residual caused by changes in waste flow and waste characteristics with a maximum lag time of five minutes. These facilities should also utilize continuous chlorine residual monitoring.

Flow proportional control is preferred over manual control for smaller facilities and may be required on a case-by-case basis. The design shall shut off the chlorination for small systems where the flow is zero, such as late at night.

In all cases where dechlorination is required, a compound loop control system or equivalent should be provided.

All sample lines should be designed so that they can be easily purged of slimes and other debris and drain or be protected from freezing.

Alarms and monitoring equipment that adequately alert the operators in the event of deficiencies, malfunctions, or hazardous situations related to chlorine supply metering equipment, leaks, and residuals may be required on a case-by-case basis.

Design of instrumentation and control equipment should allow operation at initial and design flows.

10.2.2.8 Residual Chlorine Testing

Equipment should be provided for measuring chlorine residual. There are five EPA accepted methods for analysis of total residual chlorine and they are:

- 1) Ion Selective Electrode,
- 2) Amperometric End Point Titration Method,
- 3) Iodometric Titration Methods I & II,
- 4) DPD Colormetric Method and,
- 5) DPD Ferrous Titrimetric Method.

Where the discharge occurs in critical areas, the installation of facilities for continuous automatic chlorine residual analysis and recording systems may be required.

10.2.3 Design Details

10.2.3.1 Housing

a. General

An enclosed structure shall be provided for the chlorination equipment.

Chlorine cylinder or container storage area shall be shaded from direct sunlight.

Chlorination systems should be protected from fire hazards, and water should be available for cooling cylinders or containers in case of fire.

Any building which will house chlorine equipment or containers should be designed and constructed to protect all elements of the chlorine system from fire hazards. If flammable materials are stored or processed in the same building with chlorination equipment (other than that utilizing hypochlorite solutions), a firewall should be erected to separate the two areas.

If gas chlorination equipment and chlorine cylinders or containers are to be in a building used for other purposes, a gastight partition shall separate this room from any other portion of the building. Doors to this room shall open only to the outside of the building and shall be equipped with panic hardware. Such rooms should be at or above ground level and should permit easy access to all equipment.

A reinforced glass, gastight window shall be installed in an exterior door or interior wall of the chlorinator room to permit the chlorinator to be viewed without entering the room.

Adequate room must be provided for easy access to all equipment for maintenance and repair. The minimum acceptable clearance around and in back of equipment is 2 feet, except for units designed for wall or cylinder mounting.

b. Heat

Chlorinator rooms should have a means of heating and controlling the room air temperature above a minimum of 55° F. A temperature of 65° F is recommended.

The room housing chlorine cylinders or containers in use should be maintained at a temperature less than the chlorinator room, but in no case less than 55° F unless evaporators are used and liquid chlorine is withdrawn.

All rooms containing chlorine should also be protected from excess heat.

The room containing ozone generation units shall be maintained above 35°F at all times

c. Ventilation

All chlorine feed rooms and rooms where chlorine is stored should be force-ventilated, providing one air change per minute, except "package" buildings with less than 16 square feet of floor space, where an entire side opens as a door and sufficient cross-ventilation is provided by a window. For ozonation systems, continuous ventilation to provide at least 6 complete air changes per hour should be installed. The entrance to the air exhaust duct from the room should be near the floor and the point of discharge should be so located as not to contaminate the air inlet to any building or inhabited areas. The air inlet should be located to provide cross-ventilation by air at a temperature that will not adversely affect the chlorination equipment.

Chlorinators and some accessories require individual vents to a safe outside area. The vent should terminate not more than 25 feet above the chlorinator or accessory and have a slight downward slope from the highest point. The outside end of the vent should bend down to preclude water entering the vent and be covered with a screen to exclude insects.

d. Electrical

Electrical controls for lights and the ventilation system should operate automatically when the entrance doors are opened. Manually controlled override switches should be located adjacent to and outside of all entrance doors, with an indicator light at each entrance. Electrical controls should be excluded, insofar as possible, from rooms containing chlorine cylinders, chlorine piping, or chlorination equipment.

e. Dechlorination equipment (SO2) shall not be placed in the same room as the Cl2 equipment. SO2 equipment is to be located such that the safety requirements of handling Cl2 are not violated in any form or manner.

10.2.3.2 Piping and Connections

a. Dry Chlorine

Piping systems should be as simple as possible, with a minimum number of joints; piping should be well supported, adequately sloped to allow drainage, protected from mechanical damage, and protected against temperature extremes.

The piping system to handle gas under pressure should be constructed of Schedule 80 black seamless steel pipe with 2,000-pound forged steel fittings. Unions should be ammonia type with lead gaskets. All valves should be Chlorine Institute-approved. Gauges should be equipped with a silver protector diaphragm.

Piping can be assembled by either welded or threaded connections. All threaded pipe must be cleaned with solvent, preferably trichlorethylene, and dried with nitrogen gas or dry air. Teflon tape should be used for thread lubricant in lieu of pipe dope.

b. Injector Vacuum Line

The injector vacuum line between the chlorinator and the injector should be Schedule 80 PVC or fiber cast pipe approved for moist chlorine use.

c. Chlorine Solution

The chlorine solution lines can be Schedule 40 or 80 PVC, rubber-lined steel, saran-lined steel, or fiber cast pipe approved for moist chlorine use. Valves should be PVC, PVC-lined, or rubber-lined.

10.2.3.3 Water Supply

An ample supply of water shall be available for operating the chlorinator. Where a booster pump is required, duplicate equipment shall be provided, and, when necessary, standby power as well. When connection is made from domestic water supplies, equipment for backflow prevention shall be provided. Where treated effluent is used, a wye strainer shall be required. Pressure gauges should be provided on chlorinator water supply lines.

10.2.3.4 Standby Equipment and Spare Parts

Standby chlorination capabilities should be provided which will ensure adequate disinfection with any unit out of operation for maintenance or repairs. An adequate inventory of parts subject to wear and breakage should be maintained at all times.

10.2.3.5 Scales

Scales shall be provided at all plants using chlorine gas. At large plants, scales of the indicating and recording type are recommended. Scales shall be provided for each cylinder or container in service; one scale is adequate for a group of cylinders or containers connected to a common manifold. Scales should be constructed of or coated with corrosion-resistant material. Scales shall be recommended for day tanks when using HTH.

10.2.3.6 Handling Equipment

Handling equipment should be provided as follows for 100- and 150-pound cylinders:

A hand truck specifically designed for cylinders

A method of securing cylinders to prevent them from falling over

Handling equipment should be provided as follows for 2,000-pound containers:

Two-ton-capacity hoist

Cylinder lifting bar

Monorail or hoist with sufficient lifting height to pass one cylinder over another cylinder trunnions to allow rotating the cylinders for proper connection.

10.2.3.7 Container Space

Sufficient space should be provided in the supply area for at least one spare cylinder or container for each one in service.

10.2.3.8 Automatic Switchover of Cylinders and Containers

Automatic switchover of chlorine cylinders and containers at facilities having less than continuous operator attendance is desirable and will be required on a case-by-case basis.

10.2.4 Safety

10.2.4.1 Leak Detection and Controls

A bottle of 56% ammonium hydroxide solution shall be available for detecting chlorine leaks.

All installations utilizing 2,000-pound containers and having less than continuous operator attendance shall have suitable continuous chlorine leak detectors. Continuous chlorine leak detectors would be desirable at all installations. Whenever chlorine leak detectors are installed, they should be connected to a centrally located alarm system and shall automatically start exhaust fans.

10.2.4.2 Breathing Apparatus

At least one gas mask in good operating condition and of a type approved by the National Institute for Occupational Safety and Health (NIOSH) as suitable for high concentrations of chlorine gas shall be available at all installations where chlorine gas is handled and shall be stored outside of any room where chlorine is used or stored. Instructions for using, testing, and replacing mask parts, including canisters, shall be posted. At large installations, where 1-ton containers are used, self-contained air breathing apparatus of the positive pressure type shall be provided.

10.2.4.3 Container Repair Kits

All installations utilizing 1-ton containers should have Chlorine Institute Emergency Container Kits. Other installations using cylinders should have access to kits stored at a central location.

10.2.4.4 Piping Color Codes

It is desirable to color code all piping related to chlorine systems.

10.3 Alternate Methods

10.3.1 Ozonation

10.3.1.1 Application

Ozonation may be substituted for chlorination whenever chlorine availability, cost, or environmental benefits justify its application.

Ozone is generated on-site from either air or high-purity oxygen. Ozonation should be considered if high-purity oxygen is available at the plant for other processes.

10.3.1.2 Design Basis

The design requirements for ozonation systems should be based on pilot testing or similar full-scale installations.

As a minimum, the following design factors should be considered:

- a. Ozone dosage
- b. Dispersion and mixing of ozone in wastewater
- c. Contactor design

All design criteria shall be submitted upon request to justify the basis of design of the ozonation system. The detailed design requirements will be determined on a case-by-case basis.

10.3.2 Ultraviolet Disinfection

10.3.2.1 Application

UV disinfection may be substituted for chlorination, particularly whenever chlorine availability, cost, or environmental benefits justify its application. For tertiary treatment plants where dechlorination is required or chlorine toxicity is suspected, UV disinfection is a viable alternative.

10.3.2.2 Design Basis

In the design of UV disinfection units there are three basic areas that should be considered:

- a. Reactor hydraulics
- b. Factors affecting transmission of UV light to the microorganisms
- c. Properties of the wastewater being disinfected.

UV disinfection is considered as Developmental Technology and all design criteria shall be submitted upon request to justify the basis of the UV disinfection system. The detailed design requirements will be determined on a case-by-case basis.

Section 9 Effluent Disposal

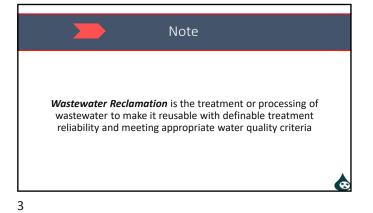






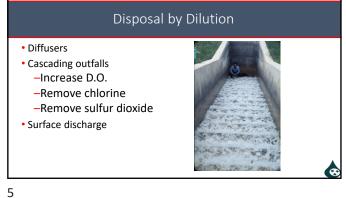
Effluent Disposal Dilution Lakes Rivers - Streams **Wastewater Reclamation** - Land application Underground disposal Groundwater recharge basins

2



Disposal by Dilution • Treatment required prior to discharge: -Stabilize waste -Protect public health -Meet discharge requirements Site specific · Most common method of effluent disposal

4





Land Treatment Systems

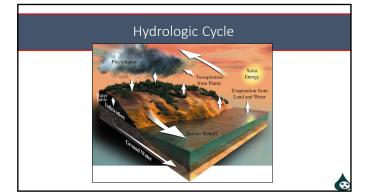
- When high-quality effluent or even zero-discharge is required, land treatment offers a means of reclamation or ultimate disposal
- Land treatment = the controlled application of wastewater to the land surface to achieve a designed degree of treatment through physical, chemical, and biological processes within the plant-soilwater matrix.
 - Soil texture, soil structure, permeability, infiltration, available water capacity, and cation exchange capacity
 - Adsorption and precipitation are the main processes involved in the retention of wastes in the soil

Land Treatment Systems

- Simulate natural pathways of treatment
- Use soil, plants, and bacteria to treat and reclaim wastewater
- Treatment is provided by natural processes as effluent moves through soil and plants
- Some of wastewater is lost by evaporation and transpiration
- Remainder returns to hydrologic cycle through surface runoff or percolation to groundwater

7

8

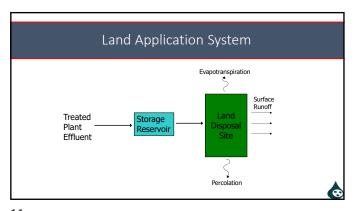


Land Application System

- Treatment prior to application
- Transmission to the land treatment site
- Storage
- · Distribution over the site
- Runoff recovery system
- Crop systems

9

10



3 Major Land Treatment Processes

1. Slow rate

- Irrigation, ridge-and-furrow, border strip flooding
 - Vegetation uses portion of flow, some goes to groundwater
 - Organic wastes removed by filtration and adsorption
 - Designed for no surface runoff
- 2. Rapid infiltration
 - Moderately and highly permeable soils by spreading basins or sprinklers (vegetative cover not used)
 - Treated effluent collected by drain tiles and discharged to surface water or it
- 3. Overland flow
 - Highly impermeable soils, applied at upper reaches of grass covered slopes, flows over vegetation, surface runoff collected

(3)

12

• Control of ponding problems - Percolation - Crop selection - Drainage tiles • Install PVC laterals below ground • Potential odor release with spray systems • Routine inspection of equipment • Plan "B" in case system fails

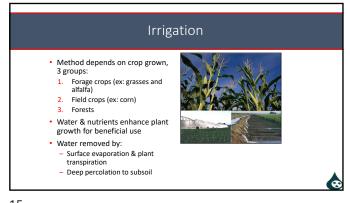
Wastewater Reclamation:
Land Application

• Irrigation most common:
• Ridge and furrow
• Sprinklers
• Surface/drip systems
• Border strip flooding
• Overland flow
• Wetlands treatment

Wastewater Treatment Plant & Poplar Tree Reuse System; Woodburn, Oregon

13 14

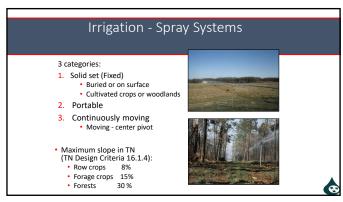
· Nitrogen is the major limiting factor



• Irrigation application of wastewater over relatively flat area, usually by spray (sprinklers) or surface spreading
• Water and nutrients are absorbed by plants and soil
• In soil, organic matter is oxidized by bacteria

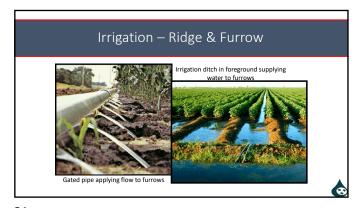
15 16

Most common land treatment in US Spray: fixed or moving Surface spreading: controlled flooding or ridge & furrow Climate affects efficiency If ground freezes, subsurface seepage is greatly reduced. Therefore storage of treated wastewater may be necessary Ex: lawns, parks, golf courses, pastures, forests, fodder crops (corn, alfalfa), fiber crops, cemeteries





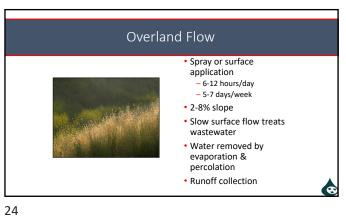
Irrigation – Ridge & Furrow Ridge and Furrow = a series of interconnected ditches (furrows) which allow for the distribution, infiltration, and treatment of wastewater Wastewater flows through furrows between rows of crop Wastewater slowly percolates into Wastewater receives partial treatment before it is absorbed by plants



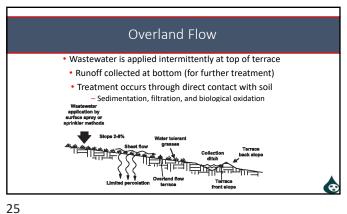
<u>Parameter</u>	<u>% Removal</u>
BOD	98
COD	80
Suspended Solids	98
Nitrogen	85
Phosphorus	95
Metals	95
Microorganisms	98

21 22

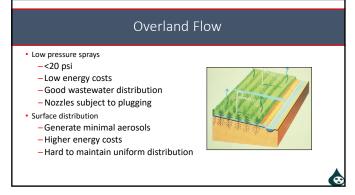
Irrigation – Removal Efficiencies	
 Under normal circumstances: Water and nitrogen are absorbed by crops Phosphorus and metals are adsorbed by soil particles Bacteria is removed by filtration Viruses are removed by adsorption 	
 Nitrogen cycle Secondary effluent contains ammonia, nitrate and organic nitrogen Ammonia and organic nitrogen are retained in soil by adsorption and ion exchange, then oxidized to nitrate Major removal mechanisms are ammonia volatilization, crop uptake and denitrification 	æ



23







		Distribution Methods			
	Methods	<u>Advantages</u>	<u>Limitations</u>		
gs	General	Low energy costs Minimize aerosols and wind drift Small Buffer zones	Difficult to achieve uniform distribution Moderate erosion potential		
Methods	Gated Pipe	Same as General, plus: Easy to clean Easiest to balance hydraulically	Same as General, plus: Potential for freezing and settling		
Surface	Slotted or Perforated Pipe	Same as General	Same as Gated Pipe, plus: Small openings clog Most difficult to balance hydraulically		
S	Bubbling Orifices	Same as General, plus: Not subject to freezing/settling Only the orifice must be leveled	Same as General, plus: Difficult to clean when clogged		
Low	-pressure Sprays	Better distribution than surface methods Less aerosols than sprinkler Low energy costs	Nozzles subject to clogging More aerosols and wind drift than surface methods		
Spri	nklers	Most uniform distribution	High energy costs Aerosol and wind drift potential		

27 28

Suitable Grasses					
Co	ommon Name	Perennial or Annual	Rooting Characteristics	Method of Establishment	Growing Height (cm)
	Reed canary	Perennial	sod	seed	120-210
Grass	Tall fescue	Perennial	bunch	seed	90-120
Ģ	Rye grass	Annual	sod	seed	60-90
Season	Redtop	Perennial	sod	seed	60-90
Se	KY bluegrass	Perennial	sod	seed	30-75
Cool	Orchard grass	Perennial	bunch	seed	15-60
_	Common Bermuda	Perennial	sod	seed	30-45
Season	Coastal Bermuda	Perennial	sod	sprig	30-60
Warm :	Dallis grass	Perennial	bunch	seed	60-120
Wa	Bahia	Perennial	sod	seed	60-120

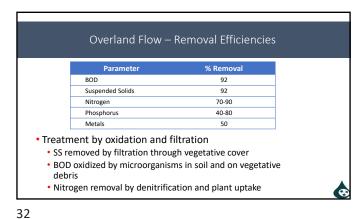
Suitable Grasses • Well established plant cover is essential for efficient performance • Primary purpose of plants is to facilitate treatment of wastewater • Planting a mixture of different grasses usually gives best results • Ryegrass used as a nurse crop; grows quickly until other grasses are established

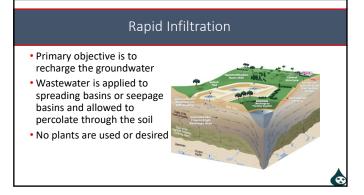
Suitable Grasses

- Cool Season Grass plant from Spring through early Summer or early Fall to late Fall
- Warm Season Grass generally should be planted from late Spring through early Fall
- Planting time affected by expected rainfall, location, climate, grass variety, etc
- Amount of seed required to establish cover depends on:
 - Expected germination
 - -Type of grass

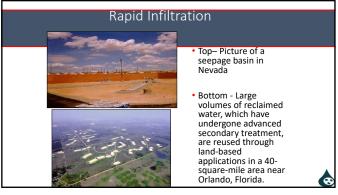
31

- Water availability
- -Time available for crop development



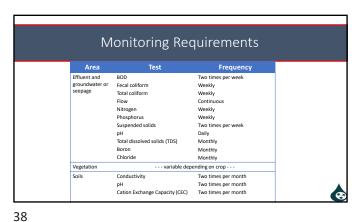


33 34





Land Treatment Limitations · Excessive nitrate ions reach groundwater -Rain can soak soil so that no treatment is achieved Do not apply nitrate in excess of crop's nitrogen uptake ability -Excessive nitrate in groundwater can lead to methylmoglobenemia (blue baby syndrome) Too much nitrate consumed by child leads to nitrate in stomach and intestines where nitrogen is absorbed into bloodstream and it bonds to red blood cells preventing them from carrying oxygen. Baby becomes oxygen deprived, turns blue and



37

Water Quality Indicators

- Receiving water measurements = tests used to determine the effect of discharge on the receiving waters and on the beneficial uses (water supply, recreation, fishery) of the receiving waters after effluent has mixed with receiving waters. receiving waters
- To measure impact:

39

41

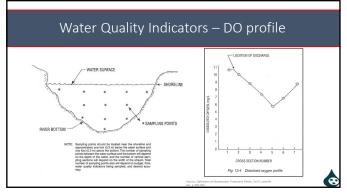
- Take a measurement upstream (not affected) and downstream (affected) and compare the two results
- "Oxygen profile" (Dissolved oxygen) to get a good measure of the effect of the effluent

 Measure the DO at several different cross sections downstream from discharge to find out where the lowest DO level occurs

Water Quality Indicators

- To determine impact, the following questions must be answered:
- 1. What are the characteristics upstream?
 - Temperature
 - Dissolved oxygen (DO)
- 2. What are the characteristics downstream?
- 3. If upstream and downstream are different, does the discharge cause the difference?
- 4. Are the downstream characteristics in violation of established standards or objectives
- 5. If downstream is in violation, did the discharge

40



Water Quality Indicators

- If results do not look correct, do not reject outright. Investigate and attempt to identify the reasons for the result.
- Sampling errors, testing errors, recording errors
- Sudden drop in DO downstream (without a similar drop upstream) indicates that the plant's BOD removal efficiency has decreased
- Sudden drop in DO could be caused by increase in temperature due to an industrial or stormwater discharge
- · Sudden changes in effluent may be due to:
- 1. Process failure
- Sudden increase in flow quantity
- Change in influent characteristics such as industrial waste discharges into the system

263

Water Quality Indicators

- Plant effluent analyzed prior to discharge:
 - -In-stream: pH, D.O., temperature
 - -In laboratory: BOD, COD, suspended solids, fecal coliforms, E. coli, N, P
- Disposal by dilution may require analysis of receiving stream upstream & downstream
 - -WET testing (Whole Effluent Toxicity)

43

Whole Effluent Toxicity (WET) test refers to the combined toxic effect to aquatic organisms from all pollutants contained in a wastewater effluent

- Looks at the effluent as a single component

WET tests measure wastewater's effects on specific test organisms' ability to survive, grow and reproduce

Acute toxicity

- Short term, lethal effects

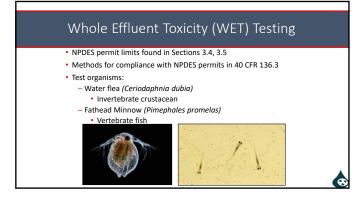
- "End of pipe" conditions

Chronic toxicity

- Long term, sub-lethal effects

- Mixed water conditions

- More sensitive test





45

Effluent Discharge, Reclamation, and Reuse Vocabulary

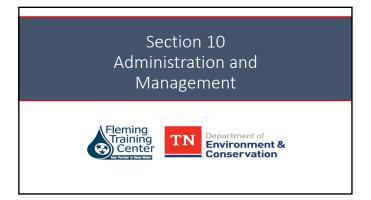
1.	The term is used to describe any rivers, streams, lakes,
	estuaries, or oceans into which wastewater effluent is discharged. Direct discharge into these waters is the most common reuse method.
2.	Chemicals are added to a sample in the field to prevent the water quality indicators of interest from changing before the analysis can be conducted in the laboratory; this is known as a
3.	A sample is a single sample of water collected at a particular time and place that represents the composition of the water only at that time and place.
4.	A collection of individual samples obtained at regular intervals – usually every one or two hours during a 24 hour period- which are combined to form a representative sample is known as a sample.
5.	The process in which an organism takes in oxygen for its life processes and gives off carbon dioxide is called
6.	The process by which water vapor is released to the atmosphere from living plants; includes the total water removed by plants and by evaporation from soil, snow, and water surfaces.
7.	The most common form of land treatment for effluent disposal is, which includes ridge and furrow, sprinklers, surface/drip systems, and border strip flooding.
8.	A type irrigation method, is a series of interconnected ditches (furrows) which allow for the distribution, infiltration, and treatment of wastewater.
9.	Another form of irrigation, are broken into 3 categories: solid set (fixed), portable, or continuously moving.
10.	This form of irrigation is used on highly impermeable soils; where wastewater is applied intermittently at top of terrace, slowly runs down the slope, and runoff is collected at the bottom for further treatment:
11.	One way to gauge the impact that effluent discharge is having on the receiving waters is to measure DO at several different cross sections downstream from the discharge to determine the lowest level; this is called a

12. The point, location, or structure where wastewate	
conduit is called thenumbered in your NPDES permit.	These locations will be identified and
numbered in your NPDES permit.	
Word Bank	
Composite	
Irrigation	
Surface waters	
Ridge and furrow	
Dissolved Oxygen profile (aka Oxygen profile)	
Overland flow	
Evapotranspiration	
Respiration	
Spray systems	
Grab	
Fixed sample	
Outfall	

Section 10 Administration and Management







Public or private, large or small, it's a complex and challenging job

Protection from environmental disasters with a minimum investment of money

External concerns (public citizens) vs. challenges within the utility

Ethical and responsible decisions

Personnel

Resources

Equipment

Preparing for the future

Preparing for the future

1 2

Functions of a manager Planning Organizing Staffing Directing Controlling In small communities, the utility manager may be the only one who has all these responsibilities

Planning

One of the most important functions
Building the resources and financial capability to provide for future needs
Future growth
Industrial development
Plant capacity
Level of treatment

Short term and long term goals
Should include input from: operational personnel, local officials, and the public

3 4

Planning (O & M) Operational Standpoint To maintain design functionality (capacity) Does the system perform as designed? Proactive or reactive? Corrective Maintenance Preventative Maintenance Predictive Maintenance Proactive can be scheduled and long-term Capital Improvement Programs (CIP) planned/budgeted

Planning (O&M)

• Corrective Maintenance (Reactive)

- Emergency

- Reliance on reactive maintenance will always result in poor system performance

• 2 types of emergencies:

1. Normal

• Sewer blockages

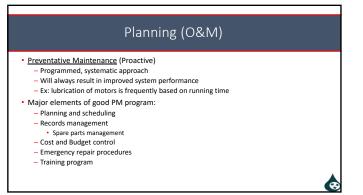
• Can be reduced by effective maintenance program

2. Extraordinary

• High-intensity rainstorm, floods, earthquakes

• Can be minimized by planned maintenance program and development of comprehensive emergency response plan

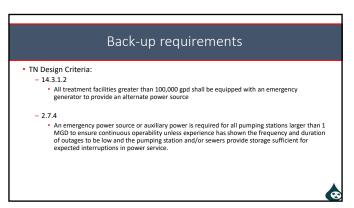
5



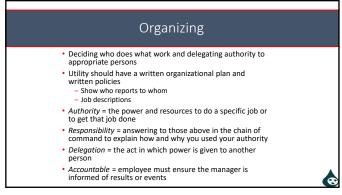


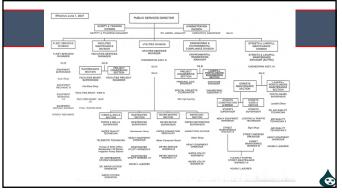
7 8





9 10





Organizing

- Employees should not be asked to accept responsibilities beyond their level of
- Authority and responsibility must be delegated properly to be effective
- 3 components present = successful delegation
 - Proper job assignments
 - Authority
 - Responsibility
- · Follow-up is important

13 14

Staffing · Should have established procedures for: Analyzing staffing needs Qualifications profile, Advertising, Interviewing Training New employee and ongoing Safety is extremely important, but not sole benefit - Protection of public's investment - Employee pride and recognition Certification Supervisor training Evaluating job performance Written evaluation strongly recommended for documentation Set goals

Staffing

- 68-221-909. Certification of operators Responsibilities Multiple functions.
- (a) All operators of water and wastewater systems are encouraged to become certified, although this part requires only that a person in direct charge of a water treatment plant, wastewater treatment plant, water distribution system or wastewater collection system be certified.
- (c) It is permissible for one (1) certified operator to have the responsibility for more than one (1) water and/or wastewater system where two (2) or more systems are involved in reasonable proximity to one another, and where the duties of operation are such that the work time of one (1) person may properly be divided among two (2) or more systems, or where a certified operator may adequately supervise the work of others in more than one (1) system.

[Acts 1984, ch. 812, § 8; T.C.A., § 68-13-909.]

Communication

- Both written and oral communication skills are needed to effectively organize and direct the operation of wastewater plant $\,$
- 2 part process:
 - Info must be given
 - Info must be understood (good listening skills)
- Communicating with employees, your governing body, and the public
- Annual report

16

- One of the most involved writing projects
- Review of what and how the utility operated the past year
- Include goals for next year

15

Communication

- Public Relations
 - Utility Operations
 - Public image
 Open communication
 - Mass Media
 - Being Interviewed Public Speaking
 - Consumer Inquiries Customer calls are frequently your first indication that something may be wrong Education can be a valuable tool

 - Franklin videos: <u>flushable wipes</u>, <u>grease</u>
 - Metro v
 - Plant Tours

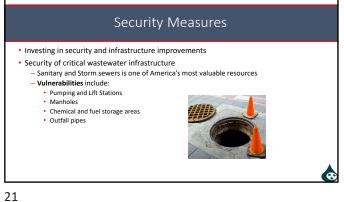




Safety Regardless of size, utility must have a safety program

- Basic elements include: safety policy statement, safety training and promotion, accident investigation and reporting Regulatory agencies OSHA (TOSHA) First Aid Hazard Communication/Right To Know Laws 29 CFR 1910.1200 - SDS · Confined Space Entry Procedures Reporting Training

20 19

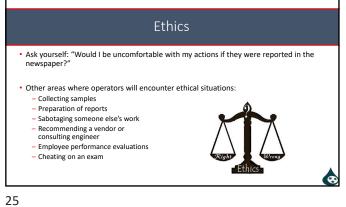


Vulnerability Analysis Worksheet ent System Capital City Wastewater Treatment Plant Assumed Emergency Flood (100 years) Description of Emergency The flood will cause considerable damage to low lying areas. Bridges will be closed, utility poles downed and electrical power interrupted. Effects of emergency Maintain pipe and fitting to repair damaged section. Provide portable pumps to bypass break. Contract for major emerge repair services FIGURE 3.12 Example of a vulnerability analysis

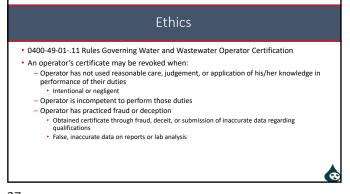


Ethics Examples of illegal and unethical activities: · Providing false information on an application for a job or certification exam Cheating on your certification exam Copying certification exam questions - Dry-labbing (writing down results without actually performing the test) Falsifying results and reports Intentionally discharging toxic wastes to receiving waters Harassing other employees Requiring operators to use unsafe equipment, work under unsafe conditions, or occupy confined space with an unsafe atmosphere

23 24



Ethics Whistleblowing = the act of reporting illegal activity to an authority Codes of Ethics · Interactions between operators - Trustworthiness and the public
Interactions among operators
Approved professional conduct Respect - Responsibility Caring Service by operators to protect the public and the environment - Justice - Civic virtue and citizenship





27

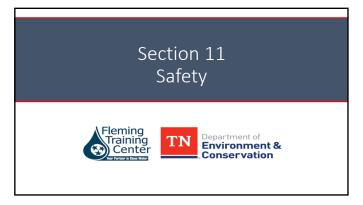
Administration and Management Vocabulary

1.	is the power and resources to	o do a specific job or to get that job done.
2.	The act of is defined as	deciding who does what work and delegating authority
	to the appropriate persons.	
3.	Answering to those above in the chain of command	to explain how and why you have used your authority is
	defined as	
4.	. A is a brief (10	0-20 minutes) safety meeting held every 7 – 10 working
	days.	
5.	. Moral principles and rules of conduct define the cor	ncept of An operator's
	certification may be revoked if they do not act with	this concept in mind.
6.	. When a manager gives power/responsibility to an e	mployee, and the employee ensures that the manager is
	informed of results or events, that employee is dem	nonstrating
7.	is the act in which pow	wer is given to another person in the organization to
	accomplish a specific job.	
8.	maintenance is proactiv	e and is defined as a programmed, systematic approach
	to maintenance activities.	
9.	. The nation's provide	s the essential services that underpin American society
	and serve as the backbone of our nation's economy	, security, and health. This includes the Water and
	Wastewater Systems Sector, which includes water of	distribution and sewage collection systems.
10.	Identifying system components, estimating disaster	effects on those components, estimating customer
	demand for service following a disaster, and identif	ying key system components that would be primarily
	responsible for a system failure are all key steps tha	t should be taken when conducting a
	analysis.	
11.	 The act of reporting illegal activity to an authority is 	called
12.		d of establishing baseline performance data, monitoring
	performance criteria over a period of time, and obs	erving changes in performance so that failure can be
	predicted and maintenance can be performed on a	planned, scheduled basis.
<u>Wo</u>	<u>/ord Bank</u> :	
		- 11
Acc	ccountability	Ethics
Org	rganizing	Accountability
016	18011121118	Accountability
Pre	reventative	Responsibility
		- W
Wh	/histleblowing	Tailgate Safety Meeting
Crit	ritical Infrastructure	Authority
		,
Pre	redictive	Vulnerability

Section 11 Safety







Safety

- An accident is caused by either an unsafe act or an unsafe environment.
- Personal cleanliness is the best means of protection against infection

1

General Duty Clause

- FEDERAL 29 CFR 1903.1
- Worker Right to Know:
 - EMPLOYERS MUST: Furnish a place of employment free of recognized hazards that are causing or are likely to cause death or serious physical harm to employees. Employers must comply with occupational safety and health standards promulgated under the Williams-Steiger Occupational Safety and Health Act of 1970.

Before Leaving Work

- Make sure to:

 - Check work assignments
 Ensure you have all equipment necessary - Inspect all Equipment
- Vehicle inspection

 When backing up a truck, one person should always be at the rear of the truck in view of the driver
- Mirrors and windows - Lights and horn

- TiresTrailer hitch/safety chain

3

4

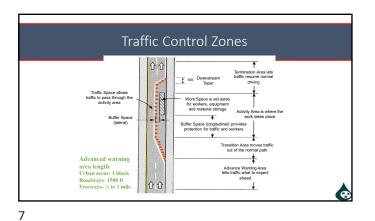
6

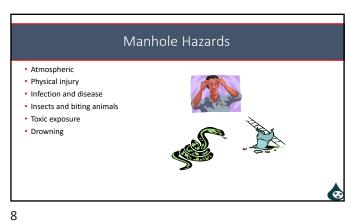
2



Traffic Control Zones Advanced warning area · Transition area • Buffer space · Work area Termination area

5





Confined Space

Fleming Training Center Conservation

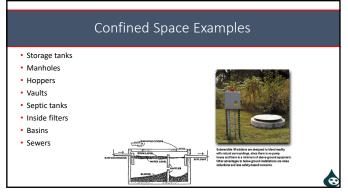
Confined Space Conditions

- Large enough and so configured that an employee can enter and perform assigned work

- Limited or restricted means of entry or exit

- Not designed for continuous employee occupancy

9 10





11 12

282



Permit Required Confined Space

14

Atmospheric Hazards Need to have atmosphere monitored!!! 1. Depletion or elimination of breathable oxygen Oxygen deficient atmosphere Minimum oxygen level is 19.5% 2. Combustible gas or vapor These can develop in the collection system or sewer plant duel to legal, illegal or accidental sources 3. Toxic or suffocating gases Comes from natural breakdown of organic matter in wastewater or toxic discharges

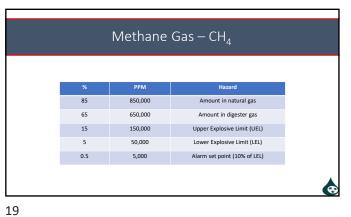
Hydrogen Sulfide – H₂S Detected by the smell of rotten eggs Loss of ability to detect short exposures Olfactory fatigue Not noticeable at high concentrations · Poisonous, colorless, flammable, explosive and corrosive Exposures to .07% to 0.1% will cause acute poisoning and paralyze the respiratory center of the body At the above levels, death and/or rapid loss of consciousness occur • S.G. = 1.19 Alarm set point = 10 ppm (0.001%)

15 16

Hydrogen Sulfide – H ₂ S			
%	PPM	Hazard	
46	460,000	Upper Explosive Limit (UEL)	
4.3	43,000	Lower Explosive (LEL)	
0.1	1,000	DEAD	
0.07	700	Rapid loss of consciousness	
0.01	100	IDLH	
0.005	50	Eye tissue damage	
0.002	20	Eye, nose irritant	
0.001	10	Alarm set point	

Methane Gas – CH₄ · Product of anaerobic waste decomposition · Leaks in natural gas pipelines - Odorless unless natural gas supplied through pipeline, has mercaptans added, but soil can strip the odor • Explosive at a concentration of 5% or 50,000 ppm Spaces may contain concentrations above the Lower Explosive Limits (LEL) and still have oxygen above the 19.5% allowable · Colorless, odorless, tasteless · Does not decrease oxygen content · Acts as an asphyxiant Coal miners used canaries as early alarms; if bird died, it was time to get out • S.G.= 0.55 Alarm set point is 10% LEL = 5000 ppm

17 18



Carbon Monoxide - CO Decreases amount oxygen present Hazardous because it readily binds with hemoglobin in blood, starving the person's body of oxygen ALWAYS VENTILATE • 0.15% (1500 ppm) DEAD • Will cause headaches at .02% in two hour period • Maximum amount that can be tolerated is 0.04% in 60 minute period • Colorless, odorless, tasteless, flammable and poisonous Manufactured fuel gas • S. G. = 0.97 • Alarm set point at 35 ppm

Carbon Monoxide - CO			
%	PPM	Hazard	
74	740,000	Upper Explosive Limit (UEL)	
12.5	125,000	Lower Explosive (LEL)	
0.2	2,000	Unconscious in 30 minutes	
0.15	1,500	IDLH	
0.05	500	Sever headache	
0.02	200	Headache after 2-3 hours	
0.0035	35	8-hour exposure limit	
0.0035	35	Alarm set point	

Oxygen – O₂ • ALWAYS ventilate – normal air contains ~ 21% • Oxygen deficient atmosphere if less than 19.5% Oxygen enriched at greater than 23.5% Speeds combustion Could be from pure oxygen being used to oxidize hydrogen sulfide Leave area if oxygen concentrations approach 22% • Early warning signs that an operator is not getting enough oxygen: - Shortness of breath Chest heaving - Change from usual responses

22 21

	Oxyge	n – O ₂
%	PPM	Hazard
23.5	235,000	Accelerates combustion
20.9	209,000	Oxygen content of normal air
19.5	195,000	Minimum permissible level
8	8,000	DEAD in 6 minutes
6	6,000	Coma in 40 seconds, then DEAD

Oxygen – O₂ • When O₂ levels drop below 16%, a person experiences Rapid fatigue - Inability to think clearly Poor coordination Difficulty breathing - Ringing in the ears - Also, a false sense of well-being may develop

23 24

284

Oxygen – O₂

- In a confined space, the amount of oxygen in the atmosphere may be reduced by several factors
 - Oxygen consumption
 - During combustion of flammable substances
 - Welding, heating, cutting or even rust formation
 - Oxygen displacement
 - Carbon dioxide can displace oxygen
 - Bacterial action



25 26

Atmospheric Alarm Units

- · Alarms set to read:
 - Flammable gasses exceeding 10% of the LEL
 - H₂S exceeds 10 ppm and/or
 - O₂ percentage drops below 19.5%
 - CO alarm set point is 35 ppm
- · Calibrate unit before using
- Most desirable units: simultaneously sample, analyze and alarm all three atmospheric conditions

Atmospheric Alarm Units

- Some physical and environmental conditions that could affect the accuracy of gas detection instruments include:
 - Caustic gasesTemperature
 - TemperatureDirty air
 - Humidity
 - Air velocity
 - Vibration

27 28

Safety Procedures if Explosive Atmosphere Discovered

- Immediately notify supervisor
- Do not remove manhole cover
- Turn off running engines in area
- Route vehicles around area
- Inspect up and downstream of manhole
- Route traffic off the street
- Notify waste and or pretreatment facility
- Cautiously ventilate
- NO SMOKING IN AREA



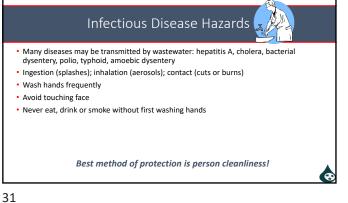
Ventilation

• Blowers need to be placed upwind of manhole and at least 10 feet from opening

• Gas driven engine – exhaust must be downwind of manhole

• Air intake should be 2-5 feet above ground service

29 30





LOTO General Requirements

- · Every facility should have a written program
- · Utilize tagout system if energy isolating device not capable of being locked out
- Lockout/tagout hardware provided

33

- Devices used only for intended purposes
- Tagout shall warn DO NOT START, DO NOT ENERGIZE, DO NOT OPERATE
- · Only trained employees shall perform lockout/tagout

Requirements for Lockout of Equipment Before beginning work on any pump, the first thing to be done is to lock it out. The person doing the work should have the key Notify employees · Employees notified after completion of work and equipment re-energized CAUTION

Recommend Steps for Lockout/Tagout

- Notify employees that device locked and tagged out
 - Turn off machine normally
 - De-activate energy
 - Use appropriate lockout/tagout equipment
 - Release any stored energy
 - Try to start machine by normal means

Steps for Restoring Equipment

34

- Check area for equipment or tools
- Notify all employees in the area
- · Verify controls are in neutral
- · Remove lockout/tagout devices and re-energize
- Notify employees maintenance and/or repairs are complete and equipment is operationally

35 36

Training Requirements · Employer shall train all employees · All new employees trained Recognition of applicable hazardous energy • Purpose of program Procedures Consequences ANNUAL REQUIREMENT 37

Inspections

- Conduct periodic inspection at least annually
- Shall include review between the inspector and each authorized employee
- Recommendation: Frequent walk through of work areas and observation of Maintenance and Operation area

Required Record Keeping

- Written Lockout/Tagout Program
- Training: Annual and New Employees
- Inspections: Annual including new equipment, inspection of devices, and procedures

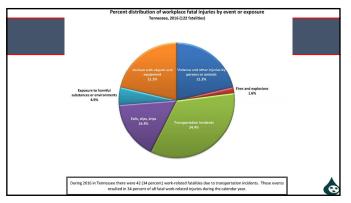
Most Cited Industry Standards By TOSHA

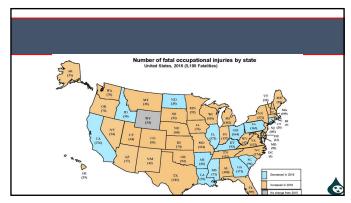
- No written Hazard Communication Program
- · Inadequate Hazard Communication Training
- PPE Hazard Assessment not Done
- No Energy Control Program Lockout/Tagout
- No MSDS on Site

38

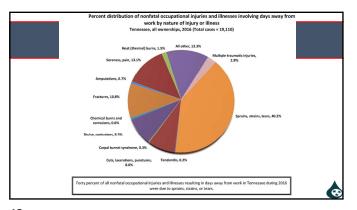
- No one Trained in First Aid
- No Emergency Action Plan
- Metal Parts of Cord and Plug Equipment Not Grounded
- Unlabeled Containers of Hazardous Chemicals

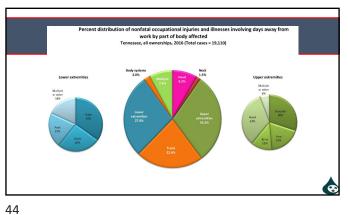
39 40



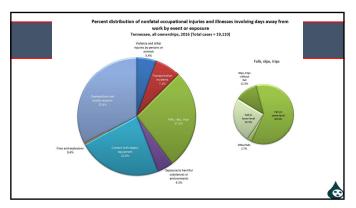


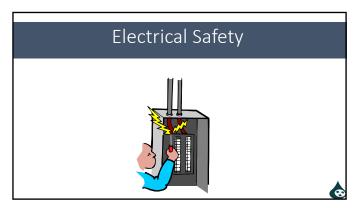
42 41





43





45 46

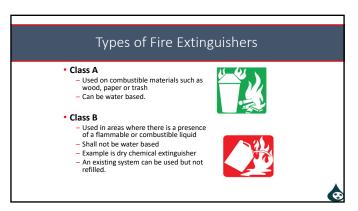
OSHA Says Any electrical installations shall be done by a professionally trained electrician. Any employee who is in a work area where there is a danger of electric shock shall be trained. Employees working on electrical machinery shall be trained in lockout/tagout procedures



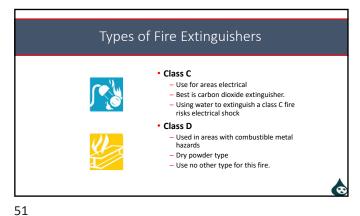
47 48

288

Fire Protection Equipment • Fire extinguishers shall be located where they are readily accessible. · Shall be fully charged and operable at all times. - Charged after each use. • All fire fighting equipment is to be inspected at least annually. Portable fire extinguishers inspected at least monthly and records kept. · Hydrostatic testing on each extinguisher every five years. · Fire detection systems tested monthly if batter operated.



49 50



Types of Fire Extinguishers Class Material Method Α Wood, paper Water Carbon dioxide, foam, dry chemical or Halon В Flammable liquids (oil, grease, paint) Carbon dioxide, dry С Live electricity chemical, Halon D Metals Carbon dioxide

52

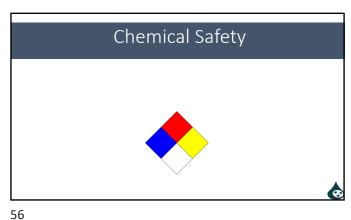
Types of Fire Extinguishers		
	Common materials such as paper, wood or most other combustibles	
Combination ABC are most common	Flammable liquids such as gasoline, paint remover or grease	
Have the types of extinguishers available depending upon analyses performed in	Electrical fires Combustible metals usually	
each area	found in industry	

Fire Extinguishers To operate a fire extinguisher, remember the word PASS Pull the pin. Hold the extinguisher with the nozzle pointing away from you −**A**im low. Point the extinguisher at the base of the fire. —Squeeze the lever slowly and evenly. **-S**weep the nozzle from side-to-side.

53 54

> Safety 289





Personal Protective Equipment

• Gloves
• Coveralls / Overalls
• Face Shield / Goggles
• Respirator / SCBA
• Boots
• Ear Plugs / Muffs

Safety Data Sheets Previously called MSDS RIGHT-TO-KNOW Information • Lists: - Common and chemical name - Manufacturer info - Hazardous ingredients MATERIAL Health hazard data SAFETY - Physical data DATA Fire and explosive data SHEETS - Spill or leak procedures - Special precautions

Note

What is the difference between a MSDS and the new SDS?

SDSs are in use globally

The Safety Data Sheets (formerly MSDSs) will now have a specified 16-section format

Minimum Info for SDS Product identification Physical/chemical properties Stability & reactivity · Hazard Identification • Composition/info on ingredients • Toxicological information · First-aid measures Ecological information* Disposal considerations* Fire-fighting measures · Accidental release measures Transport information* · Handling and storage Regulatory information* Other information (including date of SDS or last revision)* Exposure controls * Non mandatory

59 60

290

57

Safety

58

MSDS to SDS In addition, chemical manufacturers and importers will be required to provide a label that includes a harmonized signal word, pictogram, and hazard statement for each hazard class and category The use of pictograms will enable workers, employers, and chemical users worldwide to understand the most basic chemical information without language barriers

OSHA Pictograms and Hazards

Health Hazard

Flame

- Carcingoge

- Carcingoge

- Representative Foreign

- Application Foreign

- Special Fo

61 62

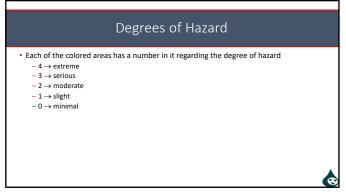
PERSONAL PROTECTION

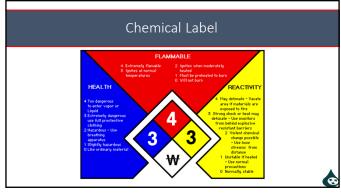
* "Right to Know"

- In 1983, OSHA instituted Hazard
Communication Standard 1910-1200,
a rule that gives employees the right
to know the hazards of chemicals to
which they may be exposed in the
workplace.

64

63





65 66

Safety 291

Terms

- Lower Explosive Level (LEL) minimum concentration of flammable gas or vapor in air that supports combustion
- Upper Explosive Limit (UEL) maximum concentration of flammable gas or vapor in air that will support combustion
- Teratogen causes structural abnormality following fetal exposure during pregnancy
- Mutagen capable of altering a cell's genetic makeup



67

Trenching Basics

- Provide stairways, ladders, ramps or other safe means of access in all trenches 4 feet or deeper
 - These devices must be located within 25 feet of all workers
 - Ladders used in trenches shall protrude at least 3 feet above the trench edge
- Minimum diameter of rungs on a fixed steel ladder is %-inch
- Minimum clear length of rungs on a fixed steel ladder is 16

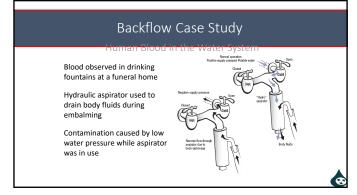
Trenching Basics • Trenches 5 feet deep or greater require a protective system, which can be shielding, shoring or sloping – A registered engineer must approve all shielding and shoring • Trenches 20 feet deep or greater require that the protective system be designed by a registered professional engineer • Keep excavated soil (spoils) and other materials at least 2 feet from trench edges. • The support or shield system must extend at least 18 inches above the top of the vertical side.

69 70

Cross-Connection Control

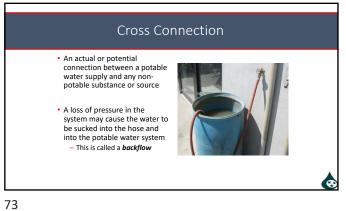


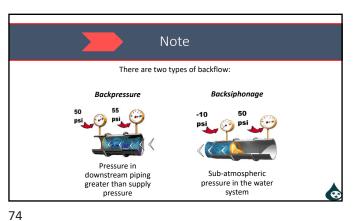


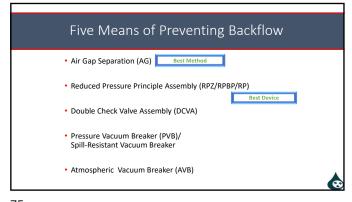


71 72

²⁹² Safety

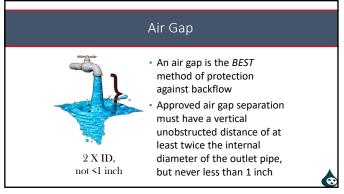






Air Gap · An air gap is the vertical separation between the water supply line outlet and the overflow rim of the non-pressurized receiving fixture or tank

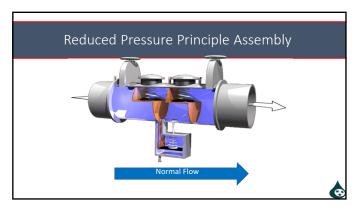
75 76



Air Gap Separation Limitations The air gap is the best method of backflow prevention, but it is easily defeated through modifications or being bypassed • The air gap separation causes a loss of pressure in the system · Sanitary control is lost - cannot be installed in an environment containing airborne contamination

78 77

> Safety 293



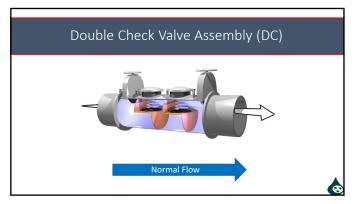
Reduced Pressure Principle Assembly

- The reduced pressure principle backflow prevention assembly (RP) consists of two independently operating check valves together with a hydraulically operating, mechanically independent, pressure differential relief valve located between the check valves, all located between two resilient seated shutoff valves and four properly located test cocks.
- BEST device to protect against backflow



79

80



Double Check Valve Assembly (DC)

- · The double check valve backflow prevention assembly (DC) consists of two independently operating check valves installed between two tightly closing resilient seated shutoff valves and fitted with four properly located test cocks
- · Similar to the RP, but has no relief port so it cannot maintain a lower pressure in the zone between the checks and nowhere for the water to go during a backflow incident or failure

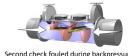


81

82

Double Check Valve Assembly (DC)

- Since the water in a DC cannot leave the system during a backflow event or assembly failure then it is a higher risk and therefore cannot be used in a high hazard (contaminant) application
- · If one check fails the other will continue to protect, but given enough time the second check will fail and backflow will occur



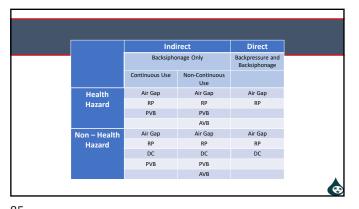
Second check fouled during backpressure

Other Devices Pressure Vacuum Breaker Incoming water pressure will compress the spring on the check and flow into the body As pressure builds up in the body it will compress the spring on the air valve and close it allowing water to travel downstream Atmospheric Vacuum Breaker Designed to prevent backsiphonage. It consists of a body, a single moving float that acts as a check valve when there is no flow and as a airinlet valve when flow is present, and an air-inlet opening covered by a cap

83

294

84





85 86





87 88

Safety 295

Safety Vocabulary

1.	A is defined by OSHA as a person capable of identifying existing and		
	predictable hazards in the surroundings, or working conditions that are unsanitary, hazardous, or danger to employees, and who has authorization to take prompt corrective measures to eliminate the hazards.		
2.	The is the unit for expressing the relative intensity of sounds on a scale of zero to the		
	average least perceptible sound to about 130 for the average level at which sound causes pain to humans. It is abbreviated dB.		
3.	The is the lowest concentration of a gas or vapor that explodes if an		
	ignition source is present at ambient temperature.		
4.	is the condition in which a person's nose, after exposure to certain odors, is		
	o longer able to detect the odor.		
5.	The condition in which an atmosphere contains oxygen at a concentration of more than 23.5 percent by volume is called		
6.	An health effect is an adverse effect on a human or animal body, with symptoms		
	developing rapidly. In contrast, a health effect is one that develops slowly over a		
	long period of time or one that recurs frequently.		
7.	The atmospheric concentration of any toxic, corrosive, or asphyxiant substance that poses an immediate		
	threat to life or would cause irreversible or delayed adverse health effects or would interfere with an		
	individual's ability to escape from a dangerous atmosphere is classified as		
8 occurs when the atmosphere contains oxygen at a contains oxyge			
	of less than 19.5 percent by volume.		
9.	Gas present in the collection system is called even if it is from such sources as gas		
	mains, gasoline, and cleaning fluid. It usually results from the decomposition of organic matter in the wastewater.		
10.	. The excavated material, such as soil, from the trench of a water main or sewer.		
11.	A is defined as a space that:		
	 Is large enough and so configured that an employee can bodily enter and perform assigned work; and 		
	Has limited or restricted means of entry or exit; and		
	Is not designed for continuous employee occupancy		
12	Any substance that tends to produce cancer in an organism is called a		
	A tool that is made of a nonferrous material, usually a copper-beryllium alloy is a		
13.	77 tool that is made of a nomerrous material, asking a copper seryman alloy is a		
14.			
	finely divided (flowable) solid substance that can be aspirated to cause death by filling or plugging the		
	respiratory system or that can exert enough force on the body to cause death by strangulation, constriction,		
	or crushing.		

- 15. This type of confined space has one or more of the following characteristics:
 - Contains or has a potential to contain a hazardous atmosphere
 - Contains a material that has the potential for engulfing an entrant
 - Has an internal configuration such that an entrant could be trapped or asphyxiated by inwardly converging walls or by a floor that slopes downward and tapers to a smaller cross section

 Contains any other recognized serious safety or health hazard 		
16. This type of confined space does not contain or, with respect to atmospheric hazards, have the potentia		
contain any hazard capable of causing death or seri		
	is the wastewater has produced hydrogen sulfide	
turned black, is giving off foul odors, and contains little or no dissolved oxygen. are sulfur-containing compounds that have an offensive skunk-like odor; but can sometimes be described as smelling like garlic or onions.		
		Sometimes be described as smelling like garne or or
Word Bank		
Competent person	Carcinogen	
Permit-required	Mercaptans	
IDLH (Immediately Dangerous to Life or Health	Oxygen deficiency	
Chronic	Engulfment	
Septic		
Spoil		
Nonsparking tool		
Oxygen enrichment		
Confined space		
Non-permit		
Sewer gas		
Lower explosive limit (LEL)		
Decibel		
Acute		

Olfactory fatigue

Cross Connection Vocabulary Words

<u>Absolute Pressure</u> – The total pressure; gauge pressure plus atmospheric pressure. Absolute pressure is generally measured in pounds per square inch (psi).

<u>Air Gap</u> – A physical separation between the free flowing discharge end of a potable water supply line and an open or non-pressurized receiving vessel. An air gap acts as a physical, unobstructed separation between the water distribution system and the wastewater collections system. An "approved air gap" must be twice the internal diameter of the supply pipe measured vertically above the overflow rim of the receiving vessel, but never less than 1 inch.

The air gap is the most effective method for preventing backflow.

<u>Air Inlet</u> – The opening in the body of a device (usually a vacuum breaker) which will allow free atmosphere into the liquid passageway of the device body, which will prevent downstream siphoning. (backsiphonage) -

<u>Approved Backflow Prevention Assembly</u> – An assembly that has been evaluated/tested and approved according to the authority having jurisdiction for use within the water system.

<u>Aspirator Effect</u> – The hydraulic effect of suction created by an aspirator or restricted area of flow. At this restricted area of flow the pressure drops to sub-atmospheric, creating suction. The effect can be increased with the use of a Venturi apparatus.

<u>Atmospheric Pressure</u> – The pressure exerted by the weight of the atmosphere (14.7 psi at sea level). As the elevation above sea increases, the atmospheric pressure decreases.

<u>Atmospheric Vacuum Breaker (AVB)</u> – A non-testable backflow device consisting of a body, a checking member (float), and an atmospheric opening. An AVB protects against backsiphonage only, not backpressure.

<u>Auxiliary Water Supply</u> – Any water supply on or available to the premises other than water supplied by the public water purveyor. These waters may be polluted or contaminated and constitute an unacceptable water source over which the water purveyor does not have sanitary control.

<u>Backflow</u> – The undesirable reversal of flow of contaminated water, other liquids or gases into the distribution system of a potable water supply.

<u>Backflow Prevention Device (Backflow Preventer)</u> – Any device, method or construction used to prevent the backward flow of liquids into a potable water supply.

<u>Backpressure</u> (Superior Pressure) – The hydraulic condition of increased pressure in a system above the supply pressure which results in backflow into the potable water supply.

<u>Backsiphonage</u> – The hydraulic condition resulting in backflow due to a reduction in system pressure, which causes a sub-atmospheric pressure (vacuum) to exist in the water system.

<u>Bypass</u> – Any arrangement of pipes, plumbing or hoses designed to divert the flow around an installed backflow device or assembly through which the flow normally passes.

Check Valve – A mechanical device designed to allow flow in one direction only.

<u>Containment</u> – A water purveyor's backflow prevention policy of installing a backflow prevention device commensurate with the degree of hazard after the termination of the distribution system (water meter) and prior to any branches in the system.

<u>Contaminant</u> – Any substance introduced into the public water system that will cause illness or death. (high hazard)

<u>Continuous Pressure</u> – A condition in which upstream pressure is applied for more than 12 hours in a 24-hour period to a device or assembly. Continuous pressure can cause mechanical parts within a device to freeze.

<u>Cross Connection</u> – Any physical arrangement whereby a public water system is connected, directly or indirectly, with any other water supply system, sewer, drain, conduit, pool, storage reservoir, plumbing fixture or other device which contains or may contain contaminated water, sewage, or other waste or liquid of unknown or unsafe quality which may be capable of contaminating the public water supply as a result of backflow.

<u>Cross Connection Control</u> – The use of assemblies, methods and procedures to prevent contamination of a potable water supply through cross connections.

<u>Degree of Hazard</u> – The danger posed by a particular substance or set of circumstances. Generally, a low degree of hazard (pollutant) is one that does not affect health, but may be aesthetically objectionable. A high degree of hazard (contaminant) is one that could cause serious illness or death.

<u>Differential Pressure</u> – The relative difference in pressure between two pressure sources.

<u>Direct Cross-Connection</u> – A continuous, enclosed interconnection to allow the flow of fluid from ones system to the other. A direct cross connection is subject to both backsiphonage and backpressure.

<u>Distribution System</u> – A system of conduits (pipes, laterals, fixtures) by which a potable water supply is distributed to consumers.

<u>Double Check Detector Assembly</u> – A specially designed assembly composed of line size approved double check valve assembly, with a bypass containing a water meter and approved double check valve assembly specifically designed for such application. The meter shall register accurately for very low rates of flow up to 2 gallons per minute and shall show a registration for all rates of flow. This assembly shall only be used to protect against non-health hazards and is designed primarily for uses on fire sprinkler systems.

<u>Double Check Valve Assembly</u> – A backflow prevention assembly consisting of two independently acting internally loaded check valves, four properly located test cocks, and two shutoff valves. Used to protect against non-health hazards (pollutants) only.

<u>Dual Check</u> – An untestable backflow prevention device consisting of two independently operating check valves, without any test cocks or shut-off valves.

<u>Failed</u> – The status of a backflow prevention assembly determined by a performance evaluation based on the failure to meet all minimums set forth by the approved testing procedure.

<u>Feed Water</u> – Water that is added to a commercial or industrial system and subsequently used by the system, such as water that is fed to a boiler to produce steam.

Flood-Level Rim – The top edge of a receptor from which water overflows.

<u>Gauge Pressure</u> – Pounds per square inch (psi) that are registered on a test gauge. Gauge pressure measures only the amount of pressure above (or below) atmospheric pressure.

<u>Indirect Cross-Connection</u> – A potential cross connection where the interconnection is not continuously enclosed and is subject to backsiphonage only.

<u>Isolation</u> – A water purveyor's backflow prevention policy of installing a backflow prevention device commensurate with the degree of hazard at each fixture or appliance outlet.

Liability – Legally responsible for or being obligated by law for the protection of the potable water supply.

<u>Negative Pressure</u> – Pressure that is less than atmospheric; negative pressure in a pipe can induce a partial vacuum that can siphon nonpotable liquids into the potable distribution system.

<u>Nonpotable</u> – Any liquid that is not considered safe for human consumption.

<u>Parallel Installation</u> (Dual Installation) – The installation of two or more backflow prevention assemblies of the same type having a common inlet, outlet, and direction of flow.

<u>Passed</u> – The status of a backflow prevention assembly determined by a performance evaluation in which the assembly meets all minimums set forth by the approved testing procedure.

<u>Pathogen</u> – A disease producing organism, such as a virus, bacterium, or other microorganism. Associated with high hazard (contaminant) conditions.

<u>Performance Evaluation</u> – An evaluation of an approved backflow prevention assembly using the latest approved testing procedures in determining the status of the assembly.

<u>Plumbing</u> – Any arrangement of pipes, fittings, fixtures or other devices for the purpose of moving liquids from one point to another, generally within a single structure.

Poison – A substance that can kill, injure or impair a living organism.

<u>Pollutant</u> – A substance that would constitute a non-health hazard and would be aesthetically objectionable if introduced into the potable water system.

<u>Potable</u> – Water (or other liquids) that are safe for human consumption.

<u>Pressure</u> – The weight (of air, water, etc.) exerted on a surface, generally expressed as pounds per square inch (psi).

<u>Pressure Vacuum Breaker (PVB)</u> – A backflow prevention assembly consisting of one or two independently operating spring loaded check valves and an independently operating spring loaded air inlet valve located on the

discharge side of the check valve(s), with properly located test cocks, and tightly closing shutoff valves on each side of the check valves. A PVB is testable and protects against backsiphonage only, not backpressure.

<u>Reduced Pressure Principle Assembly (RP)</u> – A backflow prevention assembly consisting of two independently operating spring-loaded check valves together with a hydraulically operating, mechanically independent, pressure differential relief valve located between the check valves and below the first check valve. These units shall be located between two tightly closing shutoff valves with four properly located test cocks.

The RP is the best device for preventing backflow.

<u>Reduced Pressure Principle Detector Assembly</u> – A specially designed assembly composed of a line size approved reduced pressure principle backflow prevention assembly with a bypass containing a water meter and an approved reduced pressure principle backflow prevention assembly specifically designed for such application. The meter shall register accurately for very low flow rates of flows up to 2 gallons per minute and shall show registration of all flow rates. This assembly shall only be used to protect against non-health and health hazards and is designed primarily for uses on fire sprinkler systems.

<u>Refusal of Service (Shutoff Policy)</u> – A formal policy adopted by a governing board to enable a utility to refuse or discontinue service where a known hazard exists and corrective measures are not undertaken.

<u>Regulating Agency</u> – Any local, state or federal authority given the power to issue rules or regulations having the force of law for the purpose of providing uniformity in details and procedures.

<u>Relief Valve</u> – A device designed to release air from a pipeline, or introduce air into a line if the internal pressure drops below atmospheric pressure.

<u>Submerged Inlet</u> – The discharge of a piping system that is located below the flood level rim of a tank or vessel. This can result in an indirect cross connection with a potable drinking water supply.

Test Cock – An appurtenance on a device or valve used for testing the device.

<u>Venturi</u> – A specifically designed hydraulic structure designed to increase the velocity and thus decrease the pressure of a fluid through a constricted region creating suction.

<u>Venturi Effect</u> – A hydraulic principle that states that as the flow path is restricted, a fluid will exhibit a greater velocity and a reduced system pressure through the restriction. The Venturi effect can induce a vacuum in a distribution system.

<u>Waterborne Disease</u> – Any disease that is capable of being transmitted through water. Examples include typhoid, cholera, giardiasis.

<u>Water Purveyor</u> – An organization that is engaged in producing and/or distributing potable water for domestic use.

Cross-Connections Examples and Potential Hazards

<u>Connected System</u> <u>Hazard Level</u>

Sewage pumps High
Boilers High
Cooling towers High
Flush valve toilets High

Garden hose (sil cocks)

Auxiliary water supply

Aspirators

High

Dishwashers

Moderate

Car wash Moderate to high Photographic developers Moderate to high

Commercial food processors

Low to moderate
Sinks

High

Chlorinators High
Solar energy systems Low to high

SterilizersHighSprinkler systemsHighWater systemsLow to highSwimming poolsModerate

Plating vats High Laboratory glassware or washing equipment High

Pump primers Moderate to high

Baptismal founts Moderate
Access hole flush High
Agricultural pesticide mixing tanks High

Irrigation systems

Watering troughs

Autopsy tables

Low to high

Moderate

High

Section 13 References & Need to Know





Grade 1 Wastewater Treatment Operator Need-To-Know Criteria (Subject Areas)

The following list of categories suggests topics of information which are important to know in order to be a successful and proficient Grade 1 Wastewater Treatment Operator. The list may not be all inclusive, and knowledge of additional topics may be of benefit to the operator.

Category of Information: Processes

Collection Systems

- Types
- Inflow, Infiltration, Exfiltration
- Sources of wastewater
- Pre-treatment
- · Pump stations

Flow

- Measurement
- Flow equalization

Screening

- Bar screens (hand-cleaned and mechanically cleaned)
- Static screen
- Microscreen
- Rotating screens

Grinding

- Grinders
- Comminutors
- Barminutors

Grit Removal

- Hand-cleaned grit chambers
- Mechanically-cleaned grit chambers
- Aerated grit chambers
- Vortex

Clarification

- Primary (Rectangular; Circular)
- Secondary

Attached Growth/Fixed Film

- Trickling Filters
 - Standard Rate
 - High Rate
 - Roughing
- Rotating Biological Contactor (RBC)
- Activated Biofilter (ABF)

Lagoons

- Aerobic
- Facultative
- Anaerobic
- Aerated
- Discharging

Total Containment

Activated Sludge

- Conventional
- Step Feed
- Contact Stabilization
- Extended aeration
- Tapered aeration
- Oxidation ditch
- Types of aeration
- Sequencing Batch Reactor (SBR)
- Membrane Biological Reactor (MBR)

Solids handling

- Sludge conditioning
- Sludge thickening
- Anaerobic digesters
- Aerobic digesters
- Dewatering
- Drying beds
- Land application
- Composting
- 503 Regulations

Disinfection/ Use of Chlorine

- Chlorination
- Dechlorination
- UV
- Other methods

Advanced Treatment

- Nitrogen removal
- Biological

Effluent Disposal

- Discharge
- Direct Use
- Irrigation
- Underground Disposal
- NPDES Permit

Cross- Connection

- Prevention
- Types of devices

Category of Information: Support Systems

Motors

- Single Phase
- Poly Phase
- Variable Speed

Drives

- Coupled
- Direct (Shaft; Gear)
- Speed Reducer (Fixed; Variable)
- Right Angle

Pumps

- Air Lift
- Centrifugal
- Positive Displacement
 - o Piston Plunger
 - Progressive Cavity
 - Diaphragm
- Screw
- Turbine
- Metering
- Ejector

Blowers and Compressors

- Centrifugal
- Positive Displacement (Rotary; Piston)

Generators - AC & DC

Engines - Gasoline, Diesel, Gas

Joints

- Flanged
- Compression
- Dresser
- Victualic
- Fused
- Threaded

Valves

- Ball
- Check
- Globe
- Gate
- Plug
- Petcock
- Pressure Control
- Vacuum Relief
- Mud
- Butterfly
- Multiport
- Telescoping
- Sluice Gate
- Air Release
- Foot
- Altitude

Fittings

- Coupling
- Union
- Plug/Caps
- Corporation (Ferrell; Cock)
- Curb Stop
- Special

Measuring/ Control

- Signal Generators
 - o Kennison Nozzle
 - Magnetic Flowmeter
 - Parshall Flume
 - Proportional Weir
 - Rectangular Weir
 - o Venturi
 - Propeller Meter
 - o Ultrasonic
 - o Pitot Tube
- Signal Transmitters
 - o Electric
 - o Pneumatic
 - Hydraulic
 - o Mechanical
 - Telemetry
- Signal Receivers
 - o Counters
 - o Indicators
 - Log Scale Indicators
 - Totalizers
 - o Recorders
 - Combination Recorders

Meters

- o Hydraulic Rotameter
- Electrical Amp
- o Electrical Watt
- Electrical Watt Hour
- Electrical Multi.
- o Electrical VOM
- o Electrical Megger
- Mechanical RPM
- Alarms
- Controls
 - o Pneumatic
 - o Float
 - o Hydraulic
 - o Electrical
 - Telemetry
 - o Timers

Chemical Feeders

- Solids
- Liquids
- Evaporators
- Gas
- Slurry

Category of Information: Support Systems (continued)

Odor Control

- Biofilters
- Chemical Additives
- Scrubbers

Rolling Stock

- Service Vehicles
- Trucks
- Lawn Mowers
- Loaders
- Portable Pumps
- Generators

HVAC

Fans

Safety Equipment

- Personal Protection Gear
- Traffic Control (Warning Devices; Barricades)
- Hazard Detectors
- First Aid/Hygiene

Phosphorus

0

0

0

0

Settleable

Total

Volatile

Suspended

Total dissolved

Solids

Category of Information: Lab Tests

Routine Tests

- B.O.D.
- Ammonia
- Chlorine Residual
- Coliform (Fecal)
- Dissolved oxygen
- E. coli
- Total Kjedahl nitrogen
- pH

Control Tests

- Centrifuge
- Alkalinity
- C.O.D.
- Nutrients
- Micro exam
- Nitrate nitrite
- Oil and Grease

- Surfactants
- Temperature
- Total organic carbon
- Turbidity
- Volatile acids
- Settleability

Special Tests:

- Metals
- Chlorinated organics
- Cyanide

- Phenol
- Sulfate sulfide
- Biomonitoring

Category of Information: General Information

Units of expression

- Define units
- Convert units

Sources and characteristics

- Characterize
- Quality/quantity
- Physical/chemical/biological
- Effects
- Pre-aeration
- Chemical pre-treatment
- Grease control

Electrical (Basic)

Hydraulics (Basic)

Maps/plans - Interpretation and use

WWT Processes

- Sketch sequence
- Describe processes
- Explain why treated
- Goals of WWT (protect public; protect environment)

Grade 2 Wastewater Treatment Operator Need-To-Know Criteria (Subject Areas)

The following list of categories suggests topics of information which are important to know in order to be a successful and proficient Grade 2 Wastewater Treatment Operator. The list may not be all inclusive, and knowledge of additional topics may be of benefit to the operator.

Category of Information: Processes

Collection Systems

- Types
- Inflow, Infiltration, Exfiltration
- Sources of wastewater
- Pre-treatment
- Pump stations

Flow

- Measurement
- Flow equalization

Screening

- Bar screens (hand-cleaned)
- Bar screens (mechanically cleaned)
- Microscreen

Grinding

- Grinders
- Comminutors
- Barminutors

Grit Removal

- Hand-cleaned grit chambers
- · Mechanically-cleaned grit chambers
- Aerated grit chambers
- Vortex

Clarification

- Primary (Rectangular; Circular)
- Secondary
- SBR Clarification

Attached Growth/Fixed Film

- Trickling Filters
 - o Standard Rate
 - High Rate
 - Roughing
- Rotating Biological Contactor (RBC)
- Activated Biofilter (ABF)

Lagoons

- Aerobic
- Facultative
- Anaerobic
- Aerated
- Discharging
- Total Containment

Activated Sludge

- Conventional
- Step Feed
- Contact Stabilization
- Extended aeration
- Tapered aeration
- Complete mix
- Pure oxygen
- Oxidation ditch
- Types of aeration
- Sequencing Batch Reactor (SBR)
- Membrane Biological Reactor (MBR)

Solids handling

- Sludge conditioning
- Sludge thickening
- Anaerobic digesters
- Aerobic digesters
- Dewatering
- Incineration
- Drying beds
- Land application
- Composting
- 503 Regulations

Disinfection/ Use of Chlorine

- Chlorination
- Dechlorination
- UV
- Other methods

Advanced Treatment

- Filtration
- Nitrogen removal
- · Phosphorus removal
- Biological

Effluent Disposal

- Discharge
- Direct Use
- Irrigation
- Underground Disposal
- NPDES Permit

Cross- Connection

- Prevention
- Types of devices

Category of Information: Support Systems

Motors

- Single Phase
- Poly Phase
- Variable Speed

Drives

- Coupled
- Direct (Shaft; Gear)
- Speed Reducer (Fixed; Variable)
- Right Angle

Pumps

- Air Lift
- Centrifugal
- Positive Displacement
 - Piston Plunger
 - o Progressive Cavity
 - o Diaphragm
- Screw
- Turbine
- Metering
- Ejector

Blowers and Compressors

- Centrifugal
- Positive Displacement (Rotary; Piston)

Generators - AC & DC

Engines - Gasoline, Diesel & Gas

Joints

- Flanged
- Compression
- Dresser
- Victualic
- Fused
- Threaded

Valves

- Ball
- Check
- Globe
- Gate
- Plug
- Petcock
- Pressure Control
- Vacuum Relief
- Mud
- Butterfly
- Multiport
- Telescoping
- Sluice Gate
- Air Release
- Foot
- Altitude

Fittings

- Coupling
- Union
- Plug/Caps
- Corporation (Ferrell; Cock)
- Curb Stop
- Special

Measuring/ Control

- Signal Generators
 - o Kennison Nozzle
 - Magnetic Flowmeter
 - o Parshall Flume
 - Proportional Weir
 - Rectangular Weir
 - o Venturi
 - Propeller Meter
 - Ultrasonic
 - o Pitot Tube
 - Signal Transmitters
 - Electric
 - o Pneumatic
 - o **Hydraulic**
 - Mechanical
 - o **Telemetry**
- Signal Receivers
 - Counters
 - Indicators
 - Log Scale Indicators
 - o Totalizers
 - Recorders
 - o Combination Recorders
- Meters
 - o Hydraulic Rotameter
 - o Electrical Amp
 - Electrical Watt
 - Electrical Watt Hour
 - Electrical Multi.
 - Electrical VOM
 - o Electrical Megger
 - Mechanical RPM
- Alarms
- Controls
 - o Pneumatic
 - o Float
 - o Hydraulic
 - o Electrical
 - o Telemetry
 - Timers

Category of Information: Support Systems (continued)

HVAC

Chemical Feeders

- Solids
- Liquids
- **Evaporators**
- Gas
- Slurry

Odor Control

- **Biofilters**
- Chemical Additives
- Scrubbers

Rolling Stock

- Service Vehicles
- Trucks
- Lawn Mowers
- Loaders
- Portable Pumps
- Generators

Category of Information: Lab Tests

Routine Tests

- B.O.D.
- Ammonia
- Chlorine Residual
- Coliform (Fecal)
- Dissolved oxygen
- E. coli
- Total Kjedahl nitrogen
- pН

Control Tests

- Centrifuge
- Alkalinity
- C.O.D.
- Color
- Conductance
- **Nutrients**
- Micro exam
- Nitrate nitrite

Special Tests:

- Metals
- Chlorinated organics
- Cyanide

Phosphorus

- Solids
 - Settleable 0
 - Suspended
 - 0 Total dissolved
 - Total 0

Heat Exchangers

Hazard Detectors

First Aid/Hygiene

Personal Protection Gear

Traffic Control (Warning Devices; Barricades)

Dehumidifiers

Compressors

Fans

Safety Equipment

- Volatile
- Oil and Grease
- Surfactants
- Temperature
- Total organic carbon
- **Turbidity**
- Volatile acids
- Settleability
- Phenol
- Sulfate sulfide
- Biomonitoring

Category of Information: General Information

Units of expression

- Define units
- Convert units

Sources and characteristics

- Characterize
- Quality/quantity
- Physical/chemical/biological

Effects

- Pre-aeration
- Chemical pre-treatment
- Grease control

Electrical (Basic)

Hydraulics (Basic)

Category of Information: General Information(continued)

Maps/plans - Interpretation and use

WWT Processes

- Sketch sequence
- Describe processes
- Explain why treated
- Goals of WWT (protect public; protect environment)

Grade 3 Wastewater Treatment Operator Need-To-Know Criteria

The following list of categories suggests topics of information which are important to know in order to be a successful and proficient Grade 4 Wastewater Treatment Operator. The list may not be all inclusive, and knowledge of additional topics may be of benefit to the operator

Category of Information: Processes

Collection Systems

- Types
- Inflow, Infiltration, Exfiltration
- Pre-treatment
- Sources of wastewater
- Pump stations

Flow

- Measurement
- Flow equalization

Screening

- Bar screens (hand-cleaned)
- Bar screens (mechanically cleaned)
- Static screen
- Microscreen

Grinding

- Grinders
- Comminutors
- Barminutors

Grit Removal

- Hand-cleaned grit chambers
- Mechanically-cleaned grit chambers
- Aerated grit chambers
- Vortex

Clarification

- Primary (Rectangular; Circular)
- Secondary
- SBR Clarification

Attached Growth/Fixed Film

- Trickling Filters
 - Standard Rate
 - o High Rate
 - Roughing
- Rotating Biological Contactor (RBC)
- Activated Biofilter (ABF)

Lagoons

- Aerobic
- Facultative
- Anaerobic
- Aerated
- Discharging

Activated Sludge

- Conventional
- Step Feed
- Contact Stabilization
- Extended aeration
- Tapered aeration
- Complete mix
- Pure oxygen
- Oxidation ditch
- Types of aeration
- Sequencing Batch Reactor (SBR)
- Membrane Biological Reactor (MBR)

Solids handling

- Sludge conditioning
- Sludge thickening
- Anaerobic digestors
- Aerobic digestors
- Dewatering
- IncinerationDrying beds
- Land application
- Composting
- 503 Regulations

Disinfection/ Use of Chlorine

- Chlorination
- Dechlorination
- UV
- Other methods

Advanced Treatment

- Filtration
- Nitrogen removal
- Phosphorus removal
- Biological

Effluent Disposal

- Discharge
- Direct Use
- Irrigation
- Underground Disposal
- NPDES Permit

Cross- Connection

- Prevention
- Types of devices

Category of Information: Support Systems

Motors

- Single Phase
- Polv Phase
- Variable Speed

Drives

- Coupled
- Direct (Shaft; Gear)
- Speed Reducer (Fixed; Variable)
- Right Angle

Pumps

- Air Lift
- Centrifugal
- Positive Displacement
 - o Piston Plunger
 - o Progressive Cavity
 - Diaphragm
- Screw
- Turbine
- Metering
- Ejector

Blowers and Compressors

- Centrifugal
- Positive Displacement (Rotary; Piston)

Generators - AC & DC

Engines - Gasoline, Diesel & Gas

Joints

- Flanged
- Compression
- Dresser
- Victualic
- Fused
- Threaded

Valves

- Ball
- Check
- Globe
- Gate
- Plug
- Petcock
- Pressure Control
- Vacuum Relief
- Mud
- Butterfly
- Multiport
- Telescoping
- Sluice Gate
- Air Release
- Foot
- Altitude

Fittings

- Coupling
- Union
- Plug/Caps
- Corporation (Ferrell; Cock)
- Curb Stop
- Special

Cathodic Protection Devices

- Anode Rod/Bags
- Cathode Rod/Bags
- Rectifiers
- Potentiometers

Measuring/ Control

- Signal Generators
 - o Kennison Nozzle
 - Magnetic Flowmeter
 - o Parshall Flume
 - Proportional Weir
 - o Rectangular Weir
 - Venturi
 - Propeller Meter
 - o Ultrasonic
 - o Pitot Tube
- Signal Transmitters
 - Electric
 - o Pneumatic
 - Hydraulic
 - o Mechanical
 - Telemetry
- Signal Receivers
 - Counters
 - o Indicators
 - o Log Scale Indicators
 - Totalizers
 - Recorders
 - Combination Recorders
- Meters
 - Hydraulic Rotameter
 - o Electrical Amp
 - Electrical Watt
 - Electrical Watt Hour
 - Electrical Multi.
 - o Electrical VOM
 - Electrical Megger
 - Mechanical RPM
- Alarms
- Controls
 - o Pneumatic
 - Float
 - o Hydraulic
 - o Electrical
 - Telemetry
 - o Timers

Category of Information: Support Systems (continued)

Chemical Feeders

- Solids
- Liquids
- Evaporators
- Gas
- Slurry

Odor Control

- Biofilters
- Chemical Additives
- Scrubbers

Rolling Stock

- Service Vehicles
- Trucks
- Tractors
- Trailers
- Lawn Mowers
- Loaders
- Portable Pumps
- Generators

HVAC

- Heat Exchangers
- Dehumidifiers
- Fans
- Compressors
- Condensers
- Boilers

Safety Equipment

- Personal Protection Gear
- Traffic Control (Warning Devices; Barricades)
- Hazard Detectors
- First Aid/Hygiene

Category of Information: Lab Tests

Routine Tests

- B.O.D.
- Ammonia
- Chlorine Residual
- Coliform (Fecal)
- E. coli
- Dissolved oxygen
- Total Kjedahl nitrogen
- pH

Control Tests

- Centrifuge
- Alkalinity
- C.O.D.
- Color
- Conductance
- Nutrients
- Micro exam
- Nitrate nitrite

Special Tests:

- Metals
- Chlorinated organics
- Cyanide

- Phosphorus
- Solids
 - o Settleable
 - o Suspended
 - Total dissolved
 - o Total
 - o Volatile
- Oil and Grease
- Surfactants
- Temperature
- Total organic carbon
- Turbidity
- Volatile acids
- Settleability
- Specific Oxygen Uptake Rate (SOUR)
- Phenol
- Sulfate sulfide
- Biomonitoring

Category of Information: General Information

Units of expression

- Define units
- Convert units

Electrical (Basic)

Hydraulics (Basic)

Maps/plans - Interpretation and use

Sources and characteristics

- Characterize
- Quality/quantity
- Physical/chemical/biological
- Effects
- Pre-aeration
- Chemical pre-treatment
- Grease control

WWT Processes

- Sketch sequence
- Describe processes
- Explain why treated
- Goals of WWT (protect public; protect environment)

Grade 4 Wastewater Treatment Operator Need-To-Know Criteria (Subject Areas)

The following list of categories suggests topics of information which are important to know in order to be a successful and proficient Grade 4 Wastewater Treatment Operator. The list may not be all inclusive, and knowledge of additional topics may be of benefit to the operator.

Category of Information: Processes

Collection Systems

- Types
- Inflow, Infiltration, Exfiltration
- Pre-treatment
- · Sources of wastewater
- Pump stations

Flow

- Measurement
- Flow equalization

Screening

- Bar screens (hand-cleaned)
- · Bar screens (mechanically cleaned)
- Static screen
- Microscreen

Grinding

- Grinders
- Comminutors
- Barminutors

Grit Removal

- Hand-cleaned grit chambers
- Mechanically-cleaned grit chambers
- Aerated grit chambers
- Vortex

Clarification

- Primary (Rectangular; Circular)
- Secondary
- SBR Clarification

Attached Growth/Fixed Film

- Trickling Filters
 - Standard Rate
 - High Rate
 - o Roughing
- Rotating Biological Contactor (RBC)
- Activated Biofilter (ABF)

Lagoons

- Aerobic
- Facultative
- Anaerobic
- Aerated
- Discharging

Activated Sludge

- Conventional
- Step Feed
- Contact Stabilization
- Extended aeration
- Tapered aeration
- Complete mix
- Pure oxygen
- Oxidation ditch
- Types of aeration
- Sequencing Batch Reactor (SBR)
- Membrane Biological Reactor (MBR)

Solids handling

- Sludge conditioning
- Sludge thickening
- Anaerobic digesters
- Aerobic digesters
- Dewatering
- Incineration
- Drying beds
- Land application
- Composting
- 503 Regulations

Disinfection/ Use of Chlorine

- Chlorination
- Dechlorination
- UV
- Other methods

Advanced Treatment

- Filtration
- Nitrogen removal
- Phosphorus removal
- Biological

Effluent Disposal

- Discharge
- Direct Use
- Irrigation
- Underground Disposal
- NPDES Permit

Cross- Connection

Prevention

Types of devices

Category of Information: Support Systems

Motors

- Single Phase
- Poly Phase
- Variable Speed

Drives

- Coupled
- Direct (Shaft; Gear)
- Speed Reducer (Fixed; Variable)
- Right Angle

Pumps

- Air Lift
- Centrifugal
- Positive Displacement
 - Piston Plunger
 - o Progressive Cavity
 - o Diaphragm
- Screw
- Turbine
- Metering
- Ejector

Blowers and Compressors

- Centrifugal
- Positive Displacement (Rotary; Piston)

Generators - AC & DC

Engines - Gasoline, Diesel & Gas

Joints

- Flanged
- Compression
- Dresser
- Victualic
- Fused
- Threaded

Valves

- Ball
- Check
- Globe
- Gate
- Plug
- Petcock
- Pressure Control
- Vacuum Relief
- Mud
- Butterfly
- Multiport
- Telescoping
- Sluice Gate
- Air Release
- Foot

Altitude

Fittings

- Coupling
- Union
- Plug/Caps
- Corporation (Ferrell; Cock)
- Curb Stop
- Special

Cathodic Protection Devices

- Anode Rod/Bags
- Cathode Rod/Bags
- Rectifiers
- Potentiometers

Measuring/ Control

- Signal Generators
 - Kennison Nozzle
 - o Magnetic Flowmeter
 - o Parshall Flume
 - Proportional Weir
 - o Rectangular Weir
 - o Venturi
 - Propeller Meter
 - o Ultrasonic
 - o Pitot Tube
- Signal Transmitters
 - Electric
 - o Pneumatic
 - o Hydraulic
 - o Mechanical
 - o Telemetry
- Signal Receivers
 - o Counters
 - Indicators
 - Log Scale Indicators
 - o Totalizers
 - Recorders
 - o Combination Recorders

Meters

- o Hydraulic Rotameter
- o Electrical Amp
- o Electrical Watt
- Electrical Watt Hour
- o Electrical Multi.
- Electrical VOM
- Electrical Megger
- Mechanical RPM
- Alarms
- Controls
 - o Pneumatic
 - Float
 - o Hydraulic
 - o Electrical
 - Telemetry
 - Timers

2

Category of Information: Support Systems (continued)

Chemical Feeders

- Solids
- Liquids
- Evaporators
- Gas
- Slurry

Odor Control

- Biofilters
- Chemical Additives
- Scrubbers

Rolling Stock

- Service Vehicles
- Fork Lifts
- Trucks
- Tractors
- Trailers
- Lawn Mowers
- Loaders
- Portable Pumps

Generators

HVAC

- Heat Exchangers
- Dehumidifiers
- Fans
- Compressors
- Condensers
- Boilers

Safety Equipment

- Personal Protection Gear
- Traffic Control (Warning Devices; Barricades)
- Hazard Detectors
- First Aid/Hygiene

Category of Information: Lab Tests

Routine Tests

- B.O.D.
- Ammonia
- Chlorine Residual
- Coliform (Fecal)
- E. coli
- Dissolved oxygen
- Total Kjedahl nitrogen
- pH

Control Tests

- Centrifuge
- Alkalinity
- C.O.D.
- Color
- Conductance
- Nutrients
- Micro exam
- Nitrate nitrite

Special Tests:

- Metals
- Chlorinated organics
- Cyanide

- Phosphorus
- Solids
 - o Settleable
 - o Suspended
 - Total dissolved
 - o Total
 - o Volatile
- Oil and Grease
- Surfactants
- Temperature
- Total organic carbon
- Turbidity
- Volatile acids
- Settleability
- Specific Oxygen Uptake Rate (SOUR)
- Phenol
- Sulfate sulfide
- Biomonitoring

Category of Information: General Information

Units of expression

- Define units
- Convert units

Electrical (Basic)

Hydraulics (Basic)

Sources and characteristics

- Characterize
- Quality/quantity
- Physical/chemical/biological
- Effects
- Pre-aeration
- Chemical pre-treatment
- Grease control

Maps/plans - Interpretation and use

WWT Processes

- Sketch sequence
- Describe processes
- Explain why treated
- Goals of WWT (protect public; protect environment)

Suggested Wastewater Treatment Exam References

The following are approved as reference sources for the ABC wastewater treatment examinations. Operators should use the latest edition of these reference sources to prepare for the exam.

Textbooks

California State University, Sacramento (CSUS) Foundation, Office of Water Programs (www.owp.csus.edu)

- Operation of Wastewater Treatment Plants, Volume I and II
- Advanced Waste Treatment
- Manage for Success

National Environmental Training Center for Small Communities (NETCSC)

• <u>Protecting Your Community's Assets: A Guide for Small Wastewater Systems</u> A PDF version of this guide is available from: www.nesc.wvu.edu/training.cfm

Water Environment Federation (www.wef.org)

- Operation of Municipal Wastewater Treatment Plants Manual of Practice No. 11
- Activated Sludge Manual of Practice OM-9

Regulations

- <u>National Pollutant Discharge Elimination System (NPDES) Permit</u>, State of Tennessee, Department of Environment and Conservation, Division of Water Resources, Nashville, TN, 1977, Latest Revision.
- <u>Design Criteria for Sewage Works</u>, State of Tennessee, Department of Environment and Conservation, Division of Water Resources, Nashville, Latest Revision.
- <u>Rules Governing Water and Wastewater Operator Certification</u>, State of Tennessee, Department of Environment and Conservation, Board of Certification for Water and Wastewater Operators, Nashville, Chapter 400-49-01, Latest Revision.
- <u>State of Tennessee General Water Quality Criteria, and Permits, and Effluent Limitations and Standards</u> State of Tennessee, Department of Environment and Conservation, Division of Water Resources, Nashville, TN, latest versions, Chapter 400-40-03 and Chapter 400-40-05.
- <u>State of Tennessee Cross-Connection Control Manual</u>, State of Tennessee Department of Environment and Conservation, Division of Water Resources, Latest Revision.
- <u>Water and Wastewater Operator Certification Act T.C.A.</u> Section 68-221-901. T.C.A. Section 68-221-915.
- Protection of Environment, (40 CFR Part 136), U.S. Environmental Protection Agency,

Study Guides

- <u>Applied Math for Wastewater Plant Operators</u>. Price, Joanne. 2000. Boca Raton, FL: CRC Press (www.crcpress.com)
- <u>WEF/ABC Wastewater Operators' Guide to Preparing for the Certification Examination</u>, Water Environment Federation, (www.wef.org)

Section 14 Answers to Vocabulary





Section 1 Introduction

- 1. Water Pollution
- 2. Inflow
- 3. Nutrient
- 4. Coliforms
- 5. Stabilization
- 6. BOD
- 7. Primary Treatment
- 8. Infiltration
- 9. Sanitary, Stormwater, Combined
- 10. Organic
- 11. Secondary Treatment
- 12. Receiving waters
- 13. Effluent
- 14. Inorganic

Section 3 Flow Measurement

- 1. Flow
- 2. Open Channel
- 3. Weir
- 4. Flume
- 5. Palmer-Bowlus
- 6. Converging Section
- 7. Throat
- 8. Closed Channel
- 9. Primary
- 10. Diverging
- 11. Parshall Flume
- 12. Head loss
- 13. Secondary
- 14. Flow Equalization

Section 2 Preliminary Treatment

- 1. Diffuser
- 2. Grit
- 3. Hydrogen Sulfide
- 4. Mechanically, Screen
- 5. Fine
- 6. Wedgewire
- 7. Rotary Drum
- 8. Escalating Step Screen
- 9. Comminutor
- 10. Paint Filter Test
- 11. Septage
- 12. Grit Channel
- 13. Aerated Grit Chamber
- 14. Cyclonic Grit
- 15. Adsorption
- 16. Absorption
- 17. Flow Equalization

Section 4 Activated Sludge Systems

- 1. Absorption
- 2. Biomass
- 3. Activated Sludge
- 4. Adsorption
- 5. Aeration Basin
- 6. Facultative
- 7. MLSS
- 8. Aerobic, Anaerobic
- 9. Filamentous
- 10. MLVSS
- 11. Anoxic
- 12. Endogenous Respiration
- 13. Mixed Liquor
- 14. Zoogleal

Section 5 Fixed Film Systems

- 1. Biomass, Zoogleal film
- 2. Aerobic, Anaerobic
- 3. Distributor
- 4. Fixed-spray Nozzle
- 5. Nitrification
- 6. Humus Sludge
- 7. Series Operation, Parallel Operation
- 8. Ponding
- 9. Recirculation
- 10. Trickling Filter
- 11.2 Stage Filter
- 12. Underdrain, Ventilation

Section 7 Ponds and Lagoons

- 1. Stabilization Ponds
- 2. Polishing Pond
- 3. Overturn/Turnover
- 4. Parallel
- 5. Aerobic Ponds
- 6. Anaerobic Ponds
- 7. Bioflocculation
- 8. Oxidation Ponds
- 9. Facultative Ponds
- 10. Photosynthesis
- 11. Algae
- 12. Respiration
- 13. Series
- 14. Thermocline

Section 6 Sedimentation and Flotation

- 1. Sludge
- 2. Bulking
- 3. Septic
- 4. Flocculation
- 5. Gasification
- 6. Coagulant
- 7. Secondary clarifier
- 8. Short circuiting
- 9. Surface Loading Rate
- 10.Colloid
- 11. Solids Loading Rate
- 12. Detention time
- 13.Flights
- 14. Denitrification
- 15.Weir
- 16. Weir Overflow Rate
- 17. Primary Clarifier
- 18.Launder
- 19.SVI
- 20.Flotation
- 21. Sloughings

Section 8 Disinfection

- 1. Pathogenic, Waterborne Disease
- 2. Disinfection, Sterilization
- 3. Free Chlorine
- 4. Combined Chlorine
- 5. Oxidizing Agent
- 6. Free Chlorine Residual
- 7. Post Chlorination
- 8. Chlorine Residual
- 9. Reducing Agent
- 10. Chlorine Demand
- 11. Prechlorination
- 12. Breakpoint Chlorination
- 13. Ozonation
- 14. Chlorination
- 15. UV Disinfection

Section 9 Effluent Disposal

- 1. Surface Waters
- 2. Fixed Sample
- 3. Grab
- 4. Composite
- 5. Respiration
- 6. Evapotranspiration
- 7. Irrigation
- 8. Ridge and Furrow
- 9. Spray Systems
- 10. Overland Flow
- 11. D.O. profile
- 12. Outfall

Section 11 Safety

- 1. Competent Person
- 2. Decibel
- 3. Lower Explosive Limit
- 4. Olfactory Fatigue
- 5. Oxygen Enrichment
- 6. Acute, Chronic
- 7. IDLH
- 8. Oxygen Deficiency
- 9. Sewer gas
- 10. Spoil
- 11. Confined Space
- 12. Carcinogen
- 13. Non-sparking tool
- 14. Engulfment
- 15. Permit-required
- 16. Non-permit
- 17. Septic
- 18. Mercaptans

Section 10 WWTP Administration and Management

- 1. Authority
- 2. Organizing
- 3. Responsibility
- 4. Tailgate Safety Meeting
- 5. Ethics
- 6. Accountability
- 7. Delegation
- 8. Preventative
- 9. Critical Infrastructure
- 10. Vulnerability
- 11. Whistleblowing
- 12. Predictive